

THE HIGH VALUE OF LOW-PRESSURE GEOTHERMAL STEAM

K. C. LEE

Geothermal Institute, The University of Auckland

SUMMARY - Over the pressure range of 1-20 bar abs where most geothermal power plants operate, a 10% pressure loss of **saturated steam** causes a power loss of about 12 kWe/(kg/s) **steam flow rate** (i.e. electrical energy loss of 12 kJ/kg **steam**). For example, a **steam** pressure loss from 10 to 9 bar abs (1 bar drop = 10% loss) causes an electrical energy loss of 12 kJ/kg (at 80% turbine efficiency and 0.1 bar abs condenser pressure); but a pressure loss from 1 to 0.9 bar abs (0.1 bar drop = 10% loss) causes a loss of 13 kJ/kg. This is worth about \$4000/year per kg/s of steam at 5 cents/kWh and 80% plant factor. Hence, pressure loss of low-pressure **steam** costs much more than the same pressure loss of high-pressure steam. Therefore, attention should be paid to reducing pressure loss in low-pressure geothermal **steam**.

1. INTRODUCTION

The most valuable type of geothermal resource is one that can be used for power production. Unfortunately, this type of resource is rare considering the large number of geothermal energy resources, and the vast amount of geothermal energy available. Hence, these rare resources should be used efficiently.

Most geothermal fields for power production are wet fields producing two-phase steam-water fluids at the wellheads from wells about 1-2 km deep. Saturated **steam** is then separated from the water, and the **steam** is transmitted in long **steam** pipelines to **steam** turbines for power production. The **saturated steam** pressure is commonly around 7 bar abs but can be as low as 1.1 bar abs as in Wairakei LP (low-pressure) **steam**, or as high as 25 bar abs as in Rotokawa. It is common for the **steam** pressure to drop 10-20% after travelling several km in pipelines from the separators to the steam turbines. The pressure loss is due mainly to friction, and the pipe wall roughness is a major contributing factor.

Figure 1 shows that the pipe wall roughness could increase 5 to 20 times and the friction factor up to 200% due to corrosion and deposition scales after some years of operation (Lee et al, 1997). To reduce the friction factor, it was recommended that the pipe walls be cleaned every 10 years. However, it is found that 0.1 bar pressure loss from LP steam of 1 bar abs costs as much as 1 bar pressure loss from high-pressure (HP) **steam** at 10 bar abs. Therefore, the high value of LP **steam** warrants more attention be paid to reducing pressure loss in LP **steam**. For example, a 5-year old 1200mm diameter **steam** pipeline had a Darcy friction factor of 0.009, while a 20-year old one

had 0.014 (Lee et al, 1997). So, the pressure loss in the older pipe can be reduced by 35% if it is cleaned of the corrosion and deposition scales. At the current flow conditions, this translates to about \$15,000/year at 1 cent/kWh.

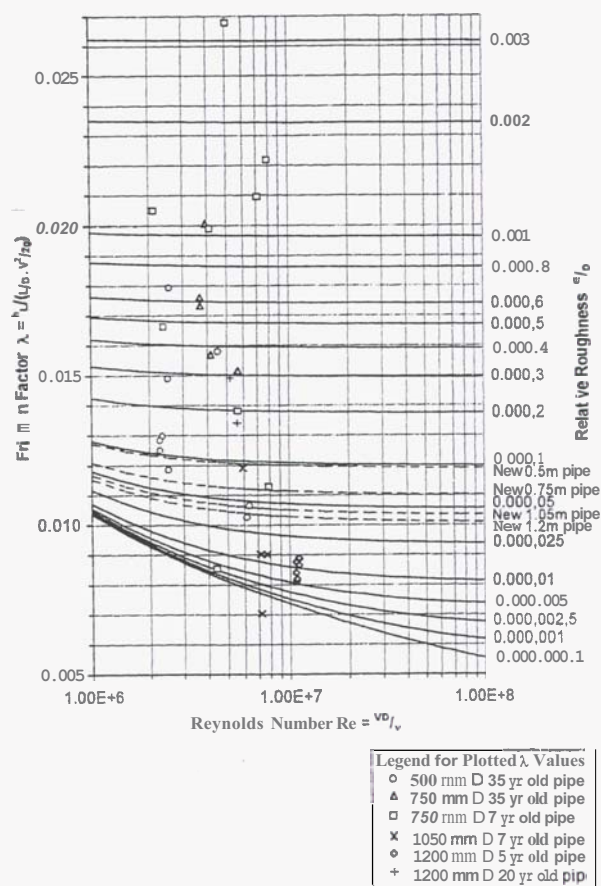


Figure 1: Measured and predicted friction factors plotted on Moody diagram (Lee et al, 1997)

This paper looks at geothermal **steam** piping costs, **costs** of **steam** pressure losses, and attempts to explain the **high** value of low-pressure geothermal **steam**.

2. STEAMPIPING

Geothermal **main steam** transmission pipelines are generally large (nominal diameter (DN) 500-1100 mm) and thin wall (8-13 mm). A steamfield in production may have **tens** of km pipelines and hundreds of **pipe supports**. Koorey (2000) and Niu (2001) attempted to reducing piping **cost** by maximising pipe **support spans**. The **maximum spans** are limited by the local stresses at the pipe supports due to the thin pipe walls. Reinforcing saddles **can** be **used** at the supports to increase the support spans. The maximum **span** for large diameter (DN>500 mm) pipelines is about 20 m.

Although the method for pressure **drop** prediction in single-phase flow is well established using a Moody diagram to indicate friction factor, the accuracy of pressure drop prediction in geothermal **steam** pipelines depends very much on the accuracy of the pipe wall roughness heights **used**. While the wall roughness of a new pipe is known reasonably accurately, a geothermal **steam** pipeline, after many years of **service**, will have corrosion and/or deposition scales that change the pipe wall roughness dramatically. For example, Wairakei 40-year old 750mm DN **steam main** lines have wall roughness of 0.23-0.83 mm (Lee et al 1997) whereas a new pipe **has** 0.046 mm (Moody diagram). Although the wall roughness may increase by 20 times, the increase in **friction** factor is only about 2 times. i.e. **the** pressure loss is doubled. This shows that the inside walls of steam pipelines **need** to be cleaned after a period of service (about 10 years), depending on **steam** quality, corrosion and deposition **rates**.

3. COST OF STEAMPIPING

The **total installed** cost (excluding valves and engineering costs) of piping varies **between** US\$2.5-3.1/kg (US\$5.0-8.7/DIF (diameter-inch-foot)) for 250 mm DN (10") to 1050 mm DN (42") pipes based on a 1997 Philippines geothermal project as shown in Figure 2. The **cost** is inclusive of thermal insulation and pipe supports but excluding valves and engineering costs. Installed **cost** of piping in \$/kg is reasonably constant over the diameter range compared to \$/DIF.

4. COST OF STEAMPRESSUREDROP

For a typical wet geothermal field producing saturated **steam** in the range of 1-20 bar abs, a 10% **steam** pressure loss **causes** a power loss of 12±1 kWe per kg/s **steam** (i.e. an electrical energy loss of 12±1 kJ/kg **steam**) as shown in Fig. 3. This is equivalent to 24% power loss, **assuming** 80% turbine efficiency and a condenser pressure

of 0.1 bar abs (see Fig. 4). Fig. 3 **also** shows that the power loss is not **affected** significantly by condenser pressure for the Same percentage pressure loss, but **that** the power loss is doubled when the percentage **pressure** loss is doubled.

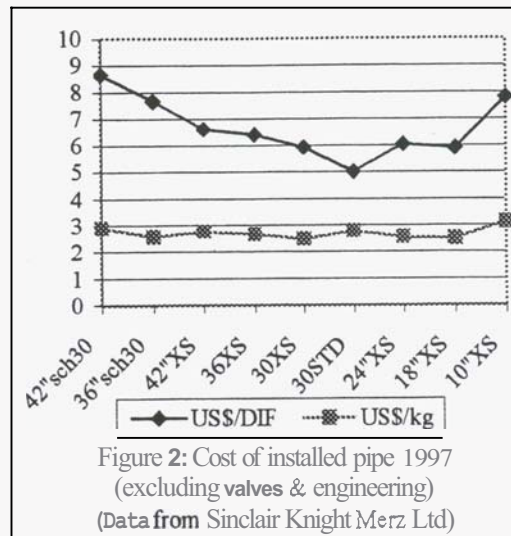


Figure 2: Cost of installed pipe 1997 (excluding valves & engineering) (Data from Sinclair Knight Merz Ltd)

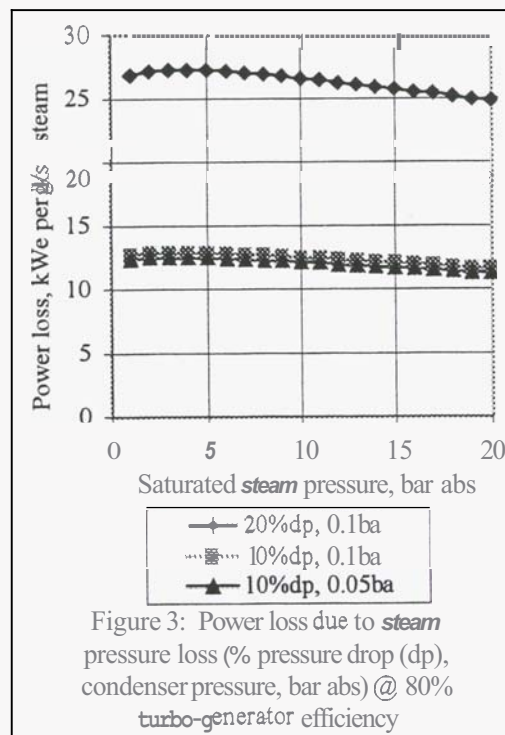
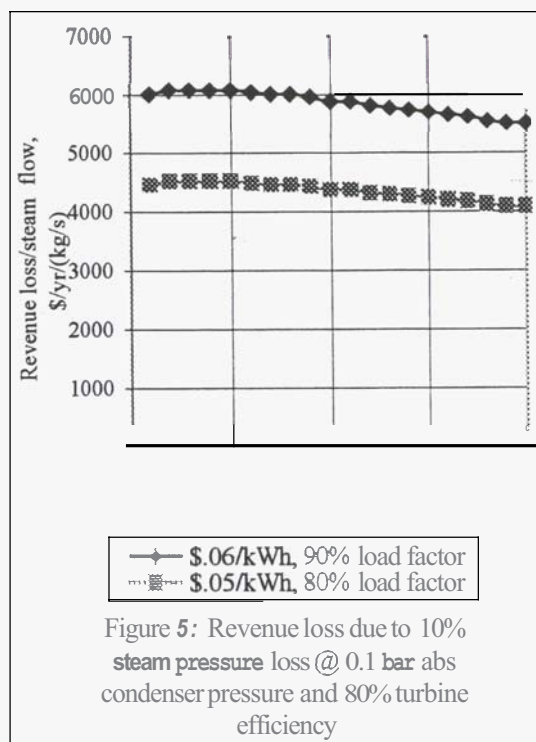
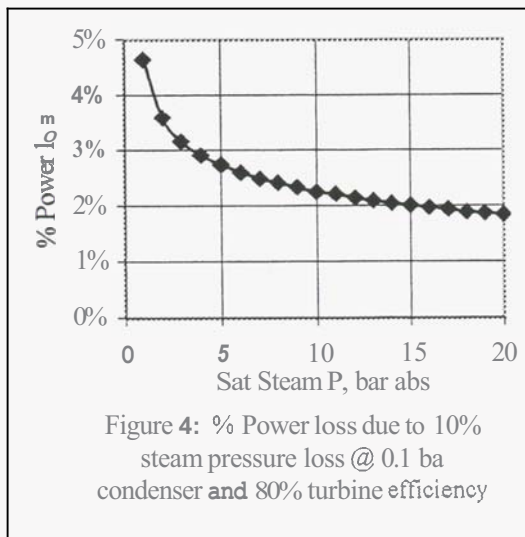


Figure 3: Power loss due to **steam** pressure loss (% pressure drop (dp), condenser pressure, bar abs) @ 80% turbo-generator efficiency

For example, at 10 bar abs turbine inlet saturated **steam** pressure and 0.1 bar abs condenser pressure, the electrical energy **produced** is 553 kJ/kg. At 9 bar abs (10% pressure loss), energy produced is 541 kJ/kg. So, the energy loss = 553-541=12 kJ/kg. Similarly, for 0.05 bar abs condenser pressure, the energy loss = 615-603=12 kJ/kg. The effect of condenser pressure **between** 0.05-0.1 bar abs on energy loss due to 10% **steam** pressure loss is therefore insignificant (2.5%). [However, the effect of condenser pressure on

power output is significant for a constant **steam** turbine inlet pressure (at 10 **bar abs**, power loss = $615-553=62 \text{ kJ/kg}=11\%$). The equivalent **annual** revenue loss is between \$4000-\$6000 per kg/s **steam** as shown in Fig. 5 (5 cents/kWh & 80% load factor and 6 cents/kWh & 90% load factor). Doubling the percentage **steam** pressure loss **marginally more** than doubles the power loss **hence** the revenue loss.



A 10% **steam** pressure loss of low-pressure **steam** is relatively smaller in term of **magnitude** of pressure loss but causes marginally higher power loss and revenue loss compared to high-pressure **steam**. That is, 0.1 bar pressure loss at 1 bar absolute **steam** costs as much as 1 bar pressure

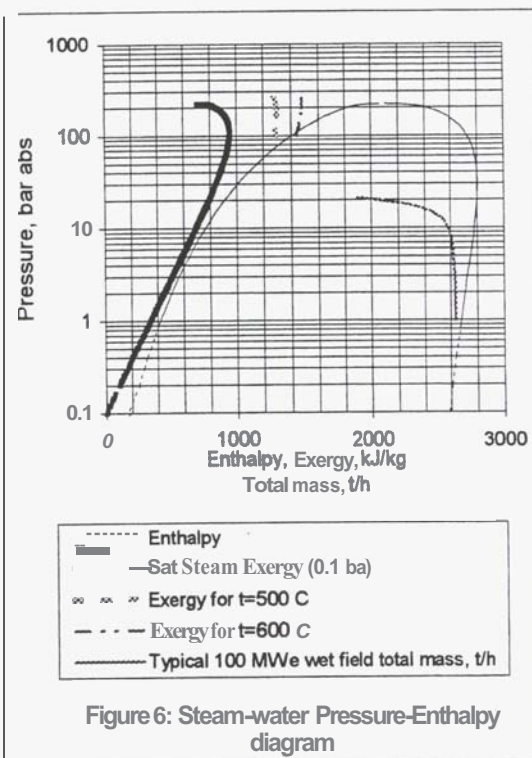
loss at 10 bar absolute **steam**. In other words, pressure loss at low **steam** pressure costs **much** more than the same **pressure** loss at high **steam** pressure.

5. PRESSURE DROP DUE TO DRAIN POTS

Lee (1981) showed that Wairakei's shallow drain pots were 40% efficient (water flow rate removed/water flow rate upstream of drain pot), deep drain pots were 80% efficient, and a drain pot with a baffle plate had 95% efficiency. The pressure drop coefficient ($\Delta P / \frac{1}{2} \rho v^2$) across a drain pot is about 10%. For a typical **steam** pressure of 7 bar abs and **steam** velocity of 40 m/s, the pressure drop across a drain pot is only 300 Pa (0.003 bar).

6. PRESSURE-ENTHALPY DIAGRAM

To explain the **almost** constant power loss over the pressure range of 1-20 bar abs due to a constant percentage of **steam** pressure loss in Figure 3, it is best to look at the steam exergy on a pressure-enthalpy (P-h) diagram in semi-log plot as shown in Figure 6. The **saturated steam** exergy based on 0.1 bar abs condenser pressure is plotted. Exergies for supercritical **steam** of 500°C and 600°C over 100-300 bar abs are also plotted for comparison. A typical wet geothermal field total mass output for a 100 MWe power station is also plotted.



The **saturated steam** enthalpy is **almost** a straight line from 1 to 20 bar abs on Figure 6. Similarly, the saturated **steam** exergy line is also nearly a

Straight line over the same **pressure** range. A straight line with the pressure on log scale clearly shows that a **constant** percentage of **pressure** loss over the **pressure** range will give a constant exergy loss. For example, a 10% pressure loss from 10 to 9 bars gives the same vertical height as a 10% pressure loss from 1 to 0.9 bar, and therefore the same **exergy** differential on the linear horizontal exergy scale. Since power or electrical energy is proportional to exergy by the turbine efficiency factor, this explains the **almost** constant power loss for a constant percentage of **steam** pressure loss in Figure 3.

It is **interesting** to note that the **exergy** of **saturated steam** at a pressure **near** the critical point, say 200 bar abs, is actually less than that at 100 bar abs where approximately the **maximum** occurs. Similarly, for supercritical **steam** at constant temperature, a maximum exergy exists with respect to **pressure**.

The total **mass** curve on Figure 6 clearly shows the **typical** constant **mass** flow at low wellhead pressure (WHP) but rapid decline with **high** WHP. This means that over the low-pressure range of 1-10 bar abs WHP, the **pressure** loss in a **steam** pipeline does not significantly affect the total mass flow from the wells. At **high** WHP (>10 bar abs), to **maintain** a constant pressure at the turbine inlet, higher pressure loss in the **steam** pipeline will require **higher** WHP which may reduce the well **output** significantly. **However**, the operating pressure is selected at the maximum power potential point which is likely to be **between** 1-10 bar abs for the typical mass curve in Figure 6. **Hence**, Figure 3 is valid even when **total** output characteristics of wells are taken **into** account.

7. CONCLUSIONS

Installed cost of mild **steel** piping for geothermal fluid transmission in 1997 was about **US\$3/kg** for

DN 250-1050 mm (10"-42") including pipe supports and thermal insulation but excluding valves and engineering design.

A 10% **saturated** steam pressure loss will **cause** a power loss of about 12 kWe/(kg/s) of **steam** over the pressure range of 1-20 bar abs. This is worth **\$4000-\$5000/year** per kg/s of **steam** at 5 cents/kWh and 80% plant factor. Pressure loss of low-pressure steam **costs** more than the **Same** pressure loss of high-pressure **steam**, hence the **high** value of low-pressure geothermal **steam**.

The constant power loss due to a constant percentage of saturated steam pressure loss can be explained by the straight line exergy plot on the semi-log pressure-enthalpy diagram.

ACKNOWLEDGMENTS

I thank the management of Sinclair Knight Merz Ltd of Auckland for allowing me to use their data. I also thank those at SKM for the provision of data, much helps and comments.

REFERENCES

- Koorey, K., (2000). Determination of the optimal pipe support spans for geothermal pipelines. *Proc WGC 2000, Florence, Italy, ZGA*, v3, 1361-1364.
- Lee, KC (1981): Performance tests of the condensate drain pots at Wairakei. *Proc 4th NZ Geothermal Workshop, The University of Auckland*, pp123-126.
- Lee, KC et al (1997): Long geothermal steam transmission pipeline. *Proc IPENZ Conf, Wellington*, v2, pp258-262.
- Niu, F., (2001). Optimising geothermal pipe support spacing. Report No. 2001.18, *Geothermal Institute, The University of Auckland*.