



# DRILLING/COMPLETION AND TESTING OF GEOTHERMAL DISTRICT HEATING (GDH) DOUBLET

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# DRILLING OF GEOTHERMAL DISTRICT HEATING (GDH) DOUBLETS





# OUTLINE



- SCOPE
- INTRODUCTION. GEOTHERMAL VS PETROLEUM
- DEEP WELL DRILLING/COMPLETION FEATURES
  - Rig selection
  - Site preparation. Rig footprint
  - Drilling
  - Bits
  - Drilling fluids
  - Directional drilling
  - Casing/lining
  - Cementing
  - Fishing
  - Waste disposal/processing
- CASE STUDY. PARIS BASIN GDH TRIPLET
- MEDIUM ENTHALPY CHP EXPLORATION
  - Deep (4-5 km) exploratory project
  - Slimhole strategy
- UNCONVENTIONAL GEOTHERMAL WELL DESIGNS
  - Dual completion
  - Fiberglass lined anti-corrosion well
  - (sub)Horizontal well concept
- MISCELLANEOUS ISSUES
  - Water injection
  - Mining risk insurance
  - Sustainability
  - Environment
  - Workover
  - Screens
  - Mud solids'control
- DRILLING CONTRACT. RIG MANAGEMENT. WORK SUPERVISION



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Provide an engineering insight into drilling and completion technology to future geothermal players with focus on design and implementation of deep, geothermal district heating (GDH) oriented, well doublets in sedimentary environments and urban/suburban locations.

Future, non conventional, well and completion designs are also discussed.



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# INTRODUCTION

## GEOHERMAL VS PETROLEUM



### INTERCOMPARISON SUMMARY SHEET

CHARACTERISTICS	GEOPOWER	GEOHEAT/CHP	OIL & GAS
Reservoir Environment	Volcano-tectonic	Sedimentary	Sedimentary
Rock type(s)	Volcanic, metamorphic <sup>(1)</sup>	Carbonate, clastic	Carbonate, clastic, shale <sup>(2)</sup> , source rocks <sup>(2)</sup>
Depth	1 000-3 000	1 000-5 000 <sup>(3)</sup>	1 000-10 000 <sup>(4)</sup>
Pressure <sup>(1)</sup>	Under pressured	Low to near hydrostatic	Low to high
Temperature	200-350° C	30-130° C	30-250° C
Flowrate	200-350 t/h <sup>(5)</sup>	150-350 m <sup>3</sup> /h	10-5 000 bbd
Fluid state	Single phase (liquid, stean) Two phase (liquid, stean)	Single phase liquid, solution gas	Single (oil, gas) Two (oil/ water, gas/water) Three phase (oil, gas)
Porosity type	Dominantly featured	Intergranular (Matirx), Fractured	Intergranular (Matrix), Fractured Non connected <sup>(6)</sup>
Site location	Remote land	Urban <sup>(7)</sup> , suburban <sup>(7)</sup> , rural <sup>(8)</sup>	Remote land off/shore
Well design	Large diameter High delivery	Large diameter high delivery	Small medium diameter
Diameter	9 <sup>5</sup> / <sub>8</sub> csg x 7" / 7 <sup>5</sup> / <sub>8</sub> (s.l.) or 8 <sup>1</sup> / <sub>2</sub> (OH) <sup>(9)</sup>	13 <sup>3</sup> / <sub>8</sub> x 9 <sup>5</sup> / <sub>8</sub> x csg x 8 <sup>1</sup> / <sub>2</sub> (OH) or 7 s.l. or 6-7" screen	7" csg x 5" tbg x perforated cemented 7"/5" csg <sup>(11)</sup>
Completion	Fullbore casing production Slotted liner completion	Fullbore casing production. Openhole, slotted liner, screen	Inner tubing/packer/safety valve completion
Production	Self flowing 2 phase (vapour lift)	Artificial lift Self flowing	Artificial lift gravity, self flowing



# INTRODUCTION

## GEOHERMAL VS PETROLEUM



### INTERCOMPARISON SUMMARY SHEET

#### footnote

- (1) rhyolitic/andesitic/metamorphic
- (2) Shale gas, source rock oil
- (3) CHP targeted wells (Hydrothermal or EGS)
- (4) Depth of tiber one well in the Gulf of Mexico
- (5) Total flow
- (6) Shale gas
- (7) Geothermal district heating
- (8) Green house heating
- (9) Standard. Exceptionally  $13^{3/8} \times 9^{5/8} / 10^{3/4}$  (s.l.)  $\times 12^{1/4}$  (OH)
- (10) Slotted x wire wrapped gravel packed screen assembly for sand control
- (11) though tubing x packer x safety valve assembly (diesel filled annulus)





## DRILLING/COMPLETION TECHNOLOGY AND PRACTICE

- Drilling of deep geothermal wells shares the same techniques and equipment in use in the oil and gas industry, whatever the significant differences, particularly in high enthalpy settings, existing between petroleum and geothermal resource environments with respect to petrography, formation temperatures and fluid thermochemistry.
- These differences require that, within a similar technological framework, specific drilling/completion procedures be implemented whenever dictated by reservoir/fluid conditions.
- Regarding low enthalpy (GDH) objectives the high production target implies appropriate customised completion (re)designs.



# INTRODUCTION



## WELL DRILLING AND COMPLETION AERIAL VIEW OF THE MELUN I'ALMONT DRILL SITE







# EUROPEAN DISTRICT HEATING LOCATIONS



MUNICH

HUNGARIAN PLAIN

PARIS



# EUROPEAN GEOTHERMAL DISTRICT HEATING (GDH) STATUS



	Existing (@ 2011)	Commissioned (@ 2015)
<b>GDH PLANTS</b>		
Europe at large (*)	210	390
EU Member States	135	300
France	45	60
Paris Basin	35	45
<b>INSTALLED CAPACITIES (MW<sub>t</sub>)</b>		
Europe at large (*)	3950	7000
EU Member States	1600	3500
France	310	
Paris Basin	290	
<b>HEAT PRODUCTION (TJ/yr)</b>		
Europe at large (*)	40000	
EU Member States	16500	
France	4050 (**)	
Paris Basin	3750 (**)	

(\*) EU m.s. + Iceland & Macedonia

(source : EGEC, 2011)

(\*\*) Including gas cogenerated base heat load (#1500 TJ/yr)



# DEEP DRILLING CANDIDATE RIGS



Hook load	Mast	Nominal power	Tête d'injection motorisé (top drive, power swivel)	Pumps	Mud quarter	Miscellaneous
250 - 300 t dyn	Telescopic, Total height 26-31 m, Total clearance/stroke 16-18 m	1100 – 1500 kW	Torque = 3600- 6000daNm Power = 375-500 kW Traction = 250-300 t Speed = 180-200 rpm Pressure = 350 bar	2 – 3 Triplex 1500-2000 kW 3600-5000 l/min 345 bar	3-4 tanks (1 mixing) 120-200 m <sup>3</sup> 2 silos 1 hopper 2 transfer pumps 2 shale shaker desanders 2 transfer pumps desilter(s) mud degaser solids CONTROL : 2	Options : - connection to grid (PCR) - automatic pipe handling - hydrocyclones - BOP : standard + 1 rotating BOP



MOBILE HYDRAULIC HOIST RIGS				technical data				
Model	strokehead in	strokehead m	new pulleys in	stroke in	top drive torque ft lbs	top drive torque daNm	gross weight kg	
HH-100	200,000	91	44,000	20	540 402	20,026 3520	49 m <sup>3</sup> 15	94,800 43,000
HH-102	220,000	100	44,000	20	560 418	20,026 3520	52 m <sup>3</sup> 16	99,200 45,000
HH-150	300,000	136	44,000	20	700 522	20,026 3520	56 m <sup>3</sup> 16	110,200 50,000
HH-200	400,000	181	44,000	20	1340 1000	20,026 3520	56 m <sup>3</sup> 18	121,200 55,000
HH-250	441,000	200	44,000	20	1340 1000	20,026 3520	56 m <sup>3</sup> 18	122,200 60,000
HH-300	600,000	272	66,000	20	1542 1150	36,141 4900	52 m <sup>3</sup> 18	198,420 90,000





# UNIT EQUIVALENTS



US units		SF/Hybrid units
inch (in)	length	25.4 mm
in <sup>2</sup>	area	6.45 cm <sup>2</sup>
in <sup>3</sup>	volume	16.4 cm <sup>3</sup>
foot/feet (ft)	length	0.305 m
ft <sup>2</sup>	area	0.093 m
ft <sup>3</sup>	volume	28.3 l
gallon (gal)	volume	3.79 l
gallon per minute (gpm)	flowrate	3.79 l/mn
pound force (lbf)	force	0.445 daN
pound /sq.inch (psi)	pressure	6.89 kPa
pound/feet (lb/ft)	nominal weight	0.069 bar
pound feet (lb/ft)	torque	0.136 daN.m
horse power (Hp)	power	746 waHs



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# RIG SELECTION

## ITEMIZED DRILLING & COMPLETION SEQUENCE (ADAPTED FROM HAGEN HOLE)



- Reservoir engineering & Well targeting
- Well design and specification
- Materials specification & procurement
- Well pad & access road civil design and engineering
- Water supply design & engineering
- Civil construction supervision
- Well drilling engineering and supervision
- Provision of drilling rig and equipment
- Provision of drilling personnel
- Provision of top drive equipment & personnel
- Provision of cementing equipment, personnel & services
- Provision of directional drilling equipment & personnel
- Provision of mud engineering personnel
- Provision of aerated drilling equipment and personnel (optional)
- Provision of mud logging / geology equipment & personnel
- Drilling tool rental or purchase
- Drill pipe inspection & hard-banding
- Provision of well measurements equipment and personnel





# RIG SELECTION REQUIREMENTS

EXPLORATION	High risk, higher rig capacity (hook load impact on work specifications and contractor skills/experience)
DEVELOPMENT	Low risk, normal and optimised rig capacity and equipment standards and specification
DEPTH TARGET	Rig capacity
WELL ARCHITECTURE	Rig capacity
MAXIMUM WEIGHT IN HOLE	Rig capacity
ENVIRONMENTAL IMPACT	Low noise, low gas emission, stringent safety and waste disposal regulations, limited foot print
RISK ANALYSIS	Mandatory in assessing the technical/environmental/economic risk
FLUID COMPOSITION	Personnel (crew and neighbours) safety
RESERVOIR PRESSURE	BOP, high pressure equipment and monitoring equipment
RIG/PERSONNEL PERFORMANCE	Mandatory in ranking candidate competitor capability in meeting project specifications and selecting contractor

IDEALLY, GIVEN A 2000 M DEVIATED (35°C) 9"5/8

CASED WELL IN AN URBAN ENVIRONMENT, A 250 t dyn HOOK LOAD, ELECTRICALLY/HYDRAULICALLY POWERED, LIMITED FOOT PRINT, HIGH TORQUE TOP DRIVE AND 3600 l/min TRIPLEX PUMP CAPACITY WOULD BEST SUIT GDH SPECS.



# CONVENTIONAL RIG (200 T)





# CONVENTIONAL HEAVY DUTY LAND RIG (600 T)





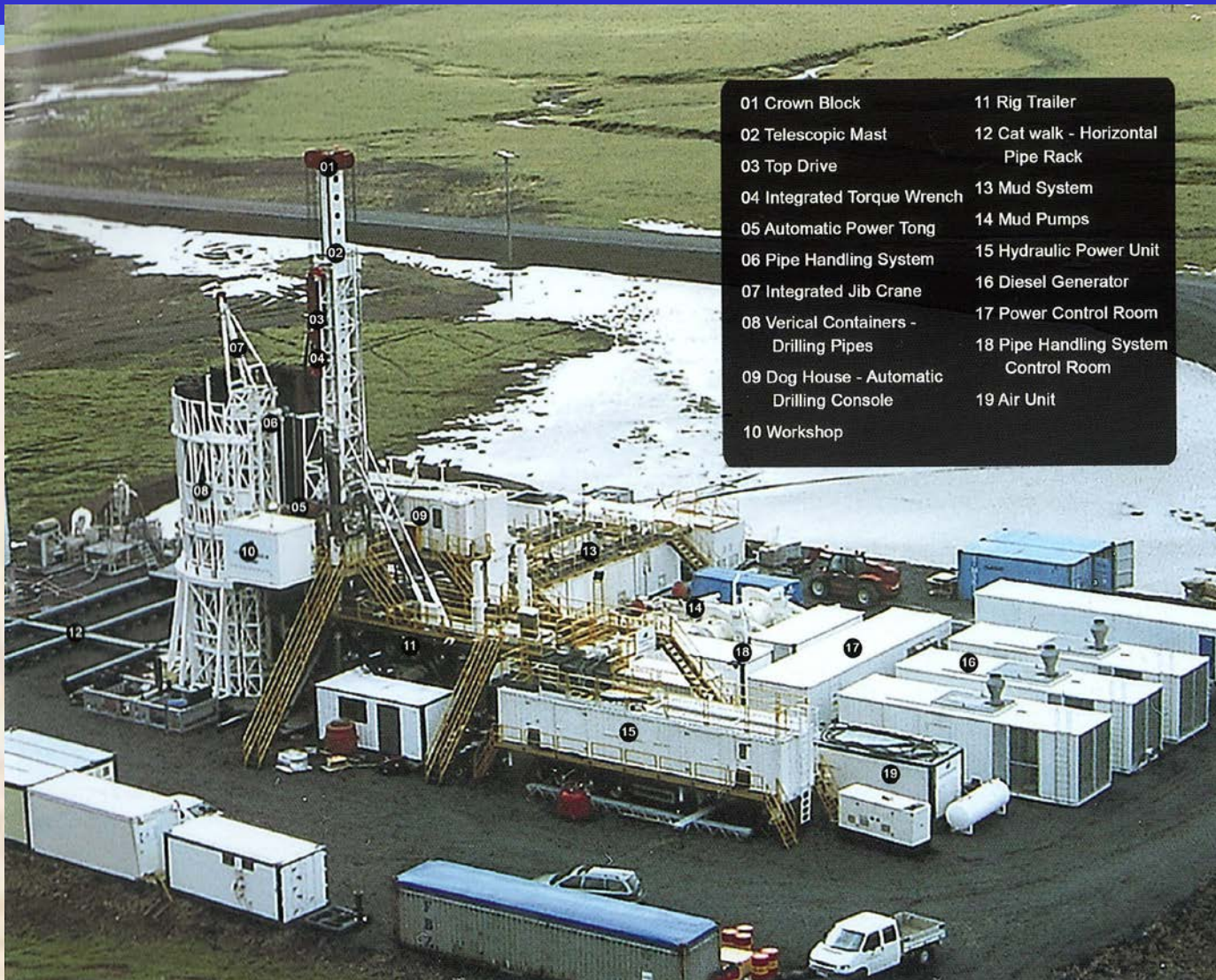
# CONVENTIONAL HEAVY DUTY LAND RIG DESCRIPTION



Source : DRILLMEC



# NOVEL DESIGN HEAVY DUTY HYDRAULIC RIG



- |   |                                      |
|---|--------------------------------------|
| 01 Crown Block                            | 11 Rig Trailer                       |
| 02 Telescopic Mast                        | 12 Cat walk - Horizontal Pipe Rack   |
| 03 Top Drive                              | 13 Mud System                        |
| 04 Integrated Torque Wrench               | 14 Mud Pumps                         |
| 05 Automatic Power Tong                   | 15 Hydraulic Power Unit              |
| 06 Pipe Handling System                   | 16 Diesel Generator                  |
| 07 Integrated Jib Crane                   | 17 Power Control Room                |
| 08 Vertical Containers - Drilling Pipes   | 18 Pipe Handling System Control Room |
| 09 Dog House - Automatic Drilling Console | 19 Air Unit                          |
| 10 Workshop                               |                                      |

Source : DRILLMEC



# INNOVATIVE RIG HYDRAULIC/ELECTRIC



**FLEXIBLE AND FAST INSTALLATION ALSO IN REMOTE AREAS:  
DEEP DRILLING RIG TERRA INVADER 350/450 SLINGSHOT**



Source : Herrenknecht Vertical GmbH)



# NOVEL COMPACT HYDRAULIC RIG DESIGN



	SPECIFICATIONS TBA 300	
	<b>Mast</b>	
	Static hook load	300 tn ..... 600,000 lbf
	Max. stroke height	20,0 m ..... 65,6 ft
	Overall height (from GL)	41,0 m ..... 134,5 ft
	<b>Draw Works</b>	
	Hybrid draw works	
	Winch (casing installation)	
	Pull (8 lines)	300 tn ..... 600,000 lbf
	Single line pull	44 tn ..... 88,000 lbf
	Stroke	20,0 m ..... 65,6 ft
	Drill pipe length (super single range III)	12,4 m ..... 40,7 ft
	max. casing length (class Range III)	14,6 m ..... 48 ft
	Crowd cylinder (DP installation)	
	Pull	138 tn ..... 276,000 lbf
	Push	33 tn ..... 66,000 lbf
	Stroke	14,0 m ..... 45,9 ft
	<b>Top Drive</b>	
	Type	TDK 65 hydraulically driven
	Rated input	530 kW ..... 711 HP
	Break out torque (max.)	65 kNm ..... 47,940 lbf-ft
	Rotation speed	0 – 180 rpm
	<b>Electro-Hydraulic Powerpack</b>	
	Rating	810 kW ..... 1,086 HP
	<b>Iron Roughneck</b>	
	Type	Varco ST 80
	<b>Power Slip</b>	
	Type	Varco PS 21
	<b>VFD Control Room</b>	
	Type	Bentec
	<b>BOP Blow Out Preventer</b>	
		13 5/8" ..... 345 bar ..... 5,000 psi

Source : BAUER



# RIG SELECTION

## EXPERIENCE AND QUALIFICATION OF PERSONNEL & SUITABILITY EQUIPMENT EVALUATION SHEET



		Maximum Points Allocation
1.0	Evidence with similar projects carried out in home country and internationally for the last 10 years	15
2.0	Drilling Rig and Equipment	45
3.0	Qualifications and Experience of Personnel	35
4.0	Company Profile and Personnel Structure	5
TOTAL POINTS		100



# OUTLINE

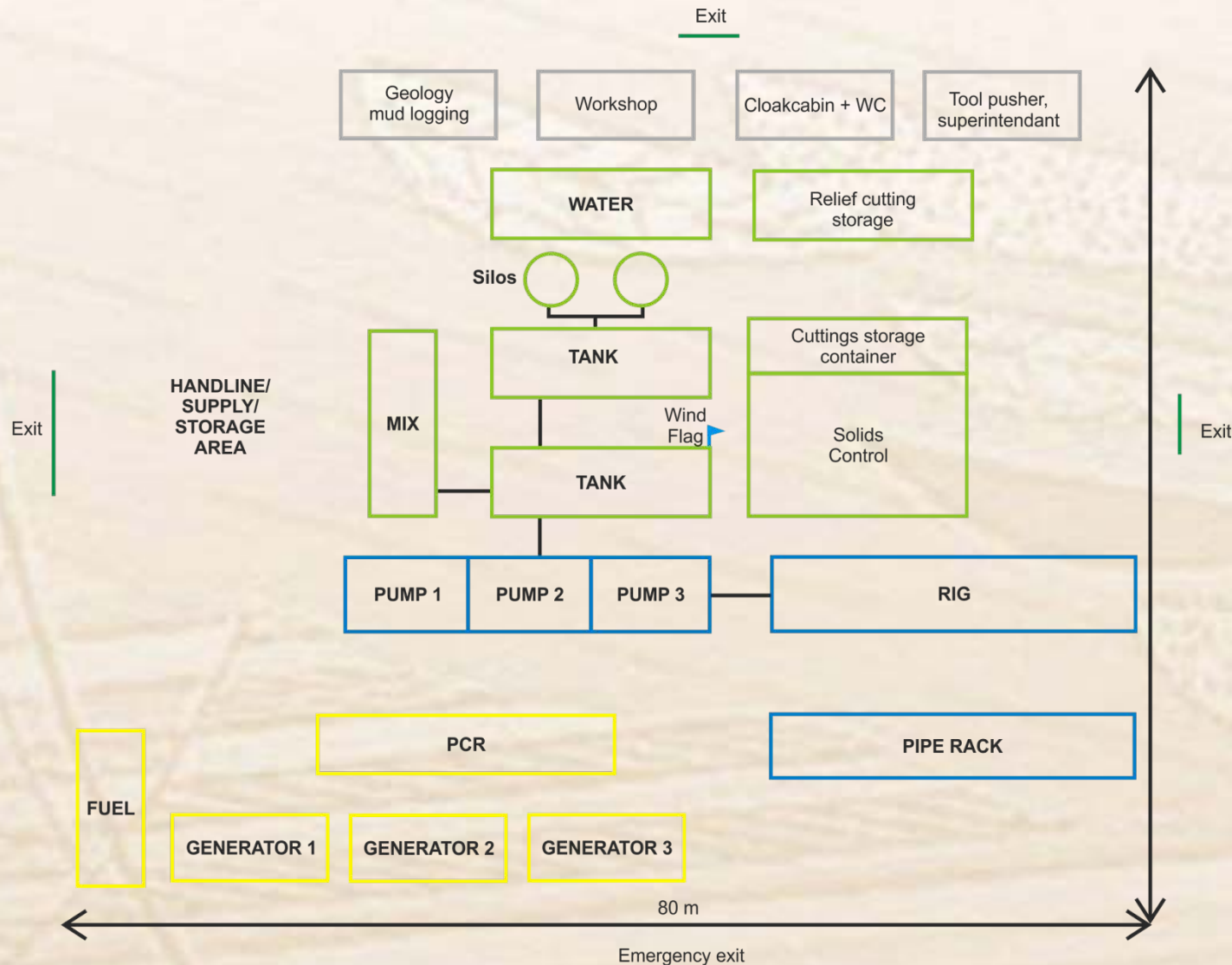


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# FOOT PRINT

## HEAVY DUTY (200-300 T) RIG AND EQUIPMENTS

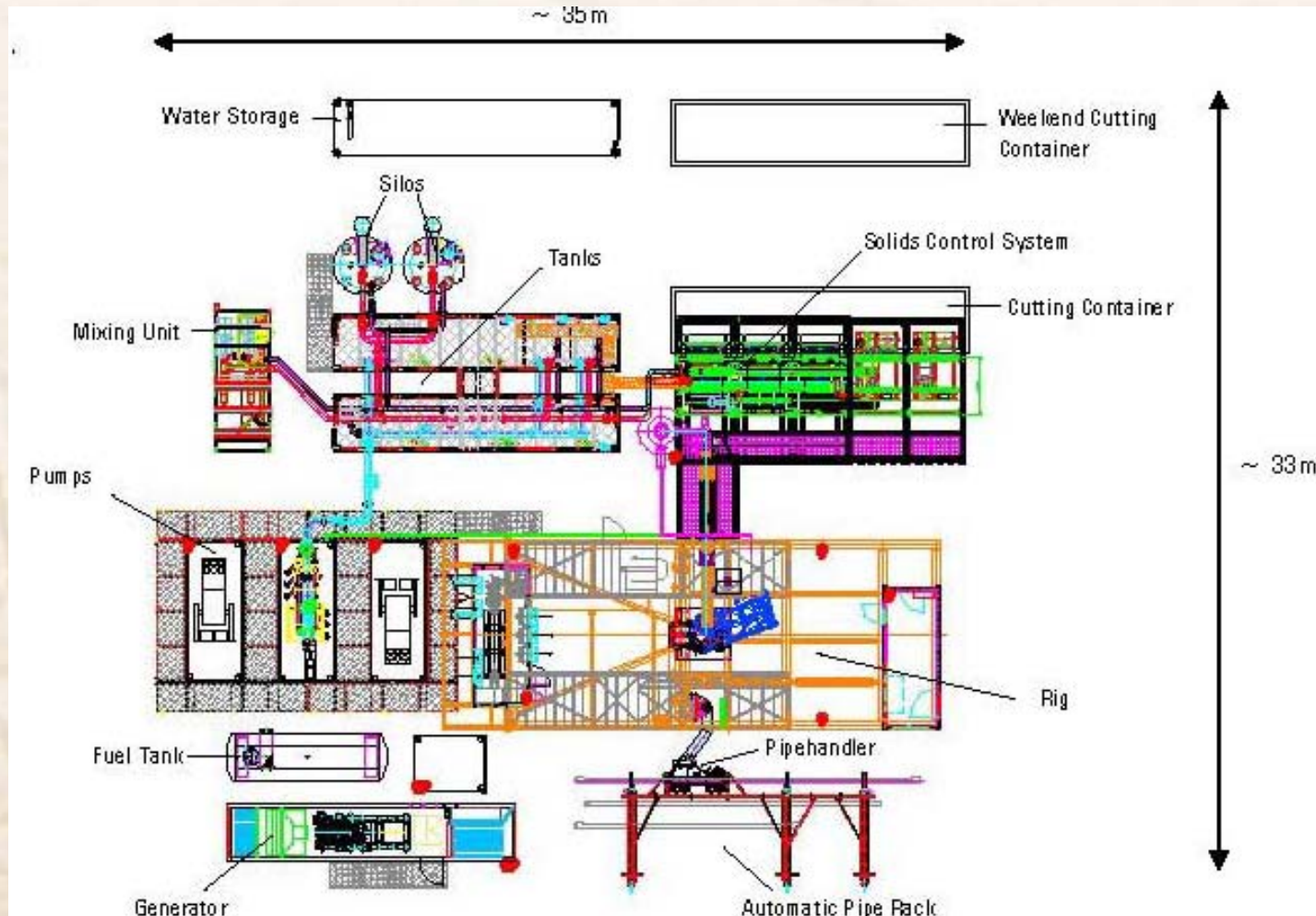








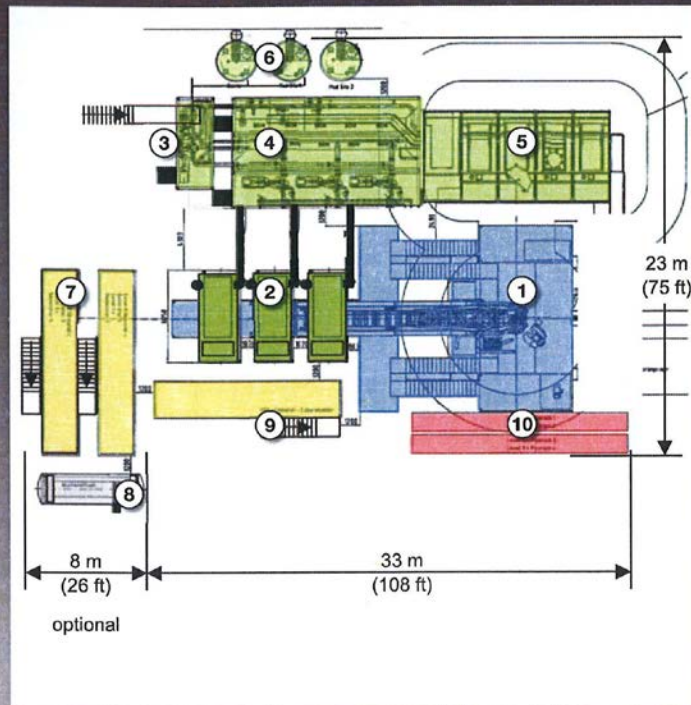
# FOOT PRINT HEAVY DUTY RIG



SOURCE : DRILLTEC



# NOVEL COMPACT HYDRAULIC RIG FOOT PRINT



## FOOTPRINT 23 m x 33 m

- |   |                        |    |   |
|---|------------------------|----|---|
| 1 | TBA 300                | 6  | Additional tanks (barite, storage) (optional) |
| 2 | Mud pumps (3 x 900 kW) | 7  | Generators (4 x 1 MW) (optional)              |
| 3 | Mixing station         | 8  | Diesel tank                                   |
| 4 | Mud tanks unit         | 9  | VFD unit                                      |
| 5 | Recycling unit         | 10 | Pipe handling                                 |

Source : BAUER



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# DEEP WELL DRILLING

## DRILLING/COMPLETION SEQUENCE



ITEM	PHASE	DC	CUS
1	Site preparation/rehabilitation		X
2	Move in/out ; rig-up/down	X	
3	Drilling	X	
4	Bits	X	
5	Drilling fluids	X	
6	Directional drilling	X	
7	Coring	X	
8	Logging		X
9	Casing, lining		X
10	Cementing	X	
11	Fishing	X	
12	Testing, sampling		X
13	Wellheads		X
14	Waste disposal/processing	X	
15	Engineering/supervision/reporting		X
16	Insurance		X
17	Contingencies		X

DC : drilling contractor

CUS : customer



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**IADC ROLLER BIT CLASSIFICATION TABLE**  
(IADC/SPE 23937, February, 1992)

Formations		Series	Types	Standard roller bearing	Roller bearing air-cooled	Roller bearing gage protected	Sealed roller bearing	Sealed roller bearing gage protected	Sealed friction bearing	Sealed friction bearing gage protected	Features Available
				1	2	3	4	5	6	7	
Steel tooth bits	Soft formations with low compressive strength and high drillability	1	1								A Air application
			2								B Special bearing seal
			3								C Center jet
			4								D Deviation control
	Medium to medium hard formations with high compressive strength	2	1								E Extended jets (full length)
			2								G Gage/body protection (additional)
			3								H Horizontal/steering applications
			4								J Jet deflection
	Hard semi-abrasive and abrasive formations	3	1								L Lug pads
			2								M Motor application
			3								S Standard steel tooth model
			4								T Two cone bit
Insert bits	Soft formations with low compressive strength and high drillability	4	1								W Enhanced cutting structure
			2								X Predominantly chisel tooth insert
			3								Y Conical tooth insert
			4								Z Other shape insert
	Soft to medium soft formations with low compressive strength	5	1								
			2								
			3								
			4								
	Medium hard formations with high compressive strength	6	1								
			2								
			3								
			4								
	Hard semi-abrasive and abrasive formations	7	1								
			2								
			3								
			4								
	Extremely hard and abrasive formations	8	1								
			2								
			3								
			4								



# BITS

## DRILLING BIT CASING COMPATIBILITIES



			Well profile
Phase	Hole (bit)	Casing	
Conductor pipe	30"	26"	
Technical casing	24"	18"5/8	
Pumping chamber	17"1/2	13"3/8	
Production casing	12"1/4	9"5/8	
Open hole	8"1/2		



# BITS



## THREADS AND MAKE-UP TORQUES FOR DRILL BITS AND CORING BITS (API RP 7G, January 1, 1995 – API Spec 7, April 1, 1994)

### Rock bits

Bit size (in)	Bit thread	Bit thread	Make-up torque	
			(daN.m)	(ft.lb)
3 3/4 – 4 1/2	2 3/8 REG	2 3/8 REG	400 – 480	3 000 – 3 500
4 5/8 – 5	2 7/8 REG	2 7/8 REG	600 – 750	4 500 – 5 500
5 1/8 – 7 3/8	3 1/2 REG	3 1/2 REG	950 – 1 200	7 000 – 9 000
7 1/2 – 9 3/8	4 1/2 REG	4 1/2 REG	1 600 – 2 200	12 000 – 16 000
9 1/2 – 14 3/8	6 5/8 REG	6 5/8 REG	3 800 – 4 300	28 000 – 32 000
14 1/2 – 18 1/2	6 5/8 or 7 5/8 REG	7 5/8 REG	4 600 – 5 400	34 000 – 40 000
18 5/8 to 26	7 5/8 or 8 5/8 REG	8 5/8 REG	5 400 – 8 100	40 000 – 60 000
27 and larger	8 5/8 REG			

### Diamond and PDC bits

Bit size (in)	Bit thread identification	Maximum pin ID (in)	Bit sub OD (in)	Minimum make-up torque (1)	
				(daN.m)	(ft.lb)
3 11/16 – 4 1/2	2 3/8 REG	1	3	243	1 791
			3 1/8	328	2 419
			3 1/4	418	3 085
4 17/32 – 5	2 7/8 REG	1 1/4	3 1/2	417	3 078
			3 3/4	626	4 617
			3 7/8	632	4 658
5 1/32 – 7 3/8	3 1/2 REG	1 1/2	4 1/8	701	5 171
			4 1/4	855	6 306
			4 1/2	1 039	7 660
7 13/32 – 9 3/8	4 1/2 REG	2 1/4	5 1/2	1 688	12 451
			5 3/4	2 234	16 476
			6	2 380	17 551
			6 1/4	2 408	17 757
9 13/32 – 14 1/2	6 5/8 REG	3 1/4	7 1/2	5 030	37 100
			7 3/4	5 133	37 857
			8	5 178	38 193
			8 1/4	5 224	38 527
14 9/16 – 18 1/2	7 5/8 REG	3 3/4	8 1/2	6 548	48 296
			8 3/4	7 824	57 704
			9	8 130	59 966
			9 1/4	8 200	60 480
			9 1/2	8 256	60 895

(1) Normal torque range is tabulated value plus 10%.

### Coring bits

Core barrel size (in)	Make-up torque	
	(daN.m)	(ft.lb)
4 1/8	400 – 490	3 000 – 3 600
4 1/2	680 – 800	5 000 – 6 000
4 3/4	550 – 660	4 050 – 4 850
5 3/4	1 000 – 1 190	7 400 – 8 800
6 1/4 × 3	2 020 – 2 410	14 900 – 17 800
6 1/4 × 4	1 100 – 1 330	8 150 – 9 800
6 3/4	1 340 – 1 630	9 900 – 12 000
8	2 580 – 3 080	19 000 – 22 700



# OUTLINE



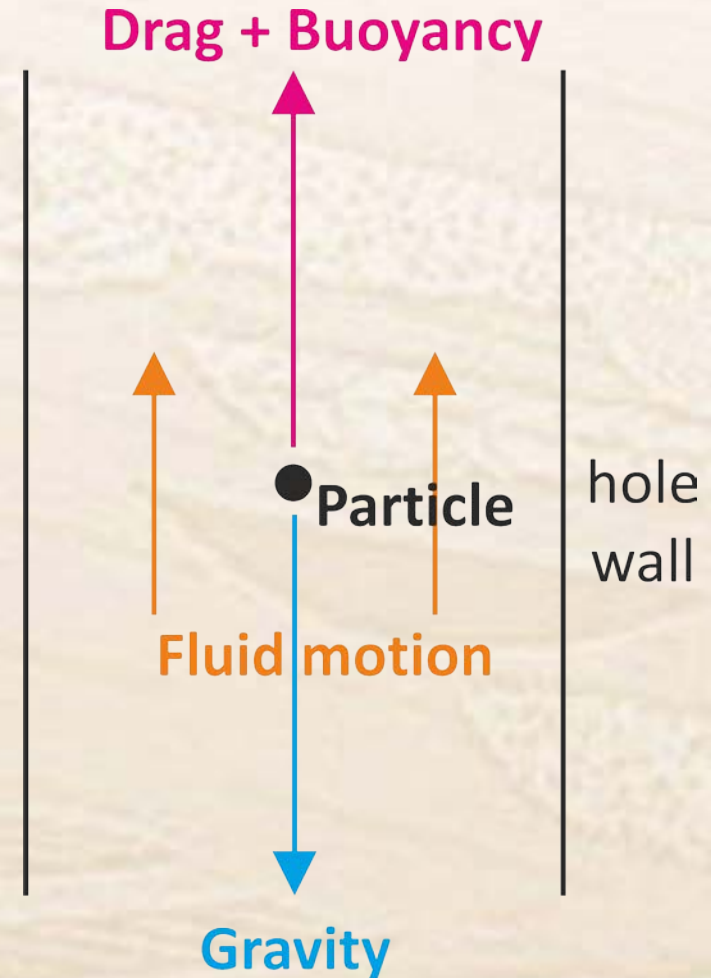
- SCOPE
- INTRODUCTION. GEOTHERMAL VS PETROLEUM
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  - Rig selection
  - Site preparation. Rig footprint
  - Drilling
  - Bits
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  - Dual completion
  - Fiberglass lined anti-corrosion well
  - (sub)Horizontal well concept
- MISCELLANEOUS ISSUES
  - Water injection
  - Mining risk insurance
  - Sustainability
  - Environment
  - Workover
  - Screens
  - Mud solids'control
- DRILLING CONTRACT. RIG MANAGEMENT. WORK SUPERVISION



# DRILLING FLUIDS



- Functions
- Properties/Rheology
- Balanced, under/over balanced
- Lost circulation
- Typical programmes
- Mud quarter equipment



**FORCES INVOLVED**



# DRILLING FLUID FUNCTIONS



- Remove cuttings from Bit
- Recover cuttings at surface
- Cooling, lubrication of Bit and Drill String
- Hole & Formation Cooling
- Wall cake
- Lost circulation control
- Secure reservoir integrity



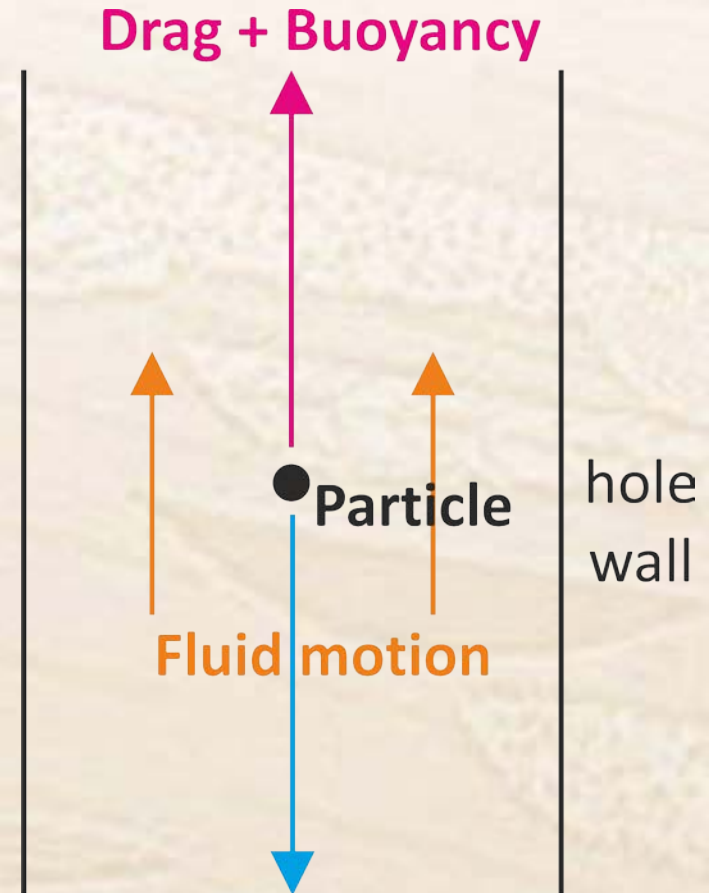
# DRILLING FLUID PROPERTIES



- Cuttings Removal
  - Factors involved
  - Fluid rheology
  - Velocity, viscosity, density
  - Particle (cuttings, chips, scale debris)
  - Size, shape, density
- Forces involved
  - **Downwards** = gravity \* particle mass
  - Upwards = drag + buoyancy
  - **Drag** (fluid velocity & viscosity; particle mass & wetted surface)
  - **Buoyancy** (fluid density \* particle displaced volume)

**Slip velocity threshold**

**Gravity force = Drag force + buoyancy**



**FORCES INVOLVED**





## ■ Limitations, Controls, Requirements

- Cuttings size & density not controlled
- Drilling fluid density partly controlled
- Drilling fluid velocity & viscosity controlled
- Fluid velocity requirement

— **Fluid velocity > Slip velocity**

### — **Exemple of typical fluid veolocties**

- Bentonite based mud # 35 m/min
- Water # 45 m/min





## ■ THIXOTROPY IS ESSENTIAL

- **Gel Strength**

- Newtonian fluid      viscosity changes with shear stress

- Non Newtonian fluid      viscosity varies with shear stress

- **Most drilling fluids and cement slurries are thixotropic**

- Stationary fluid      viscosity increases

- Non stationary fluid      viscosity decreases

- **Thixotropy allows to :**

- Keep solids in suspension when not circulating

- Release solids on shale shakers

- Build up a cake on hole wall





## ■ MUD FORMULAE

- **Water Based Bentonite**

Widely used because of its rheological properties

Eases solid removal from shakers, cyclone desanders/desilters

Adequate gelling and viscosifying properties (increasing with temperatures)

Recommended for overburden sections

- **Water Based (bio)Polymers**

Compulsory while drilling low enthalpy sensitive reservoir formations

Avoids plugging (particle invasion) damage

Environmentally friendly owing to its biodegradable nature

Adequate rheology

- **Water**

Recommended for drilling high enthalpy geothermal reservoirs and lost circulation zones. Requires high pumping rates and volumes. No cutting recovery.

- **Additives**

Thinners (viscosity, gel strength)

Lost circulation and cake control

Weighting materials (salt, barite)

LCM

Corrosion control

pH control

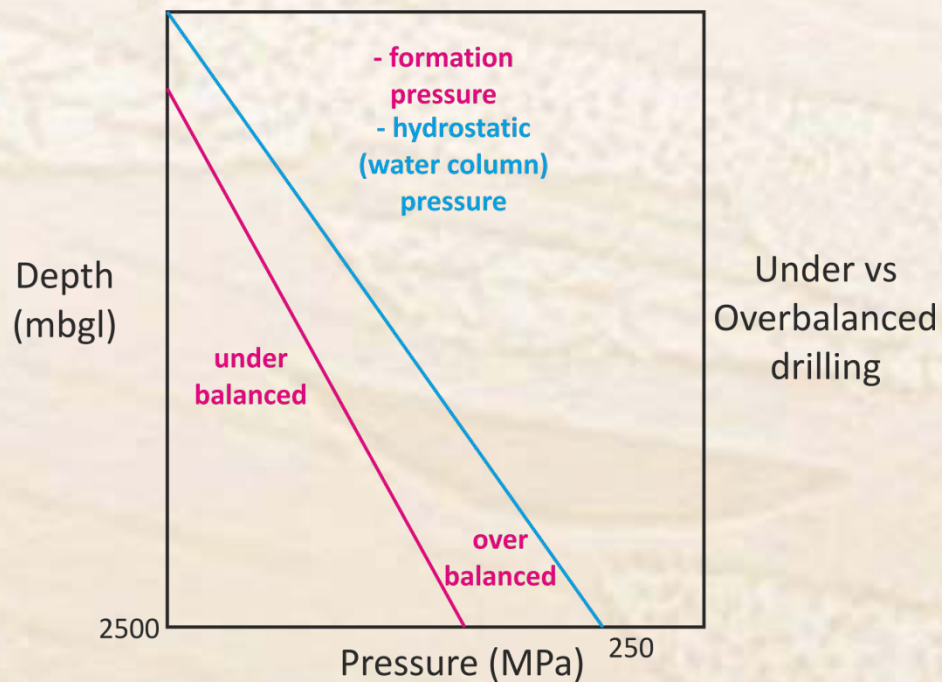
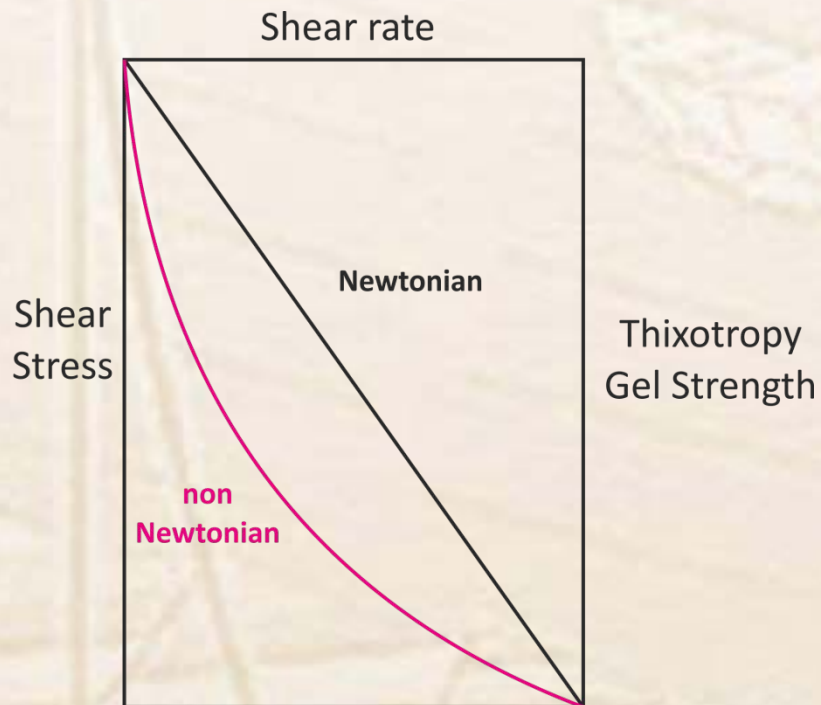
Polymers



# DRILLING FLUID PROPERTIES



## GRAPHICS







## ■ UNDER VS OVER BALANCED DRILLING

## ■ PROS AND CONS

- **Definition (see graphics slide)**

- Under balanced (under pressures)

— Formation pressure < drilling fluid hydrostatic pressure

- Over balanced

— Formation pressure > drilling fluid hydrostatic pressure

- **Pros and Cons**

Balancing	PROS	CONS
Under balanced	Fast penetration rate Formation integrity No lost circulation	Reservoir inflow Kick/blow out risk Formation collapse Stuck drill pipe
Over balanced	Safety (no inflow) Consolidated hole (thick cake) <sup>(*)</sup>	Lost circulation Mud filtrate loss (cake impact) Reduced penetration rate Differential pressure (stuck drill pipe)

*(\*) may be seen conversely at a disadvantage (reservoir plugging)*

- **Conclusion :**

keep as close as possible to balance drilling conditions unless otherwise dictated (blow out control)



# OUTLINE



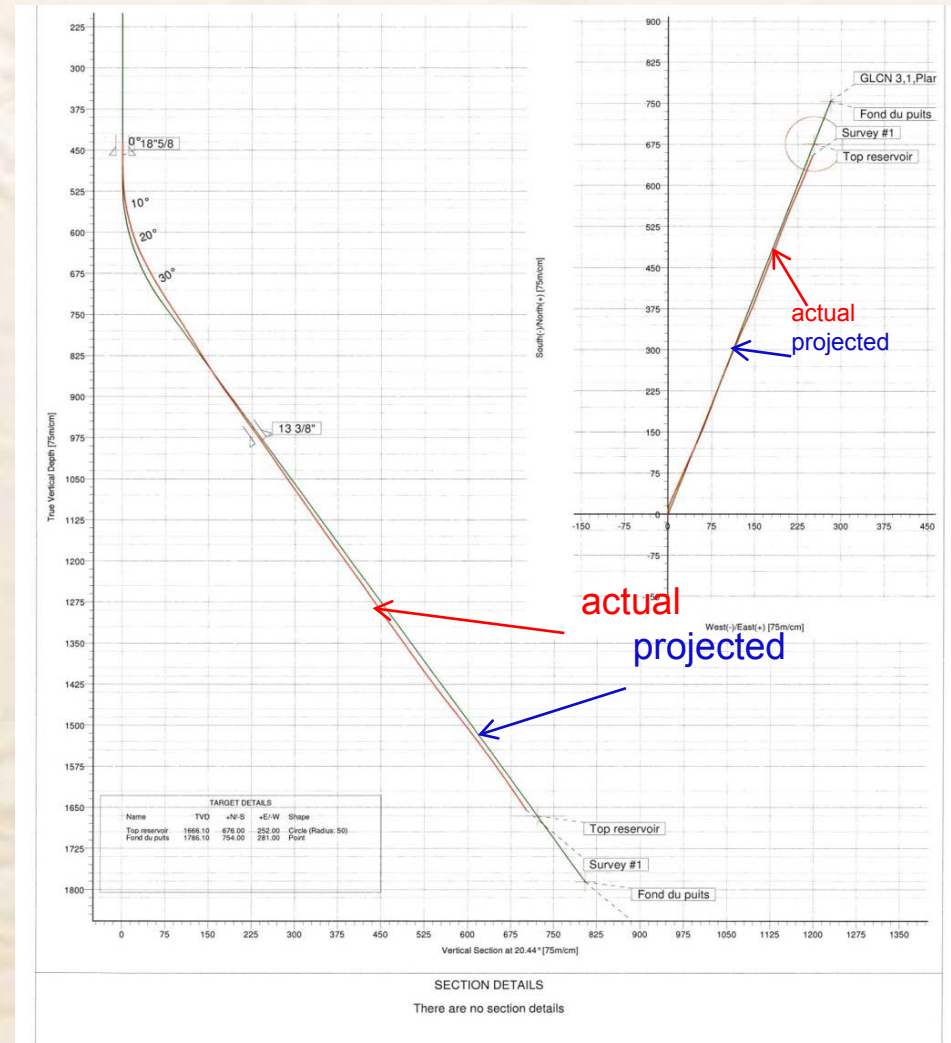
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# DIRECTIONAL DRILLING



- OBJECTIVES
- CLUSTERS
- CANDIDATE (J/S SHAPED) TRAJECTORIES
- PLANNING LIMITATIONS
- TYPICAL WELL PROFILES
- BHAs





# DIRECTIONAL DRILLING OBJECTIVES



- Adapt to site limitations and accessibility
- Terrain availability
- Optimum target matching from drill site
- Optimum well delivery by intersecting (near) vertical fractures
- Side tracking whenever needed
- Relief well(s)
- Cluster drilling
- Cost cuts



# DIRECTIONAL DRILLING CLUSTERS



- **ADVANTAGES**

- Multiwell array (f.i. GDH doublet) drilled from a single pad
- Easy and cheaper site preparation
- Cheaper land acquisition costs
- Reduced rig mob/demob costs
- Reduce well connection (f.i. GDH primary loop) costs
- Easier planning and operation

- **DISADVANTAGES**

- One way ticket strategy (redhibitory in case of exploration failure)



# DIRECTIONAL DRILLING TRAJECTORIES

## RADIUS OF CURVATURE



### RADIUS OF CURVATURE AND PROJECTION IN THE VERTICAL PLANE

$AE = L$  Length drilled from A to E

$R = \frac{360}{2\pi} \frac{\Delta L}{\Delta i}$  Radius of curvature (m)

$gbu = \frac{\Delta i}{\Delta L}$  Rate of buildup ( $^{\circ}/10$  m)

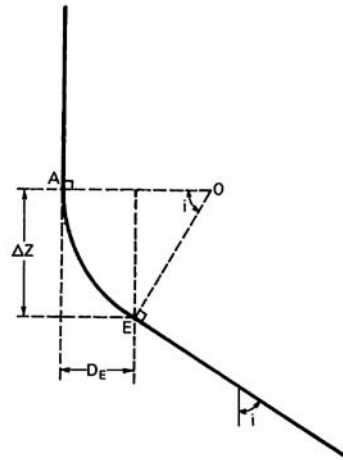
in general  $\frac{\Delta i}{\Delta L}$  is kept as constant as possible during kickoff (constant radius of curvature,

Hence:

$$R = \frac{573}{gbu}$$

$D_E = R(1 - \cos i)$  (m)

$\Delta Z = R \sin i$  (m)



Radius of curvature for different rates of buildup:

$gbu$ ( $^{\circ}/10$ m)	0.5	1.0	1.5	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0
$R$ (m)	1146	573	382	286	191	143	115	95	82	72	64	57

$m \times 3.28 = ft$   $^{\circ}/10 m \times 3.048 = ^{\circ}/100 ft$

Source : IFP/TECHNIP



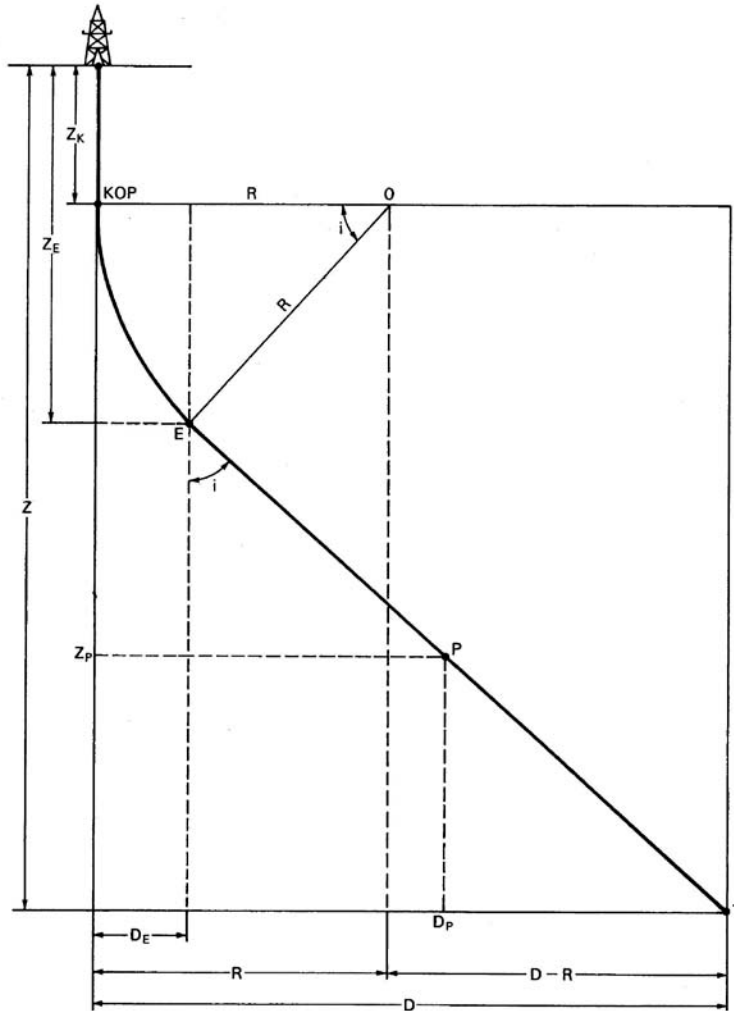
# DIRECTIONAL DRILLING TRAJECTORIES

## J SHAPED HOLE (1)



### CALCULATION OF CHARACTERISTIC POINTS OF THE THEORETICAL VERTICAL PROFILE

J hole:  $D > R$



	Measured depth $L$ (TMD)	Vertical depth $Z$ (TVD)	Inclination	Displacement
Kickoff point (K)	$Z_K$	$Z_K$	0	0
End of deviation (E)	$L_E = Z_K + \frac{\pi i R}{180}$	$Z_E = Z_K + R \sin i$	$i$	$D_E = R(1 - \cos i)$
Target (T)	$L_T = Z_K + \frac{\pi i R}{180} + \frac{Z - Z_K - R \sin i}{\cos i}$	$Z$	$i$	$D$

Vertical depth  $Z_P$  as a function of drilled depth  $L_P$  at point P:

$$Z_P = Z_K + \frac{573}{gbu} \sin i + \left( L_P - Z_K - \frac{10i}{gbu} \right) \cos i$$

Source : IFP/TECHNIP



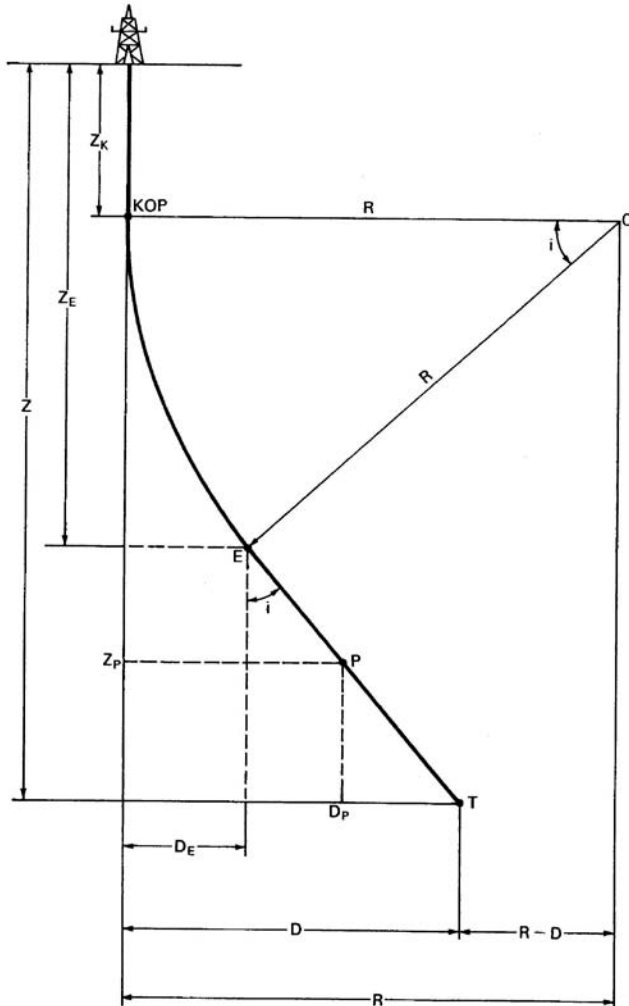
# DIRECTIONAL DRILLING TRAJECTORIES

## J SHAPED HOLE (2)



### CALCULATION OF CHARACTERISTIC POINTS OF THE THEORETICAL VERTICAL PROFILE

J hole:  $D < R$



	Measured depth $L$ (TMD)	Vertical depth $Z$ (TVD)	Inclination	Displacement
Kickoff point (K)	$Z_K$	$Z_K$	0	0
End of deviation (E)	$L_E = Z_K + \frac{\pi i R}{180}$	$Z_E = Z_K + R \sin i$	$i$	$D_E = R(1 - \cos i)$
Target (T)	$L_T = Z_K + \frac{\pi i R}{180} + \frac{Z - Z_K - R \sin i}{\cos i}$	$Z$	$i$	$D$

Vertical depth  $Z_P$  as a function of drilled depth  $L_P$  at point P:

$$Z_P = Z_K + \frac{573}{gbu} \sin i + \left( L_P - Z_K - \frac{10i}{gbu} \right) \cos i$$

Source : IFP/TECHNIP

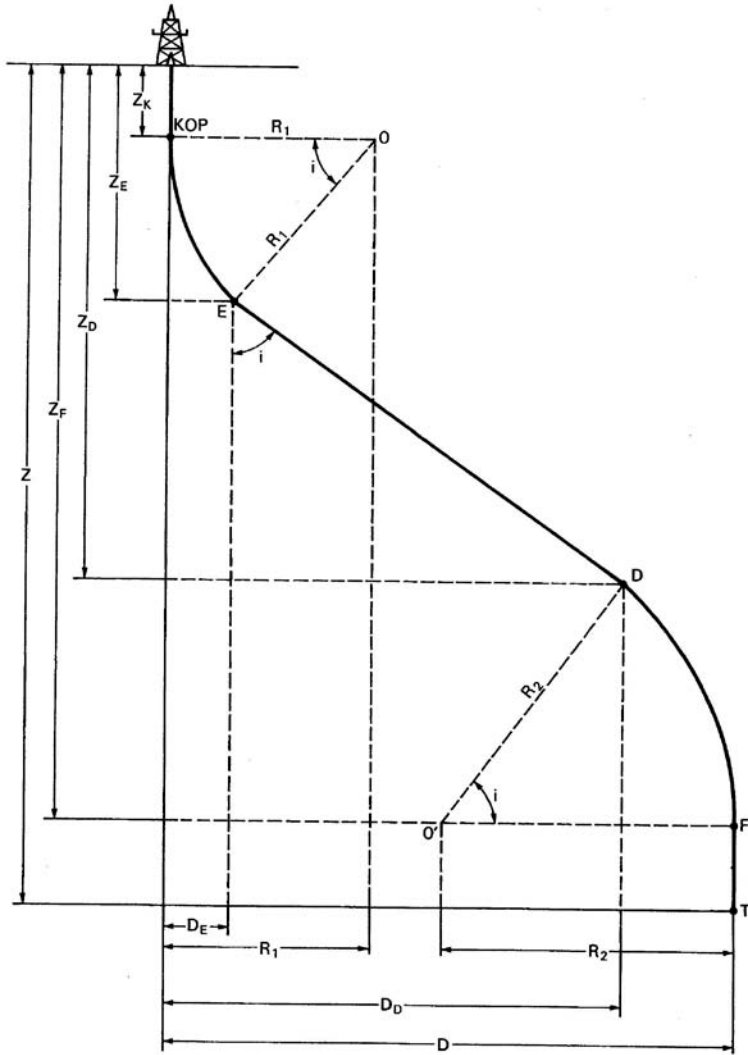


# DIRECTIONAL DRILLING TRAJECTORIES

## S SHAPED HOLE (1)



**S hole:  $R_1 + R_2 < D$**



**S hole:  $R_1 + R_2 < D$  (continued)**

Assuming a return of the well to the vertical at  $F$ , the inclination  $i$  depends on the depth selected for point  $F$ :

$$i = 180 - \tan^{-1} \left[ \frac{Z_F - Z_K}{D - R_1 - R_2} \right] - \cos^{-1} \left[ \frac{R_1 + R_2}{Z_F - Z_K} \sin \tan^{-1} \frac{Z_F - Z_K}{D - R_1 - R_2} \right]$$

The remaining calculations are identical to those in J 5 and J 7 up to  $D$  ( $Z_D$ ,  $D_D$ ).

Vertical projection at  $D$ :

$$Z_D = Z_F - R_2 \sin i$$

Measured depth at  $D$ :

$$L_D = Z_K + \frac{\pi i R_1}{180} + \frac{Z_D - Z_K - R_1 \sin i}{\cos i}$$

Displacement at  $D$ :

$$D_D = R_1 (1 - \cos i) + (Z_D - Z_K - R_1 \sin i) \tan i$$

Measured depth at  $F$ :

$$L_F = L_D + \frac{\pi i R_2}{180}$$

Total measured depth at  $T$ :

$$L_T = Z_K + \frac{\pi i R_1}{180} + \frac{Z_D - Z_K - R_1 \sin i}{\cos i} + \frac{\pi i R_2}{180} + Z - Z_F$$

Source : IFP/TECHNIP

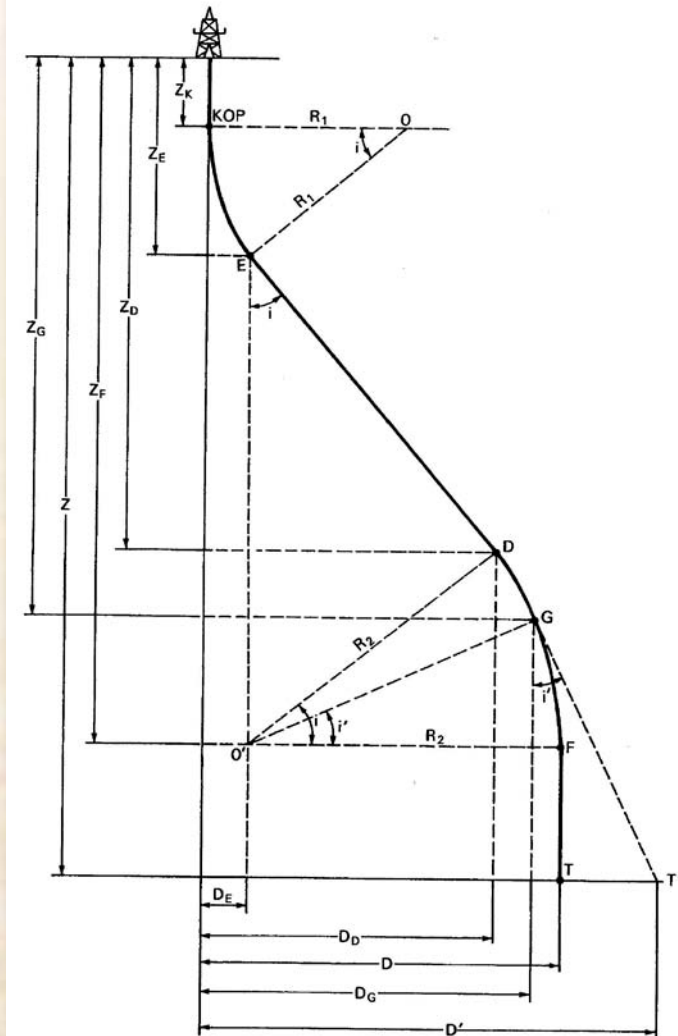


# DIRECTIONAL DRILLING TRAJECTORIES

## S SHAPED HOLE (2)



**S hole:  $R_1 + R_2 > D$**



**S hole:  $R_1 + R_2 > D$  (continued)**

Assuming a return of the well to the vertical at  $F$ , the inclination  $i$  depends on the depth selected for point  $F$ :

$$i = \tan^{-1} \left[ \frac{Z_F - Z_K}{R_1 + R_2 - D} \right] - \cos^{-1} \left[ \frac{R_1 + R_2}{Z_F - Z_K} \sin \tan^{-1} \frac{Z_F - Z_K}{R_1 + R_2 - D} \right]$$

The remaining calculations are unchanged (see J 9).

If the well does not return to the vertical, the displacement at  $T'$  from point  $G$  becomes:

$$D' = D_G + (Z - Z_G) \tan i'$$

$$L_{T'} = L_G + \frac{(Z - Z_G)}{\cos i'}$$

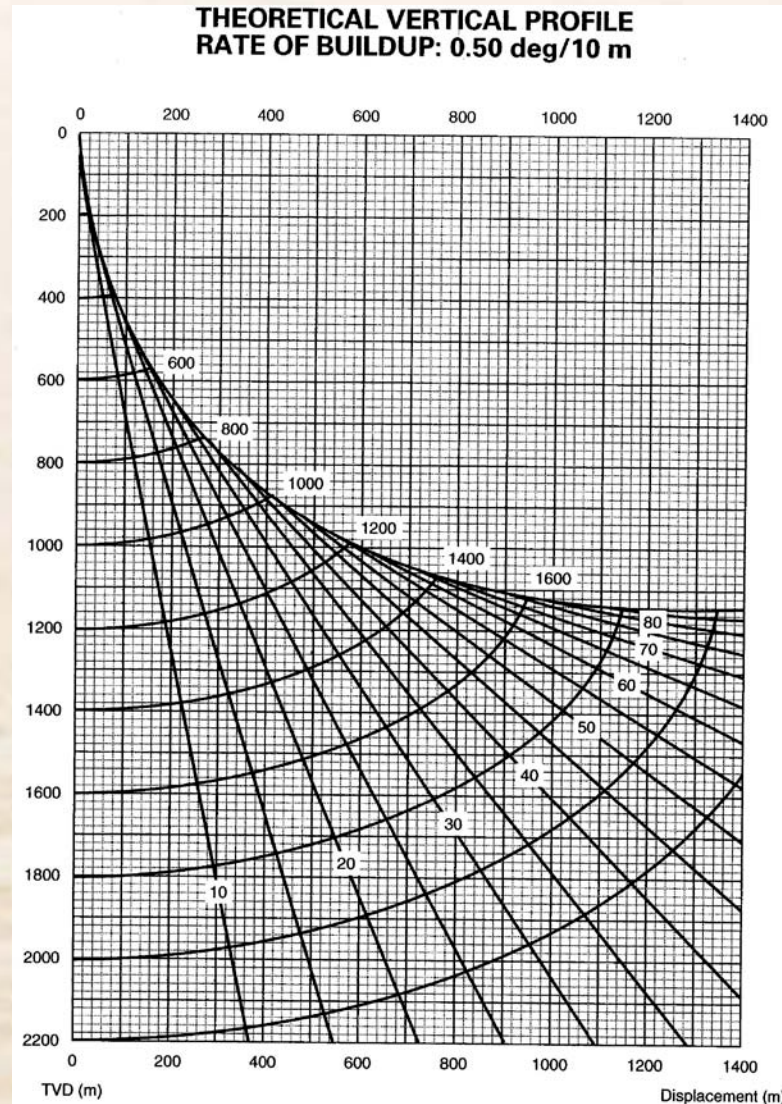
Source : IFP/TECHNIP



# DIRECTIONAL DRILLING TRAJECTORIES DISPLACEMENT VS DEPTH AND INCLINATION



Build up rate = 10/10 m



Source : IFP/TECHNIP



# DIRECTIONAL DRILLING SURVEY REPORT



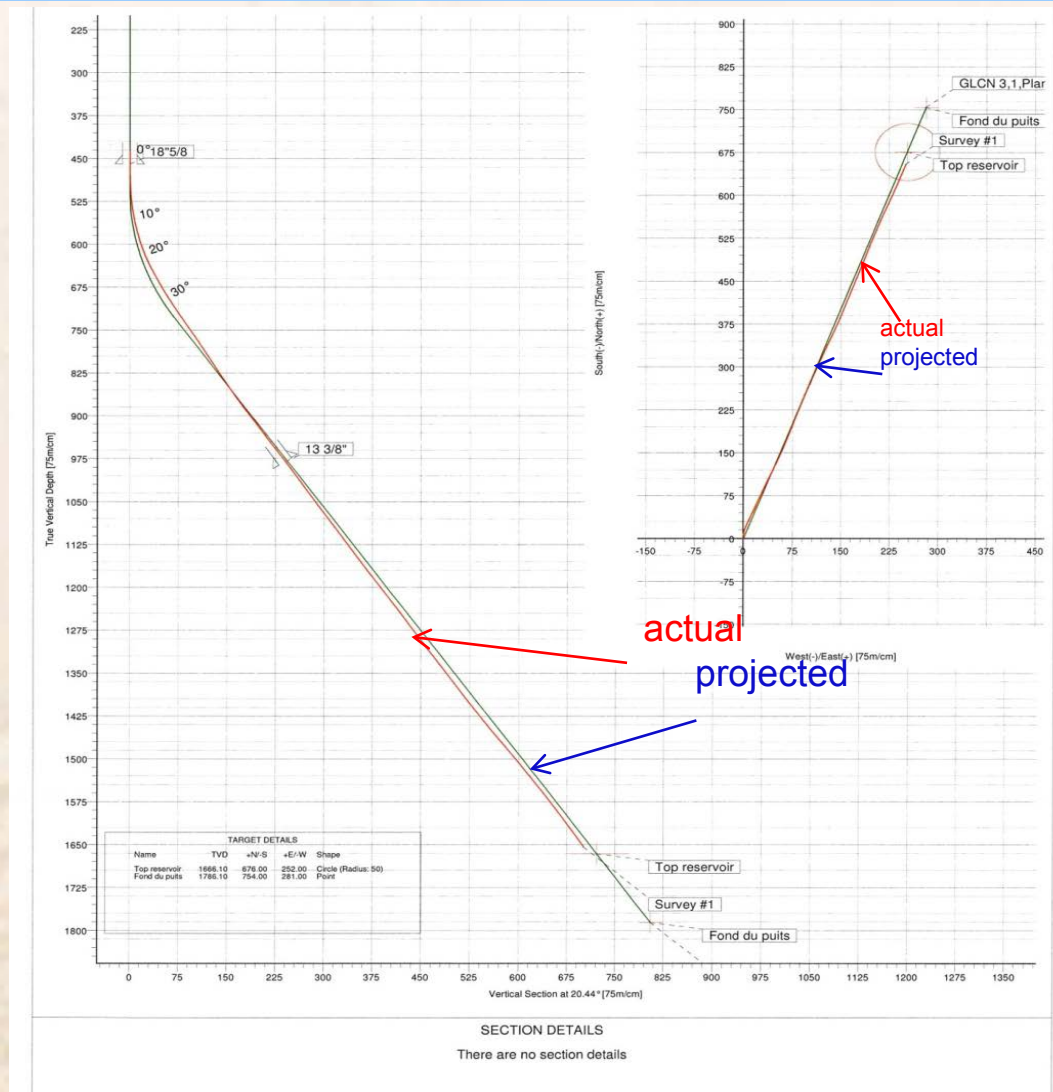
<b>Company:</b> GPC / SMP	<b>Date:</b> 9/26/2011	<b>Time:</b> 08:37:53	<b>Page:</b> 2
<b>Field:</b> Bassin Parisien	<b>Co-ordinate(NE) Reference:</b>	<b>Well:</b> GLCN 3, Grid North	
<b>Site:</b> GLCN	<b>Vertical (TVD) Reference:</b>	<b>SITE</b> 43.1	
<b>Well:</b> GLCN 3	<b>Section (VS) Reference:</b>	<b>Well</b> (0.00N,0.00E,20.44Azi)	
<b>Wellpath:</b> 1	<b>Survey Calculation Method:</b>	<b>Minimum Curvature</b>	<b>Db:</b> Sybase

## Survey: Survey #1

MD m	Incl deg	Azim deg	TVD m	+N/-S m	+E/-W m	VS m	DLS deg/30m	Bulld deg/30m	Turn deg/30m	Tool/Comment
669.00	26.81	22.73	662.13	41.08	11.73	42.59	1.258	0.833	2.100	EM MWD
679.00	26.81	22.48	671.06	45.24	13.46	47.09	0.338	0.000	-0.750	EM MWD
688.00	27.69	22.60	679.06	49.05	15.04	51.21	2.939	2.933	0.400	EM MWD
698.00	28.81	22.23	687.87	53.42	16.85	55.94	3.401	3.360	-1.110	EM MWD
707.00	30.22	21.98	695.70	57.53	18.51	60.37	4.718	4.700	-0.833	EM MWD
716.00	30.94	22.23	703.45	61.77	20.24	64.95	2.437	2.400	0.833	EM MWD
725.00	30.69	21.60	711.18	66.05	21.96	69.56	1.361	-0.833	-2.100	EM MWD
735.00	30.81	22.48	719.77	70.79	23.88	74.67	1.397	0.360	2.640	EM MWD
745.00	31.81	22.73	728.31	75.59	25.87	79.86	3.025	3.000	0.750	EM MWD
754.00	32.25	22.35	735.94	79.99	27.70	84.63	1.613	1.467	-1.267	EM MWD
763.00	32.38	22.35	743.55	84.44	29.53	89.44	0.433	0.433	0.000	EM MWD
773.00	31.44	22.98	752.04	89.32	31.57	94.72	2.992	-2.820	1.890	EM MWD
782.00	31.06	23.23	759.73	93.62	33.40	99.39	1.338	-1.267	0.833	EM MWD
792.00	30.75	23.35	768.31	98.33	35.43	104.52	0.948	-0.930	0.360	EM MWD
802.00	30.56	23.48	776.92	103.01	37.46	109.61	0.604	-0.570	0.390	EM MWD
811.00	30.88	22.35	784.65	107.25	39.25	114.20	2.200	1.067	-3.767	EM MWD
821.00	31.38	22.98	793.21	112.02	41.24	119.37	1.790	1.500	1.890	EM MWD
830.00	31.06	23.23	800.91	116.31	43.07	124.03	1.151	-1.067	0.833	EM MWD
840.00	30.31	23.73	809.51	120.99	45.10	129.12	2.377	-2.250	1.500	EM MWD
849.00	30.38	23.48	817.28	125.16	46.92	133.66	0.481	0.233	-0.833	EM MWD
859.00	30.94	22.48	825.88	129.85	48.92	138.76	2.272	1.680	-3.000	EM MWD
869.00	31.50	22.35	834.43	134.64	50.89	143.94	1.692	1.680	-0.390	EM MWD
878.00	31.06	21.85	842.12	138.97	52.65	148.61	1.703	-1.467	-1.667	EM MWD
888.00	31.31	22.48	850.68	143.77	54.60	153.78	1.233	0.750	1.890	EM MWD
897.00	31.94	21.98	858.34	148.14	56.39	158.50	2.275	2.100	-1.667	EM MWD
907.00	32.69	20.60	866.79	153.12	58.33	163.85	3.156	2.250	-4.140	EM MWD
916.00	33.06	20.60	874.35	157.69	60.05	168.73	1.233	1.233	0.000	EM MWD
928.00	33.50	20.73	884.38	163.85	62.37	175.32	1.114	1.100	0.325	EM MWD
938.00	34.00	20.10	892.70	169.06	64.31	180.87	1.831	1.500	-1.890	EM MWD
947.00	34.44	20.35	900.14	173.81	66.06	185.93	1.540	1.467	0.833	EM MWD
957.00	34.06	20.60	908.41	179.08	68.03	191.56	1.216	-1.140	0.750	EM MWD
966.00	33.25	20.10	915.90	183.75	69.76	196.55	2.854	-2.700	-1.667	EM MWD
975.00	33.13	19.35	923.43	188.39	71.43	201.47	1.426	-0.400	-2.500	EM MWD
985.00	33.38	19.10	931.79	193.57	73.23	206.96	0.855	0.750	-0.750	EM MWD
995.00	34.13	18.23	940.11	198.83	75.01	212.51	2.677	2.250	-2.610	EM MWD
1004.00	34.81	19.23	947.53	203.66	76.64	217.60	2.949	2.267	3.333	EM MWD
1014.00	34.62	19.19	955.75	209.04	78.52	223.30	0.574	-0.570	-0.120	EM MWD
1024.00	34.44	19.98	963.98	214.38	80.42	228.96	1.448	-0.540	2.370	EM MWD
1034.00	34.35	19.67	972.24	219.69	82.33	234.61	0.591	-0.270	-0.930	EM MWD
1064.00	33.13	20.60	997.18	235.34	88.07	251.27	1.325	-1.220	0.930	EM MWD
1074.00	32.94	20.60	1005.57	240.44	89.99	256.73	0.570	-0.570	0.000	EM MWD
1083.00	32.94	20.35	1013.12	245.02	91.70	261.62	0.453	0.000	-0.833	EM MWD
1092.00	33.18	20.74	1020.66	249.62	93.42	266.53	1.069	0.800	1.300	EM MWD
1102.00	33.44	20.85	1029.02	254.75	95.37	272.02	0.801	0.780	0.330	EM MWD
1111.00	33.38	21.23	1036.53	259.38	97.15	276.98	0.726	-0.200	1.267	EM MWD
1121.00	33.25	21.35	1044.89	264.50	99.14	282.47	0.437	-0.390	0.360	EM MWD
1130.00	33.31	22.10	1052.41	269.08	100.97	287.40	1.386	0.200	2.500	EM MWD
1141.00	33.81	21.48	1061.58	274.73	103.23	293.48	1.653	1.364	-1.691	EM MWD
1150.00	33.69	20.73	1069.06	279.40	105.03	298.48	1.445	-0.400	-2.500	EM MWD
1160.00	33.69	21.10	1077.38	284.58	107.01	304.03	0.616	0.000	1.110	EM MWD
1169.00	33.75	21.23	1084.87	289.24	108.81	309.03	0.313	0.200	0.433	EM MWD
1179.00	34.19	21.10	1093.16	294.45	110.83	314.61	1.338	1.320	-0.390	EM MWD
1188.00	34.06	21.60	1100.61	299.15	112.67	319.66	1.031	-0.433	1.667	EM MWD



# DIRECTIONAL DRILLING TYPICAL DEVIATED WELL PROFILES TRAJECTORIES DISPLAYS







# DIRECTIONAL DRILLING BHAS

## DIRECTIONAL DRILLING BHAS



Directional drilling  
(drill bit 17"1/2)



Directional drilling  
(PDC bit 12"1/4)

Directional drilling (drill bit 17"1/2)	Directional drilling (PDC bit 12"1/4)
Drill bit 17"1/2	PDC bit 12"1/4
Motor pump	Motor pump
Float sub	MWD tool carrier
Measurement while drilling (MWD) tool carrier	MWD emitting sub
MWD emitting sub	NMDC 9"1/2
Non magnetic drill collars (NMDC) 9"1/2	2 x DC 8 "1/4
2 x Drill collars (DC) 8 "1/4	8 x DC 6"3/4
9 x DC 6"3/4	4 x HWDP 5"
4 x Heavy weight drill pipe (HWDP) 5"	Hydraulic jar
Hydraulic jar	9 x HWDP 5"
9 x HWDP 5"	DP 5"
Drill pipes (DP) 5"	



# DIRECTIONAL DRILLING DOWNHOLE MOTORS

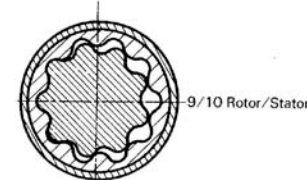
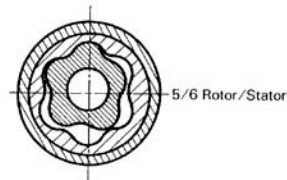
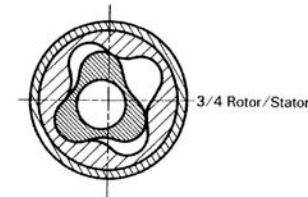
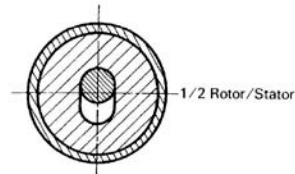


## POSITIVE DISPLACEMENT MOTORS

### I SPECIFICATIONS OF POSITIVE DISPLACEMENT MOTORS

Positive displacement motors are identified by:

- (a) Outside diameter of the body
- (b) Ratio of the shaft lobes (rotor) to the sleeve (stator) which may vary from 1/2 to 9/10:



- (c) Number of stages
- (d) Length and weight.

The hydraulic characteristics are indicated by:

- (a) Minimum and maximum flow rates
- (b) Minimum and maximum rotary speeds
- (c) Maximum pressure drop across the motor
- (d) Maximum torque supplied
- (e) Maximum mechanical horsepower output supplied
- (f) Maximum efficiency.

### II VARIATIONS IN SPECIFICATIONS

The specifications are given by the manufacturers for a specific gravity of 1.20 (10 ppg):

- The **rotary speed** is directly proportional to the flow rate:

$$N_2 = N_1 \frac{Q_2}{Q_1}$$

The higher the number of shaft lobes, the lower the rotary speed.

It varies only slightly with torque and pressure drop.



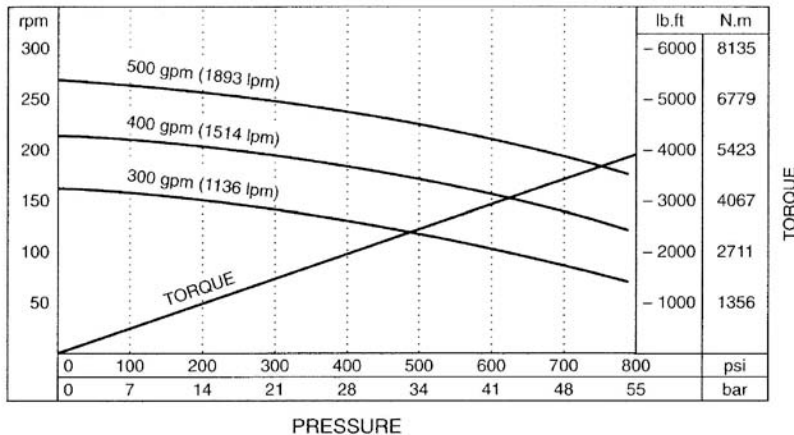
# DOWNHOLE MOTORS



## PERFORMANCE CURVES OF POSITIVE DISPLACEMENT MOTORS FOR DIFFERENT FLOW RATES $Q$

Example of a 6 3/4" – 4/5 lobe Performance Curves:

Motor start pressure 100 psi (7 bar)



## POSITIVE DISPLACEMENT MOTORS (continued)

- The **torque** is directly proportional to the pressure drop across the motor:

$$T_2 = T_1 \frac{\Delta p_2}{\Delta p_1}$$

- The **mechanical horsepower output** transmitted to the rotor is the product of the rotary speed multiplied by the torque:

$$P_m = \frac{TN}{9550}$$

- The **hydraulic horsepower** is the product of the pressure drop multiplied by the flow rate:

$$P_h = \frac{\Delta p Q}{60\,000}$$

where:

$T$  = torque (in N.m)

$N$  = rotary speed (in rpm)

$\Delta p$  = pressure drop in the motor (in kPa)

$Q$  = mud flow rate (in l/min)

$P_h$  = hydraulic horsepower (in kW)

$P_m$  = mechanical horsepower output at rotor (in kW)



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  - Drilling fluids
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  - (sub)Horizontal well concept
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  - Water injection
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  - Mud solids'control
- DRILLING CONTRACT. RIG MANAGEMENT. WORK SUPERVISION



# CASING LINING

## CASING CHARACTERISTICS



Diameter (OD)"	Nominal Weight (lb/ft)	Wall thickness (mm)
4 <sup>1/2</sup>	9.5-15.10	5.20-8.56
5 (1)	11.5-24.10	5.59-12.70
5 <sup>1/2</sup>	14-43.10	6.20-22.22
6 <sup>5/8</sup>	20-32	7.32-12.06
<b>7</b>	<b>17-57.10</b>	<b>5.87-22.22</b>
7 <sup>5/8</sup> (2)	24-55.30	7.62-19.05
8 <sup>5/8</sup>	24-49	6.71-14.15
<b>9<sup>5/8</sup></b>	<b>32.30-75.60</b>	<b>7.92-20.24</b>
10 <sup>3/4</sup> (3)	32.75-85.30	7.09-20.24
11 <sup>3/4</sup>	42-71	8.46-14.78
<b>13<sup>3/8</sup></b>	<b>48-72</b>	<b>8.38-13.06</b>
16	65-109	9.53-16.66
<b>18<sup>5/8</sup></b>	<b>87.50</b>	<b>11.05</b>
20	94-133	11.13-16.13

(1) Lining of damaged 7" csg

(2) Lining of damaged 9<sup>5/8</sup> csg

(3) Lining of damaged 13<sup>3/8</sup> csg





# CASING/LINING

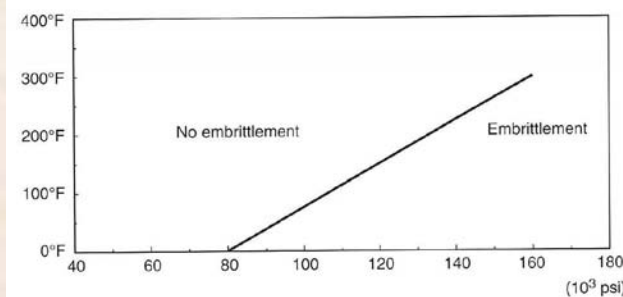
## Standard steel strength

Grade	Yield strength				Tensile strength		Hardness
	Minimum		Maximum		Minimum		Maximum
	psi	MPa	psi	MPa	psi	MPa	HRC
C75	75,000	517	90,000	620	95,000	655	22
L80	80,000	552	95,000	655	95,000	655	23
C90	90,000	620	105,000	724	100,000	690	25.4
C95	95,000	655	110,000	758	105,000	723	

## High strength steels

Grade	Yield strength				Tensile strength	
	Minimum		Maximum		Minimum	
	psi	MPa	psi	MPa	psi	MPa
P105	105,000	724	135,000	931	120,000	827
P110	110,000	758	140,000	965	125,000	827
Q125	125,000	862	155,000	1069	135,000	931
V150	150,000	1034			160,000	1104

## H2S embrittlement

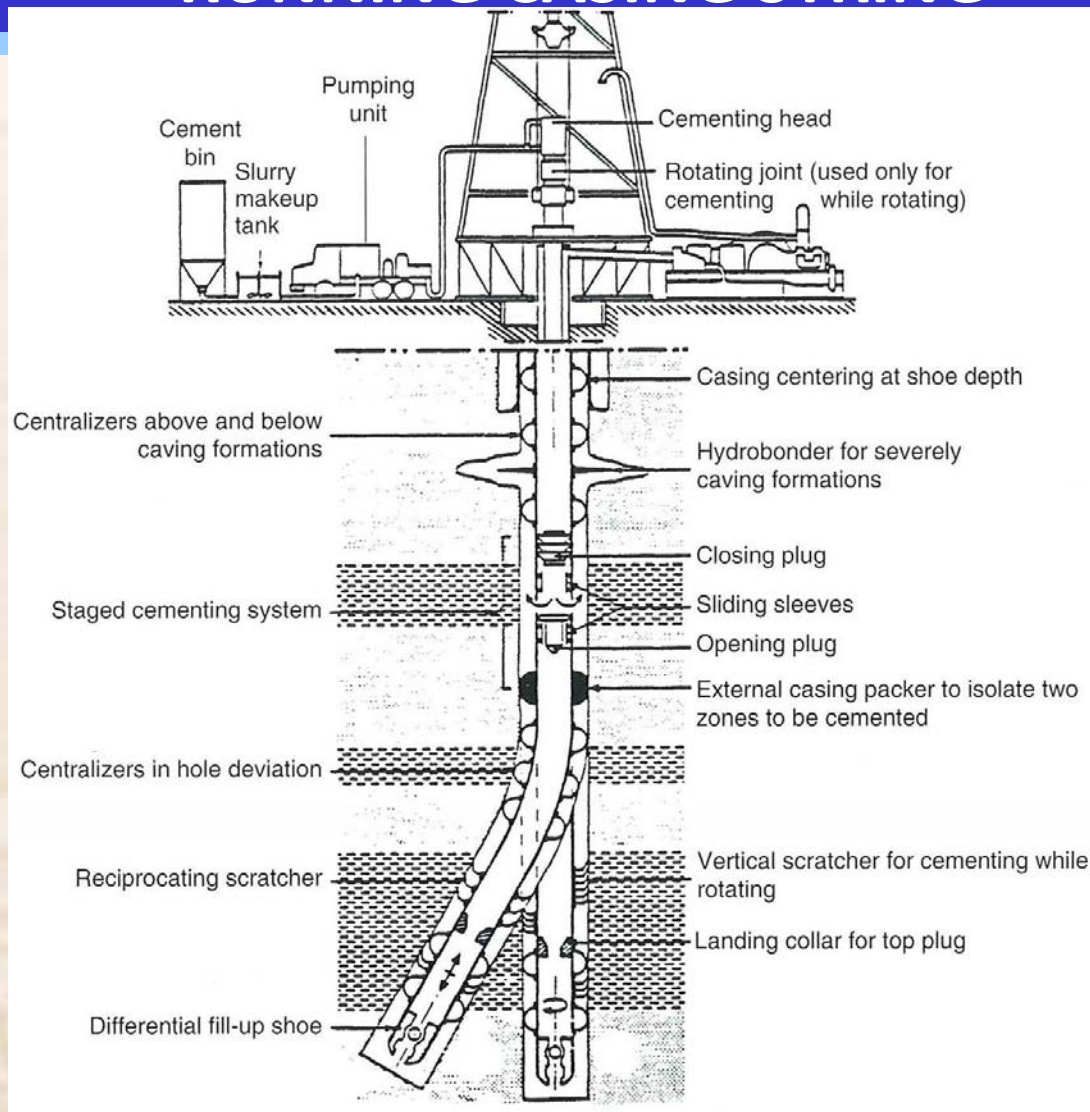


Source : J.P. NGUYEN



# CASING/LINING

## RUNNING CASING STRING



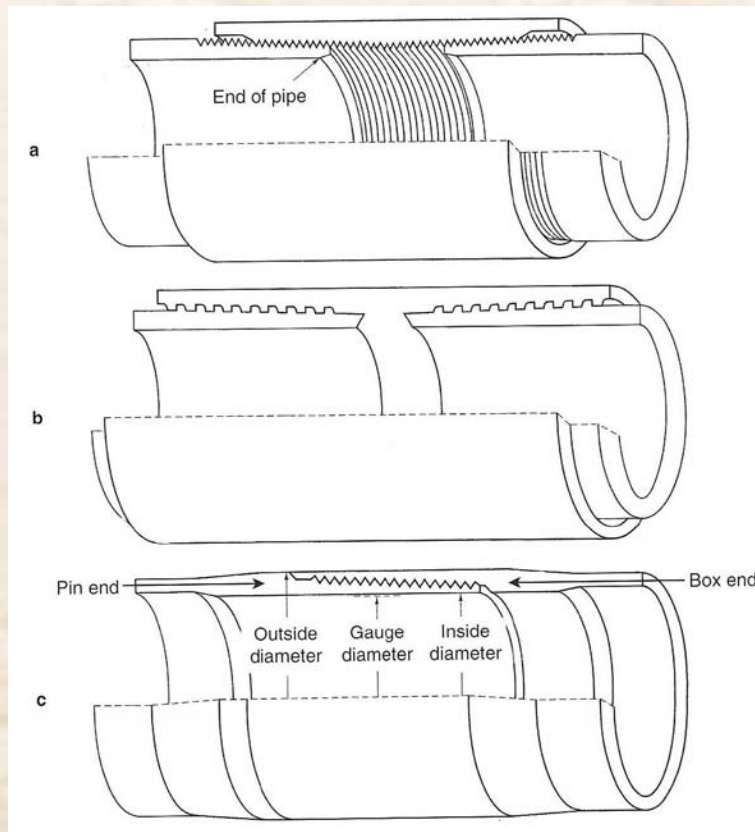
Source : Gaz de France



# CASING/LINING



## Pipe couplings

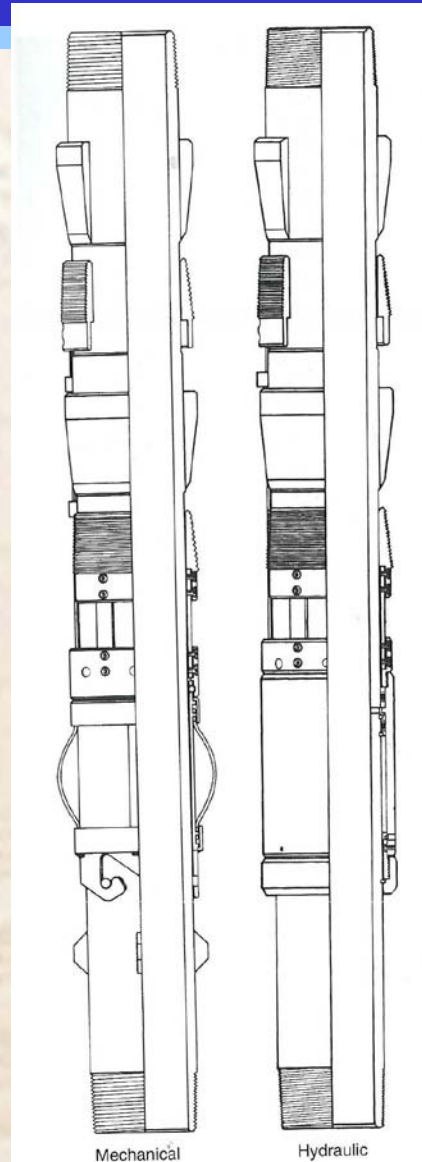


- a. API round
- b. VAM
- c. Extreme line

Source : Drilling Data Handbook, Editions Technip, Paris, 1989)



# CASING/LINING LINER HANGERS



Source : Baker



# OUTLINE



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# CEMENTING

## CEMENT CLASSES



### API Spec 10

Class	Type
A	For use from surface to 1830 m (6000 ft) depth when special properties are not required. Ordinary type.
B	For use from surface to 1830 m (6000 ft) depth when conditions require moderate to high sulfate resistance.
C	For use from surface to 1830 m (6000 ft) depth when conditions require high early compressive strength. Available in low, moderate and high sulfate-resistant types.
D	For use from 1830 m (6000 ft) to 3050 m (10,000 ft) depth under conditions of moderately high temperatures and pressures. Available in moderate and high sulfate-resistant types.
E	For use from 3050 m (10,000 ft) to 4270 m (14,000 ft) depth under conditions of high temperatures and pressures. Available in moderate and high sulfate-resistant types.
F	For use from 3050 m (10,000 ft) to 4880 m (16,000 ft) depth under conditions of extremely high temperatures and pressures. Available in moderate and high sulfate-resistant types.
G	For use from surface to 2440 m (8000 ft) depth as manufactured, or can be used with accelerators and retarders to cover a wide range of well depths and temperatures. Available in moderate and high sulfate-resistant types.
H	For use from surface to 2440 m (8000 ft) depth as manufactured, or can be used with accelerators and retarders to cover a wide range of well depths and temperatures. Available only in moderate sulfate-resistant type.
J	For use from 3660 to 4880 m (12,000 to 16,000 ft) depth under conditions of extremely high temperatures and pressures. Available only in sulfate-resistant type.

Source : J.P. NGUYEN



# CEMENTING

## CEMENT ADDITIVE CHARACTERISTICS



Cement Characteristics	Cement Additives Effect	Bentonite	Perlite	Diatomaceous earth	Pozzolan	Sand	Barite	Hematite	Calcium chloride	Sodium chloride	Lignosulfonate	CMHEC (1)	Diesel oil	Water loss additive	Lost circulation material
Density	Decreased	•	•	•	•										
	Increased					•	•	•	x	x	x				
Water required	Decreased										•				
	Increased	•	x	•	x	x	x	x							x
Viscosity	Decreased								x		•				
	Increased	x	x	x	x	x	x	x							
Thickening time	Accelerated	x					x	x	•	•					
	Retarded			x						x	•	•	x	x	
Setting time	Accelerated						x	x	•	•					
	Retarded	x	x	x	x						•	•		x	
Early strength	Decreased	x	x	x	x		x	x			•	•		x	x
	Increased								•	•					
Final strength	Decreased	x	x	•	x		x					x		x	x
	Increased														
Duration	Decreased	x	x	x									x		x
	Increased				•										
Water loss	Decreased	•									x	•	x	•	x
	Increased		x	x											

x Denotes minor effect

• Denotes major effect and/or purpose of additive

(1) Carboxymethyl hydroxyethyl cellulose

Source : Drilling Data Handbook,  
Editions Technip & Dowell Schlumberger

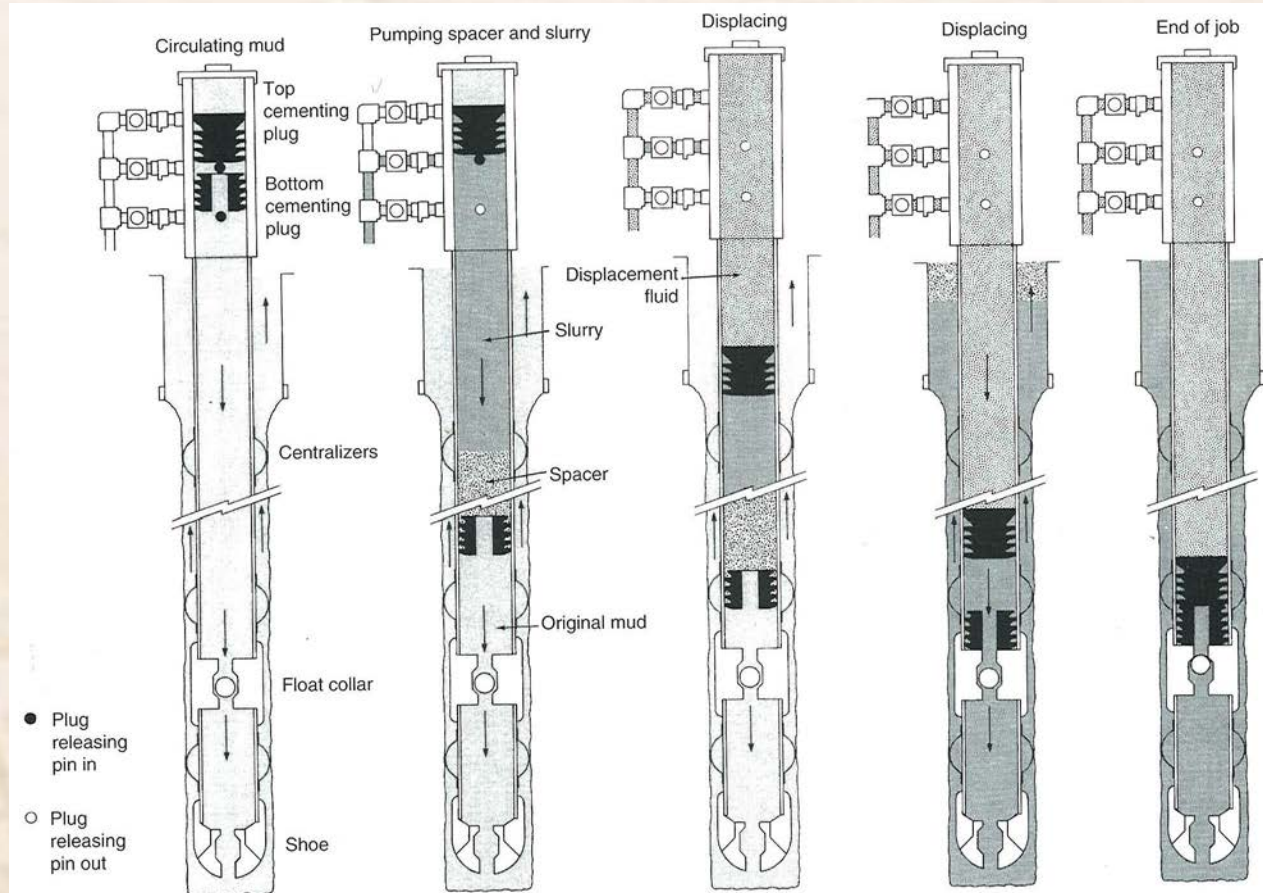


# CEMENTING

## PRIMARY CASING CEMENTING SEQUENCE



### Primary casing cementing sequence

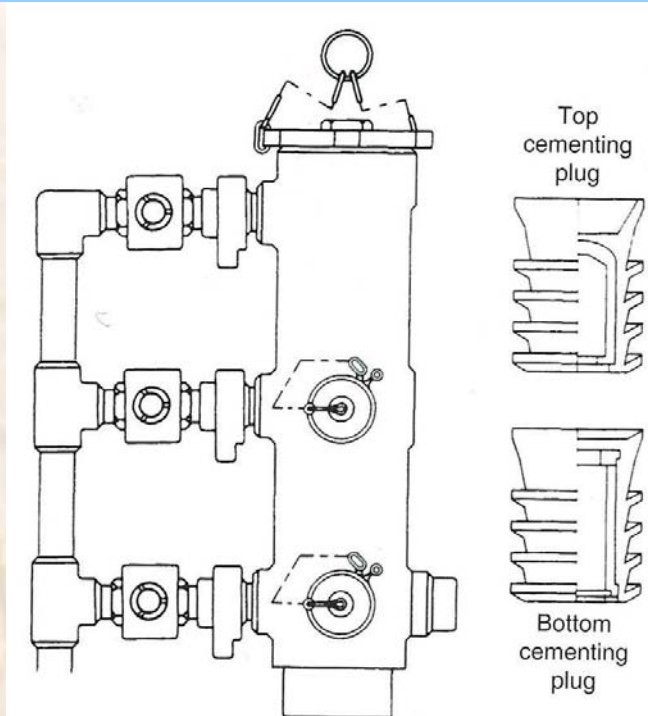


Source : Dowell Schlumberger



# CEMENTING

## TWIN-PLUG CEMENTING HEAD



**HEAD**

**PLUGS**



**Top**

**Bottom**

Source : Weatherford



# CEMENTING CASING AND CEMENTING OPERATIONS



## CEMENTING COMPONENTS

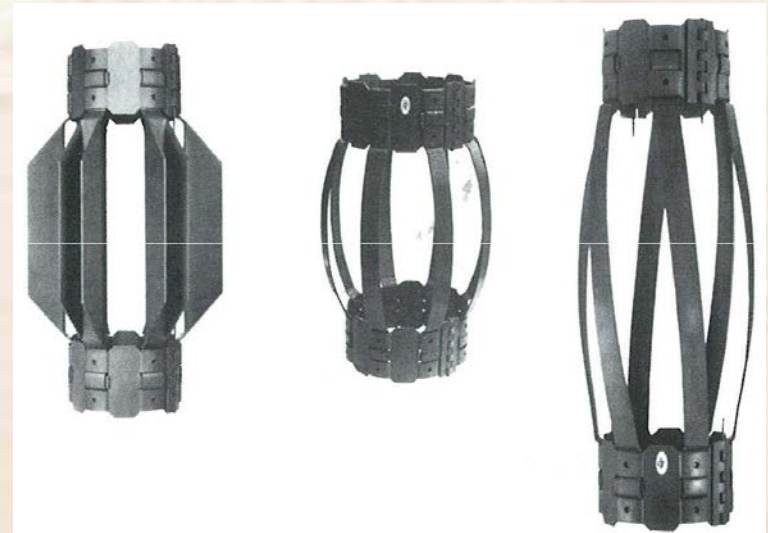


**Shoes**

**Landing float collar**

Source : Halliburton

## CENTRALIZERS

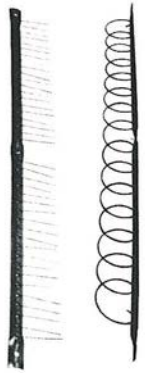


Source : Weatherford



# CEMENTING

## CEMENTING ACCESSORIES

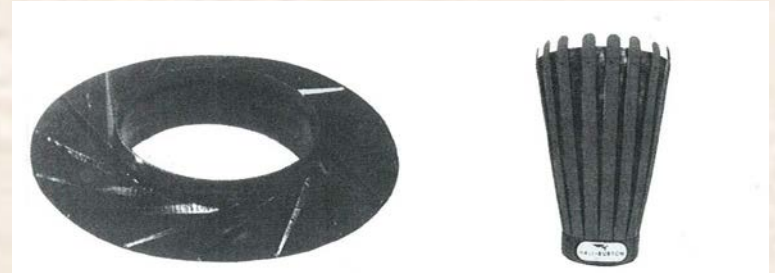


Rotating scratchers



Reciprocating scratchers

**Scratchers**



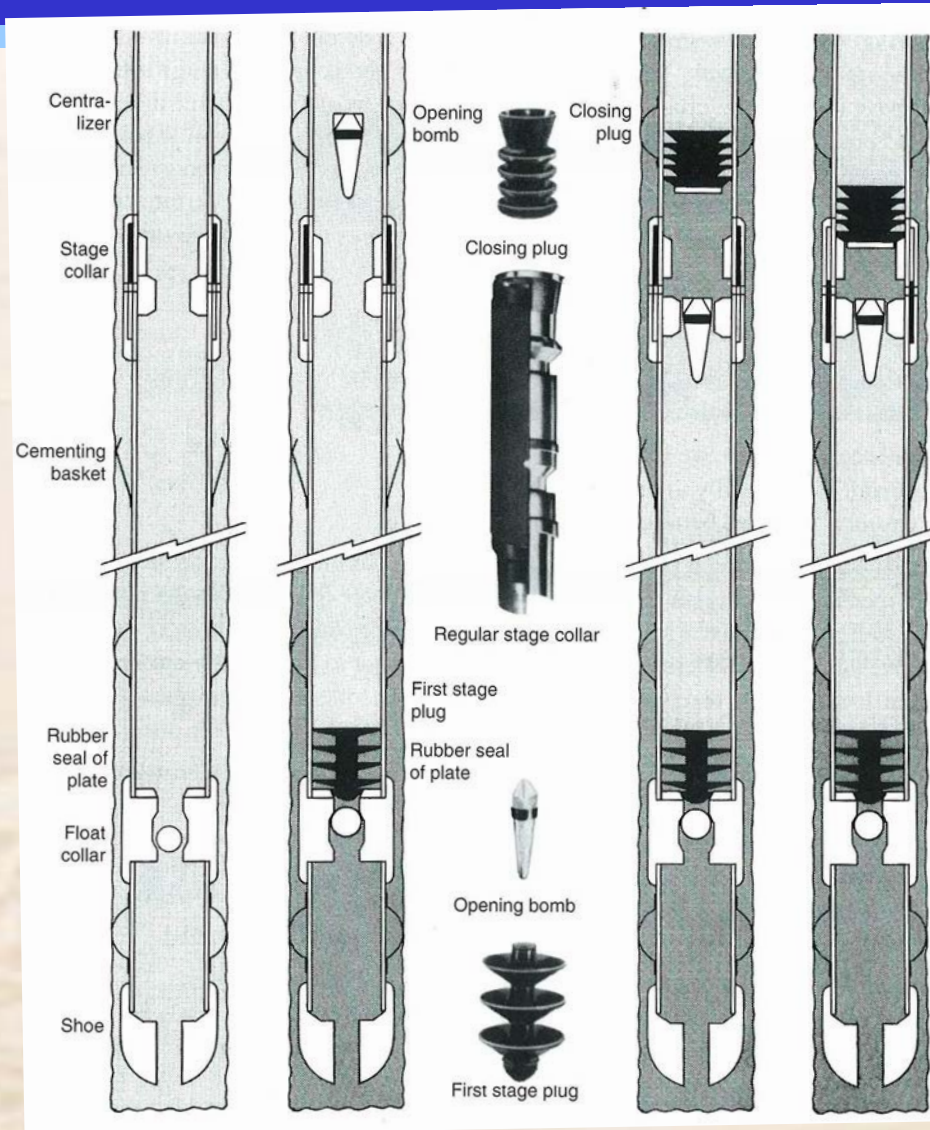
**Hydrobonder**

Source : Halliburton



# CEMENTING

## TWO-STAGE CEMENTING SEQUENCE

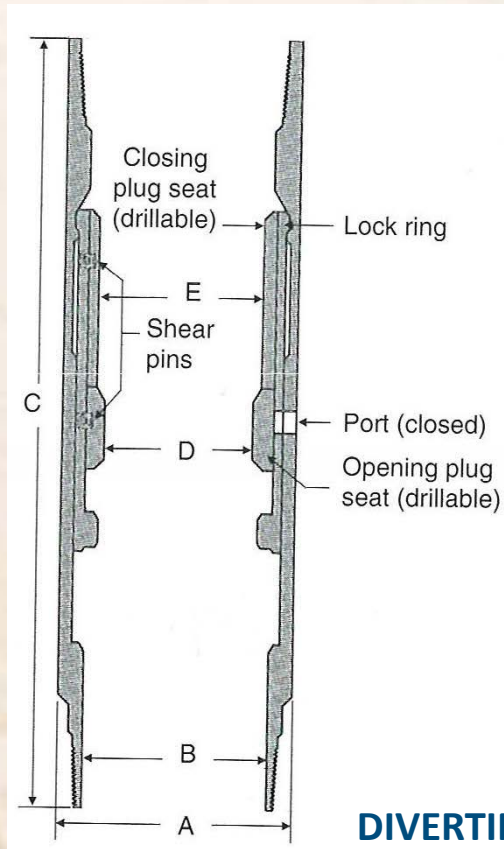


Source : Weatherford

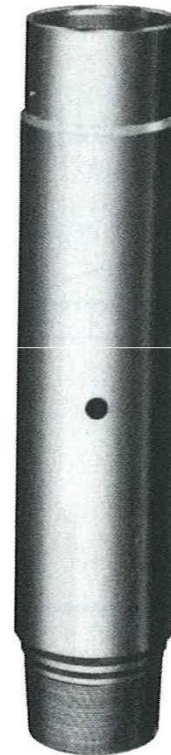


# CEMENTING

## TWO-STAGE CEMENTING EQUIPMENT



**DIVERTING VALVE**



Closing plug



**PLUG**



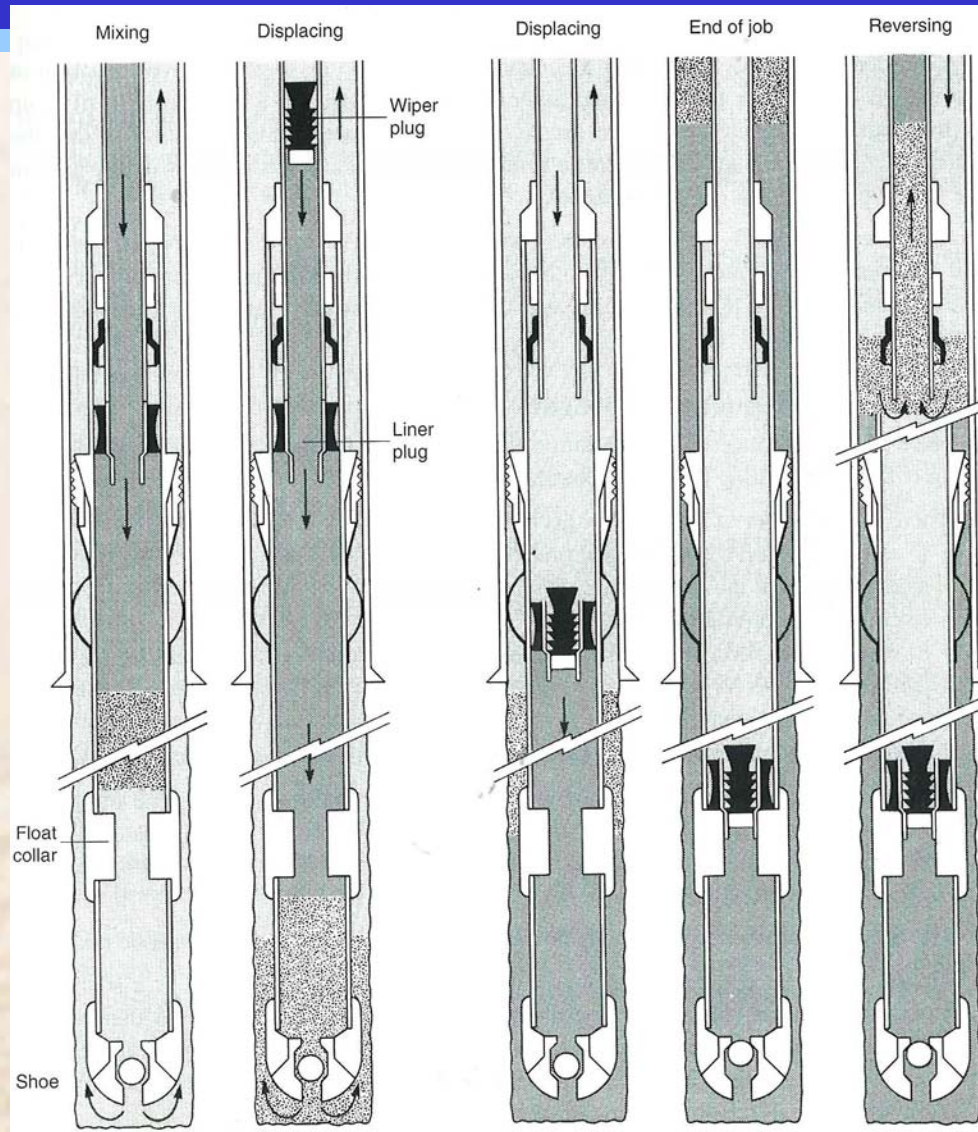
Free fall plug

**PLUGS**

Source : BJ Hughes



# CEMENTING LINER CEMENTING SEQUENCE



**LINER**

Source : Weatherford



# CEMENTING LINER CEMENTING SEQUENCE



**Weatherford®**

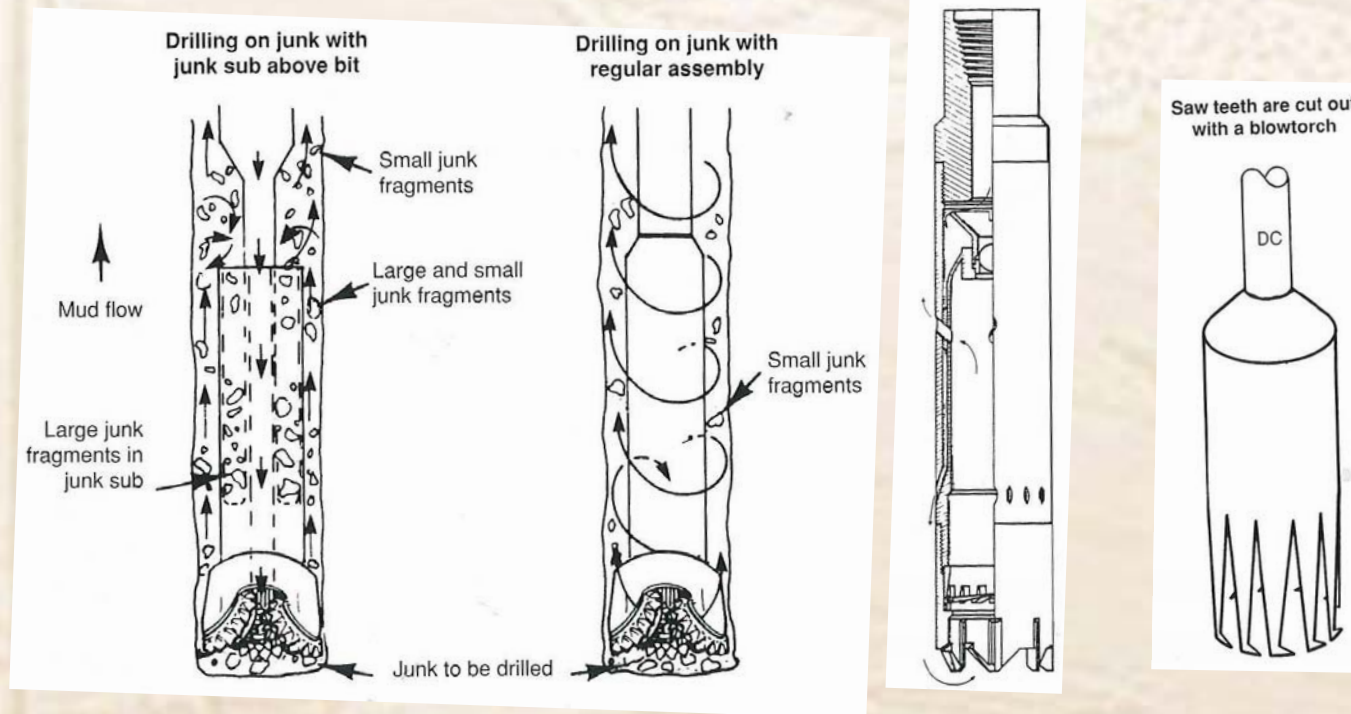
**751PD Stage Tool**



# CEMENTING LINER CEMENTING SEQUENCE



## FISHING BASKETS



Source : J.P. NGUYEN



# OUTLINE

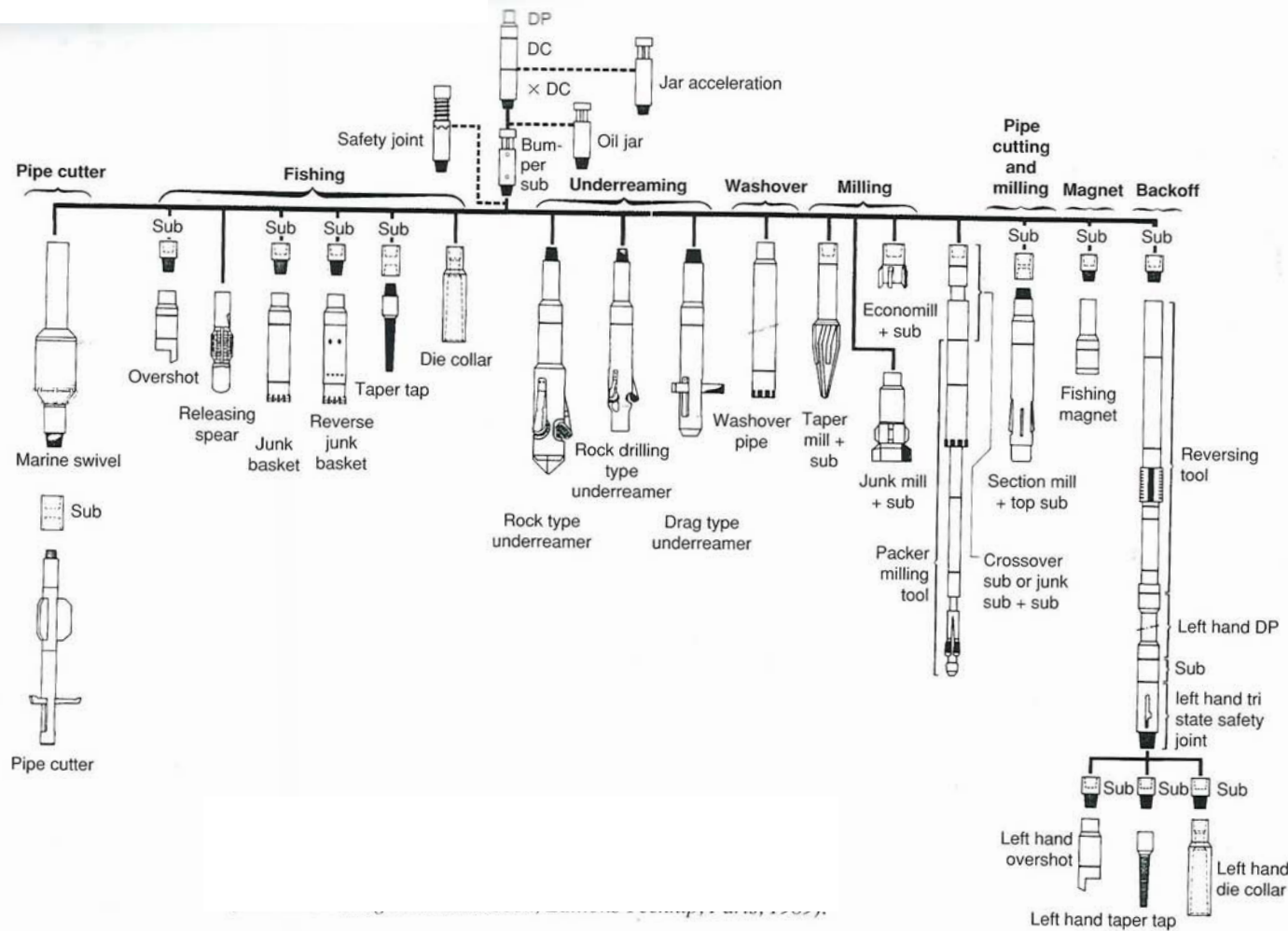


- SCOPE
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# FISHING

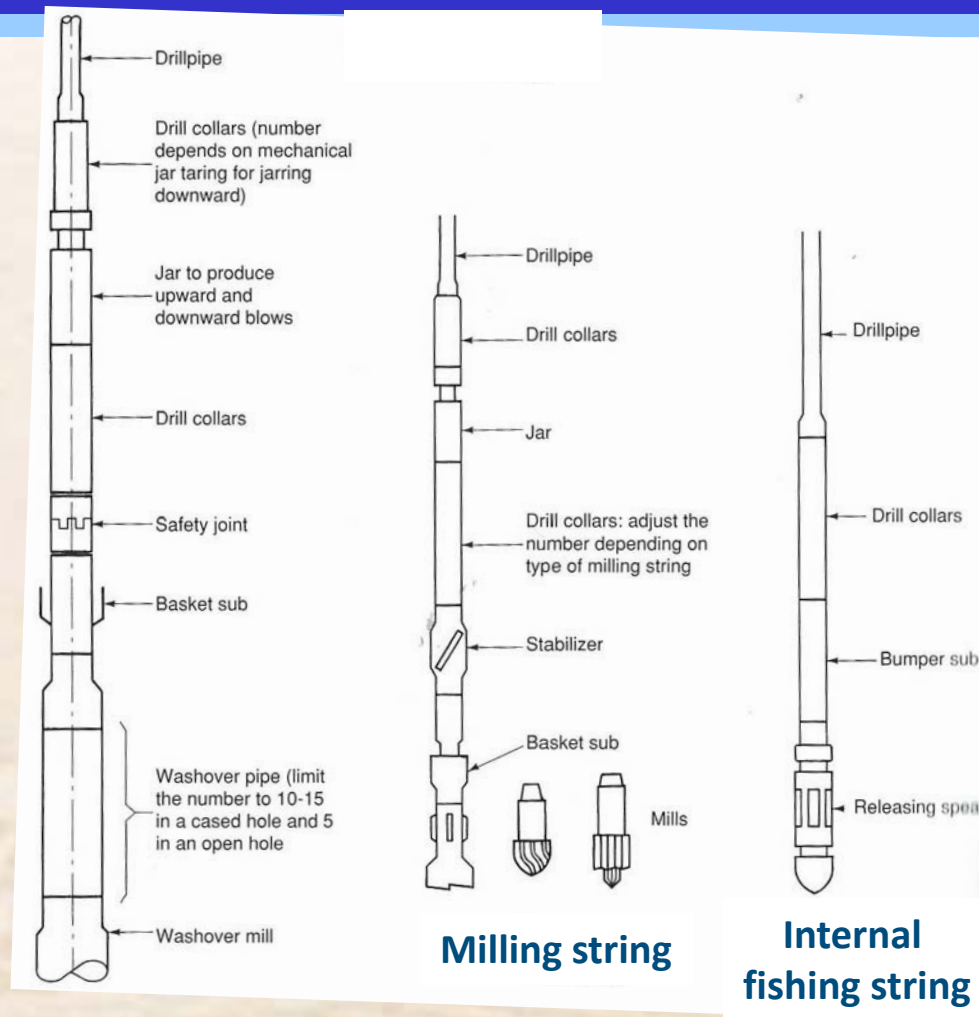
## TYPICAL FISHING, MILLING AND BACK OFF STRINGS



Source : Drilling Data Handbook, Editions Technip, Paris)



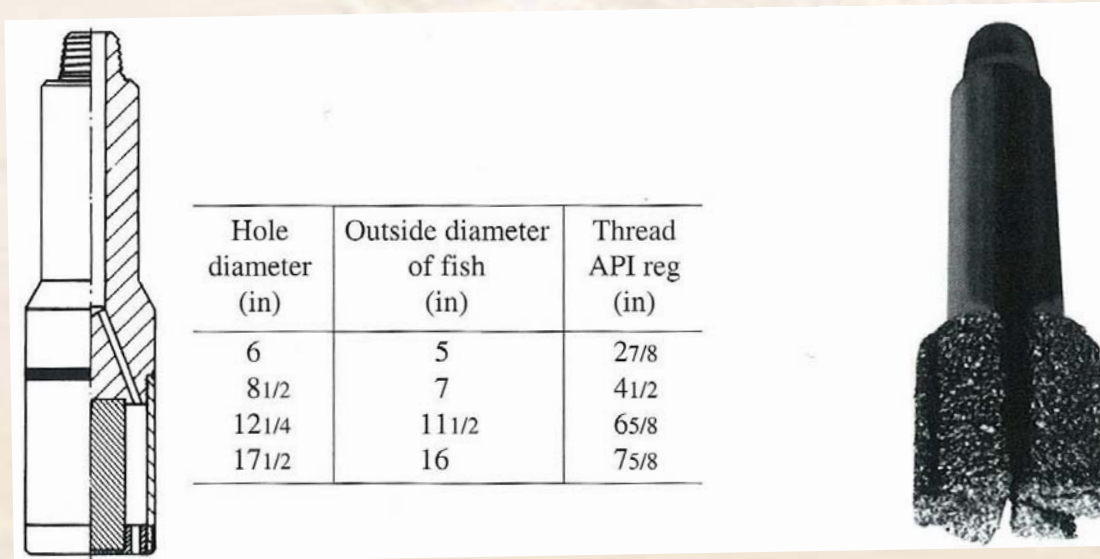
# FISHING WASHOVER ASSEMBLY



Source : J.P. NGUYEN



# FISHING MAGNET & JUNK MILL



**Permanent magnet**

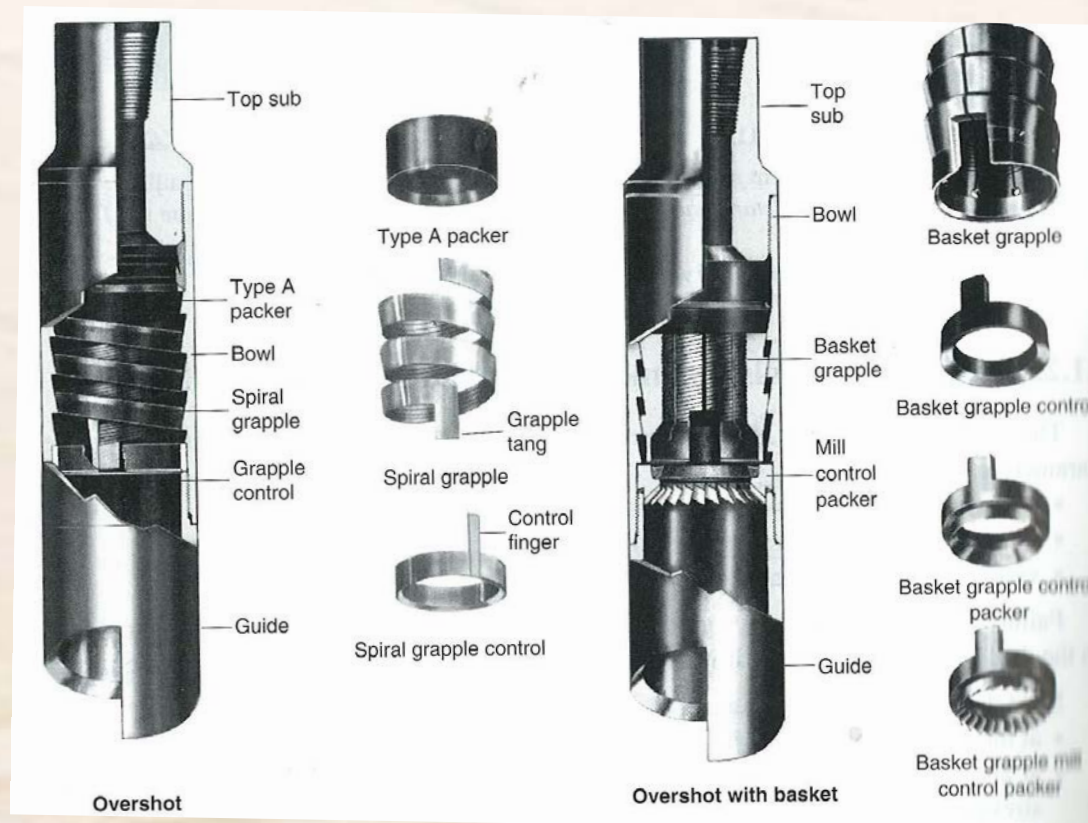
**Junk mill**

Source : Drillstar Industries

Source : Tristate Oil Tool



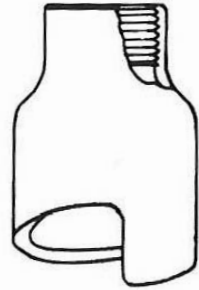
# FISHING OVERSHOT & GRAPPLES



Source : Bowen



# FISHING OVERSHOT GUIDES



Oversize guide



Wall hook guide

Source : Drillsatr Industries

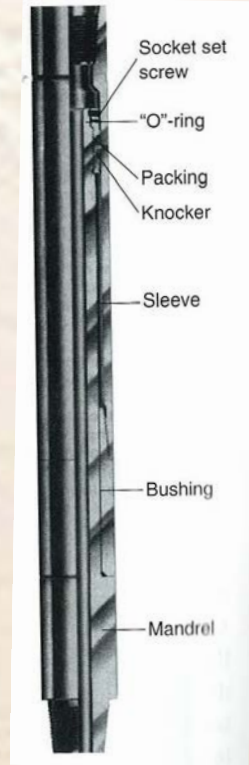


# FISHING BUMPER SUBS



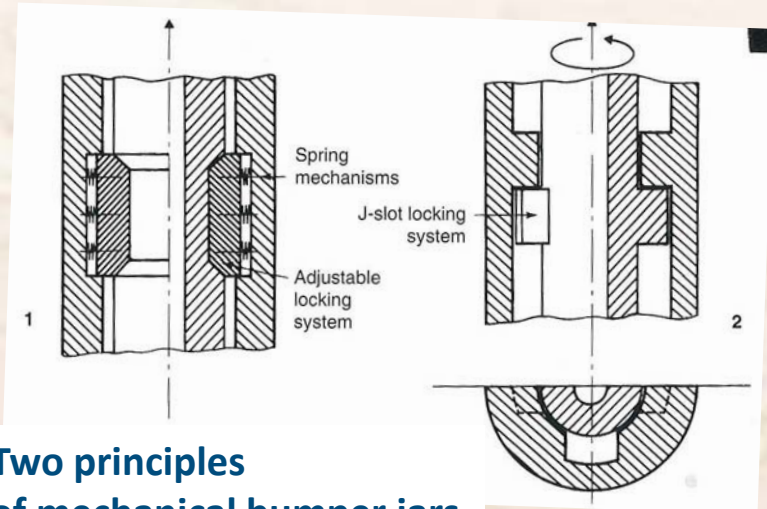
**Mechanical bumper sub**

Source : N.L. MacCullough



**Bumper sub**

Source : AZ



**Two principles  
of mechanical bumper jars**

Source : Eastman Christensen



# FISHING HYDRAULIC BUMPER SUB

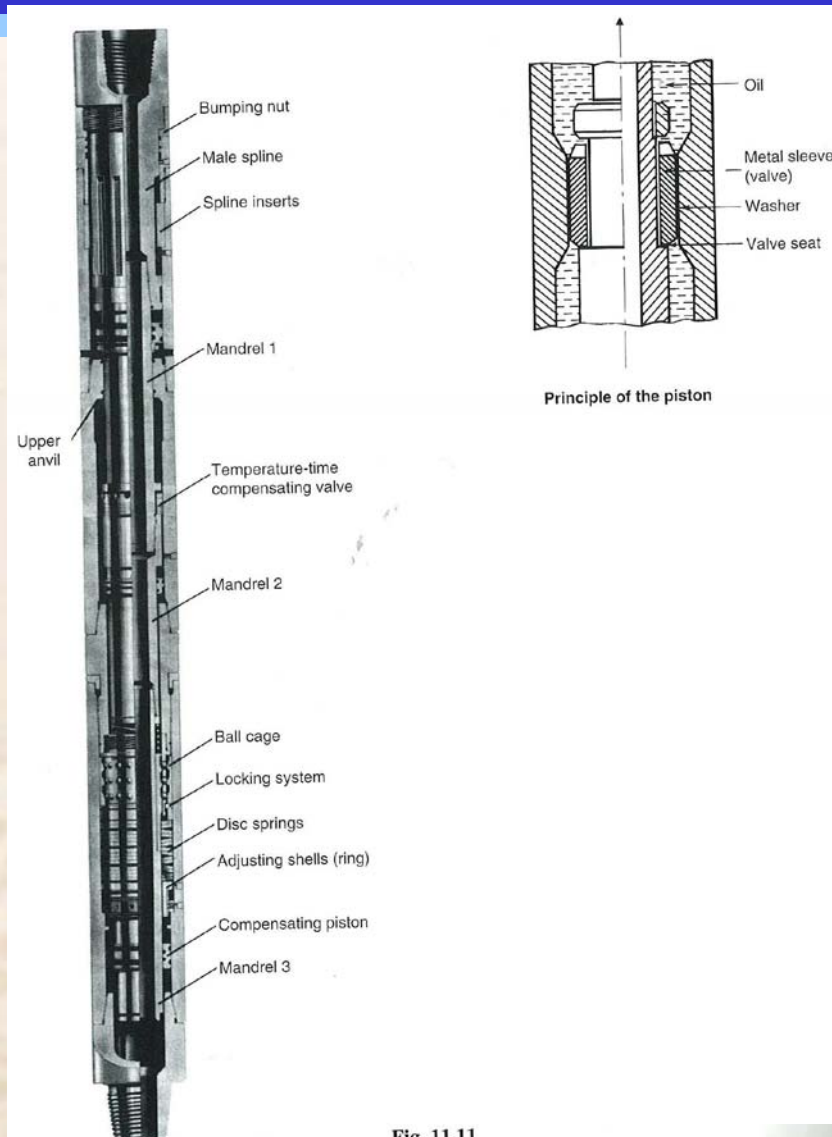


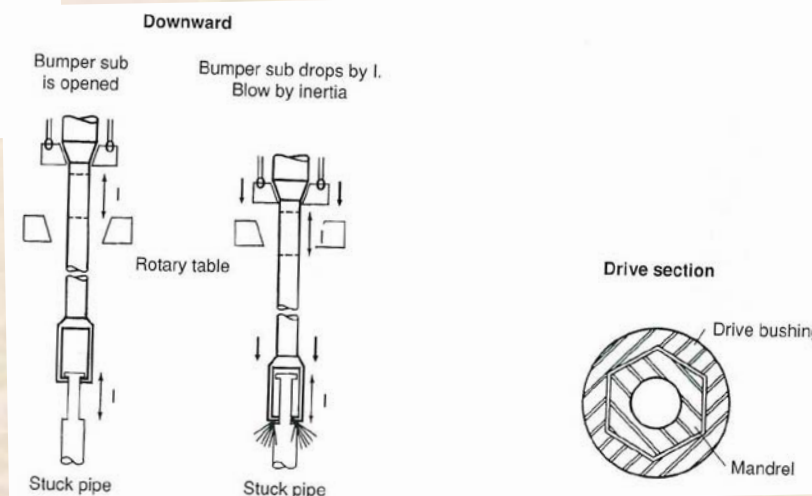
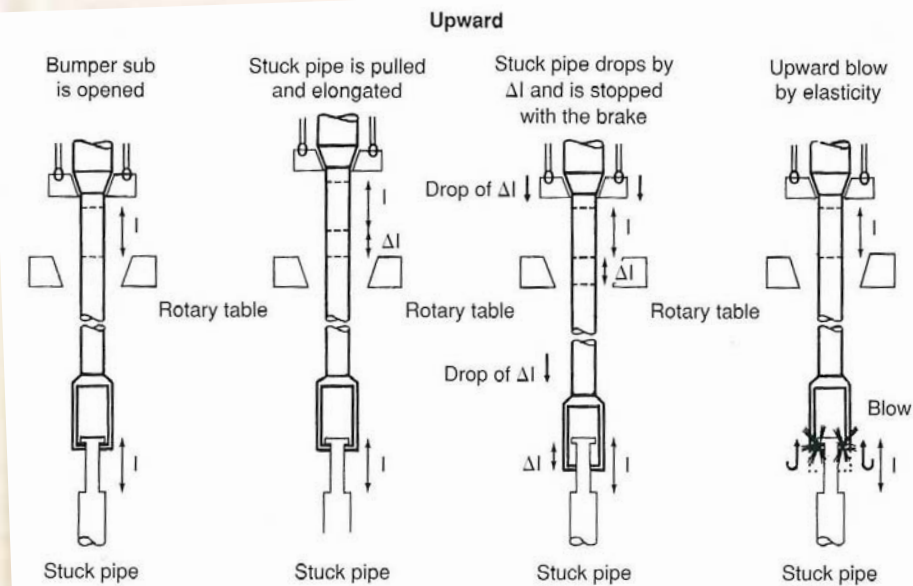
Fig. 11.11

Source : Eastman Christensen



# FISHING

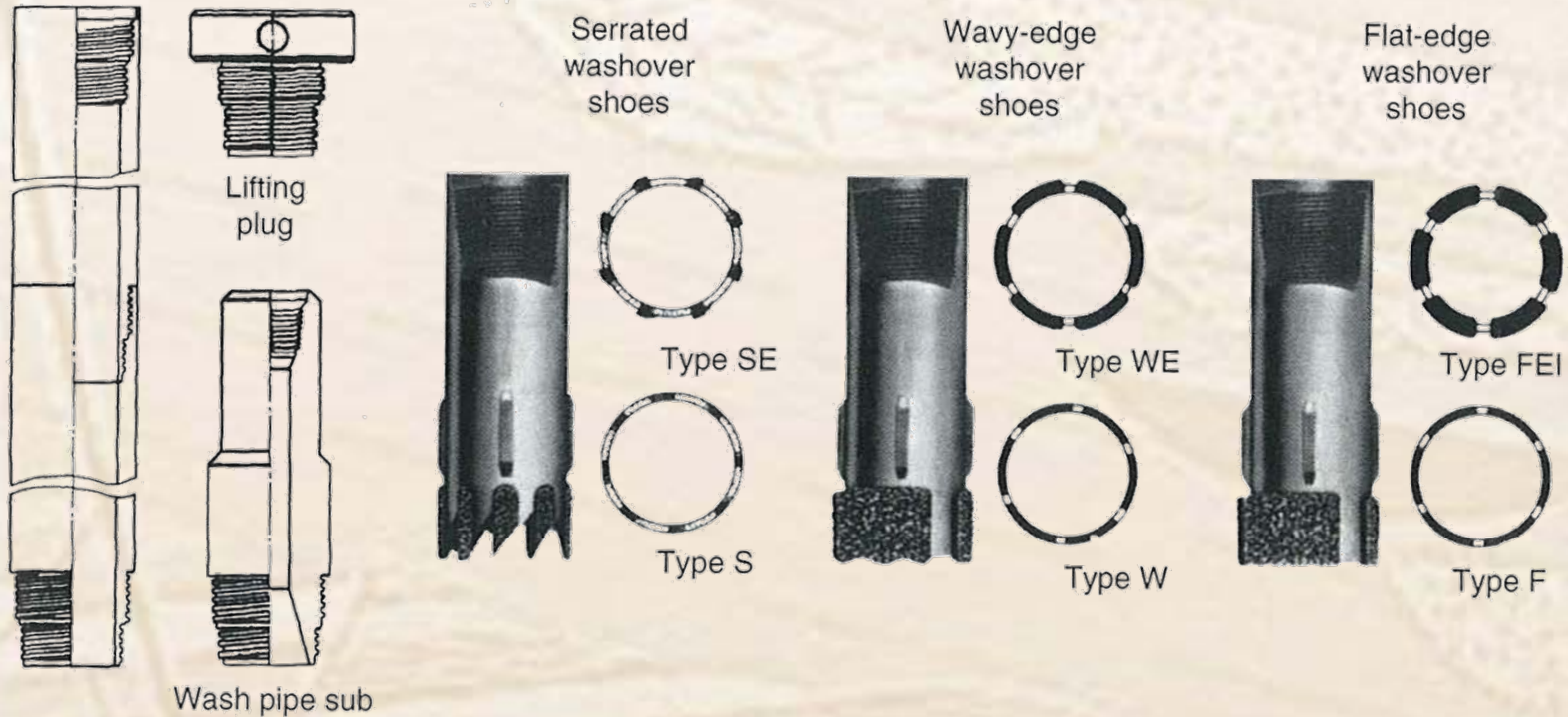
## UPWARD & DOWNWARD JARRING



Source : J.P. NGUYEN



# FISHING WASHOVER ASSEMBLY COMPONENTS



Source : Drillstar Industries



# FISHING

## TYPICAL FISHING BHAS





# OUTLINE



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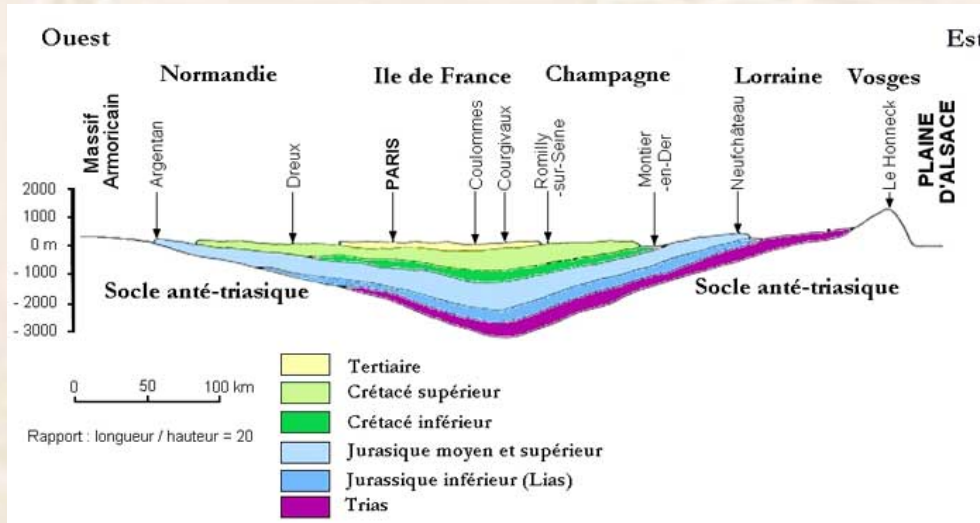


# CASE STUDY

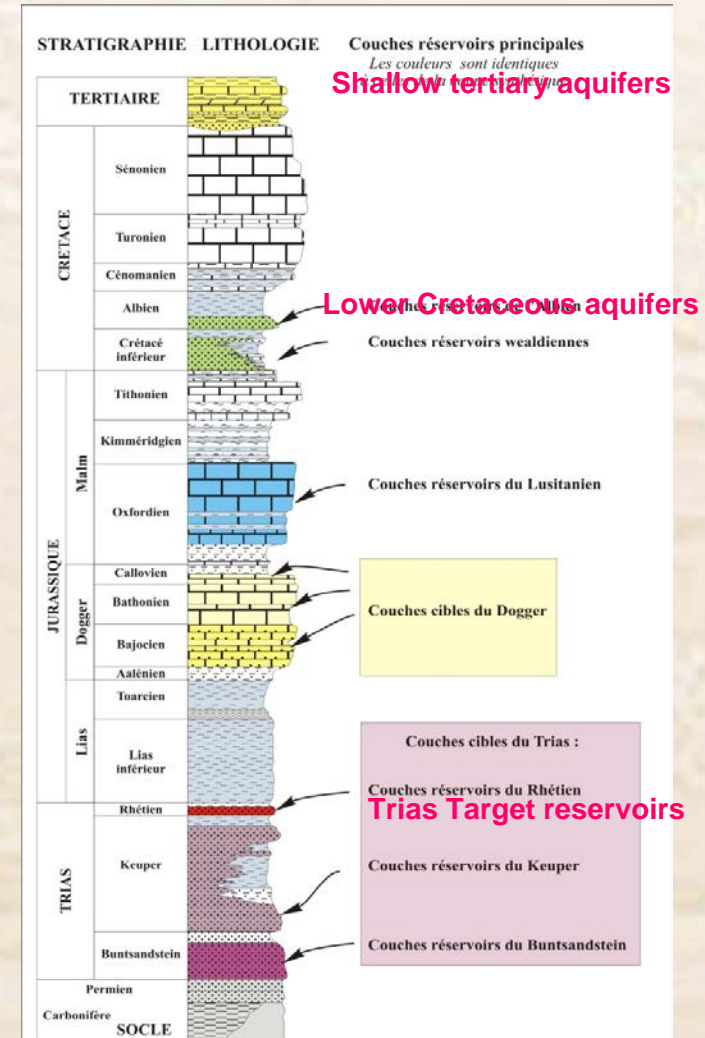
## PARIS BASIN. GEOLOGICAL SKETCHES



### West East Cross Section



### Lithostratigraphic column and target reservoir horizons



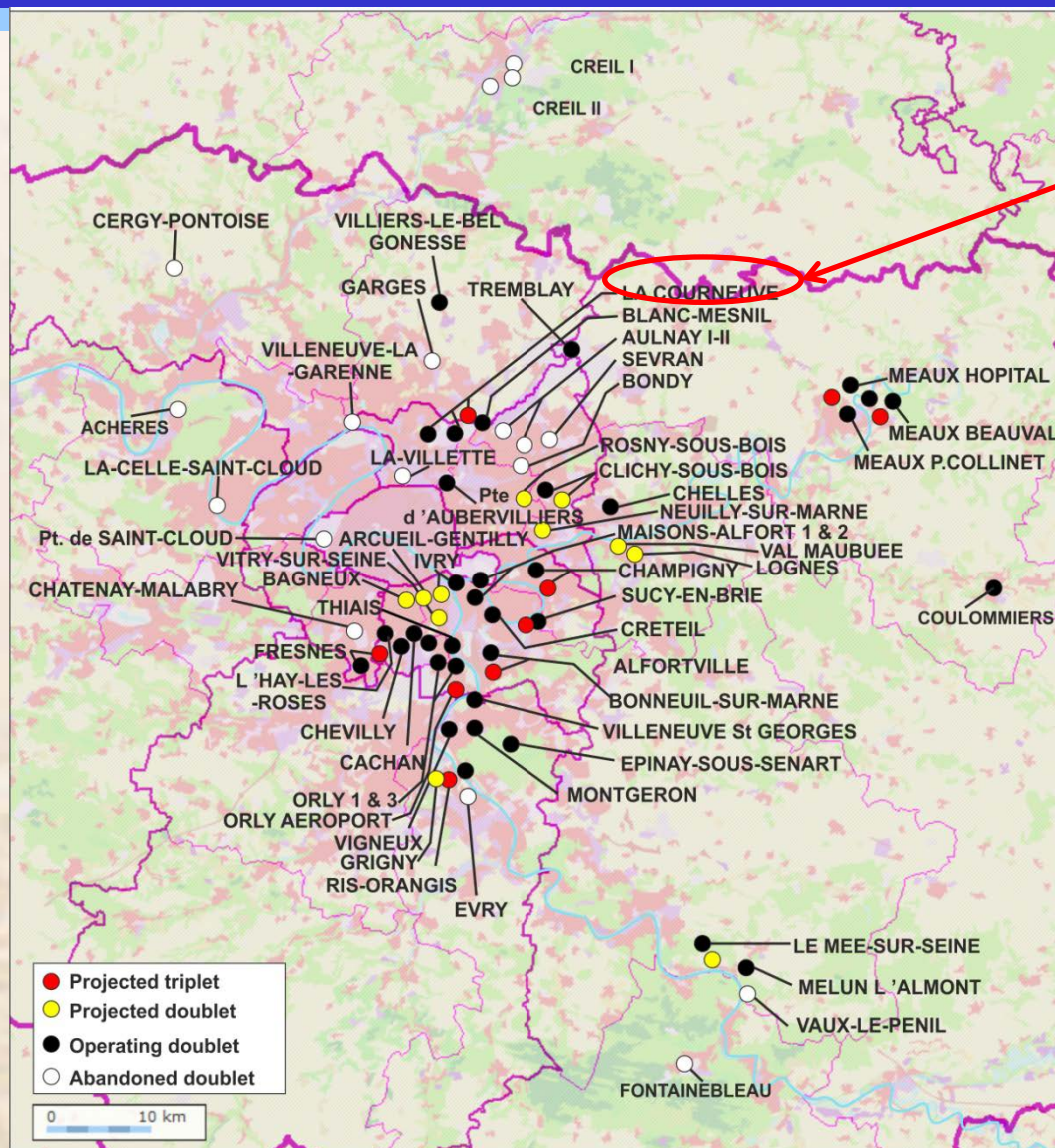


# CASE STUDY

## PARIS BASIN GDH STATUS (@ JAN. 2012)



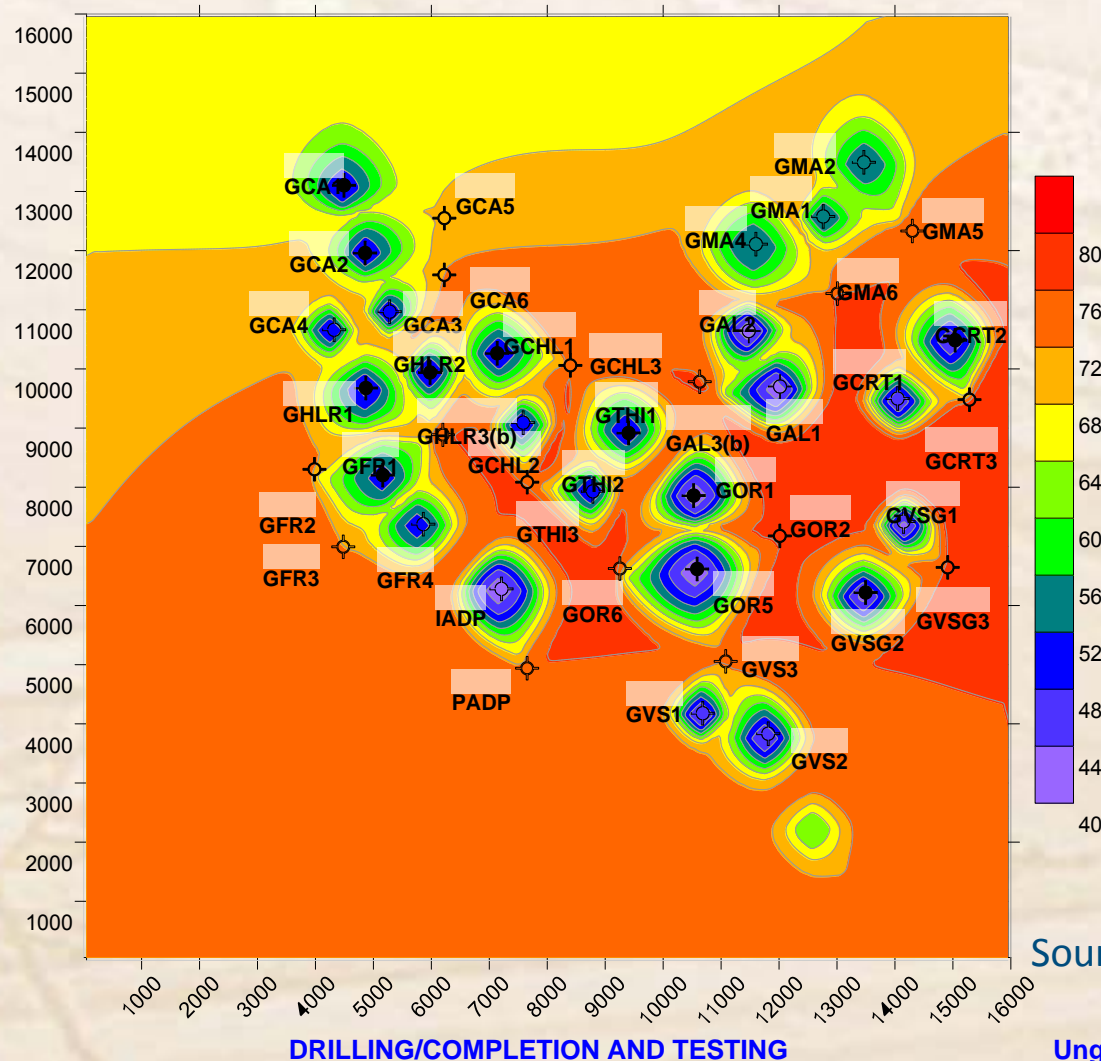
CASE STUDY





# CASE STUDY

## PARIS BASIN GDH EXPLOTATION STATUS (PARIS SOUTH)

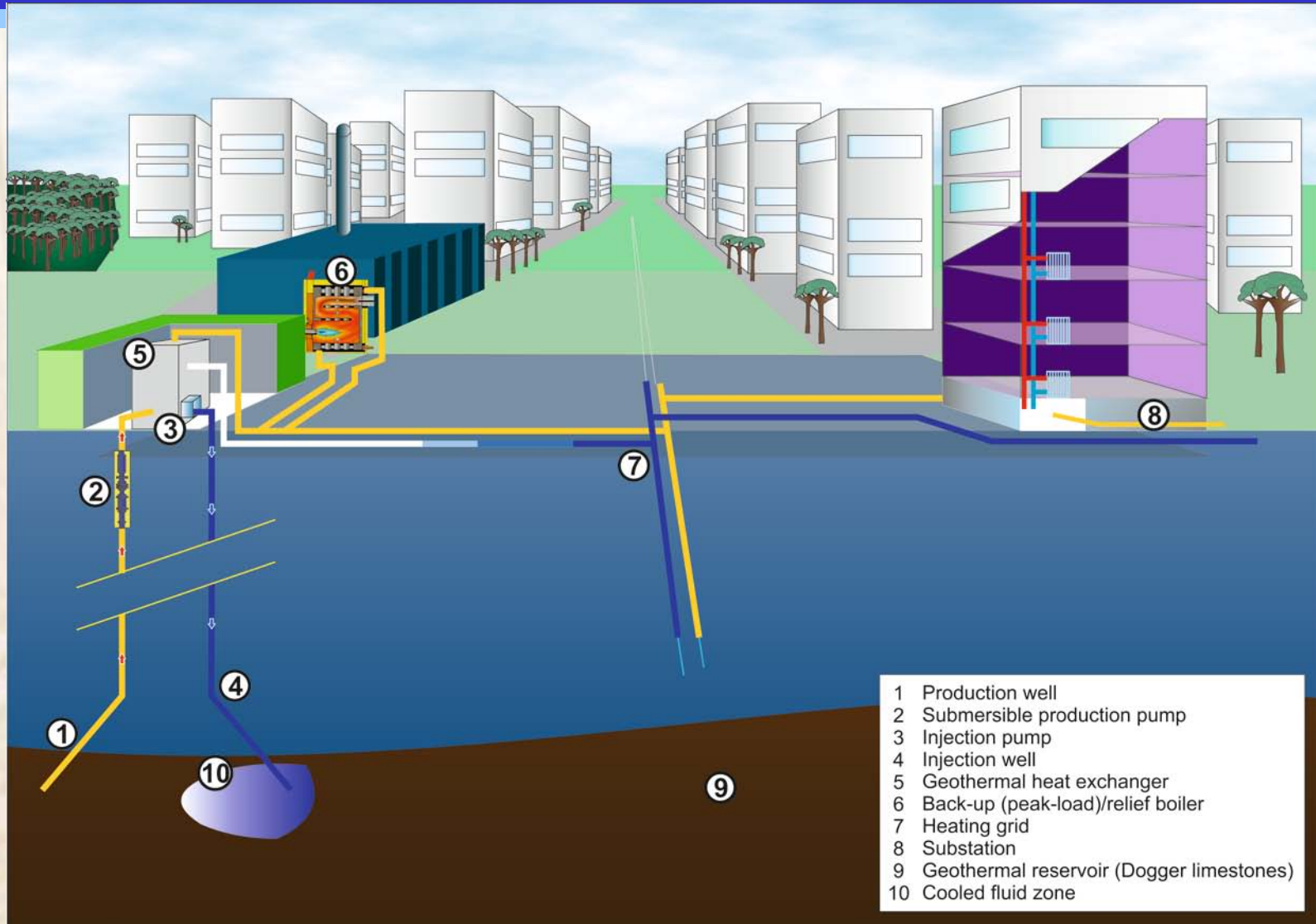


Source : Maria Papachristou



# CASE STUDY

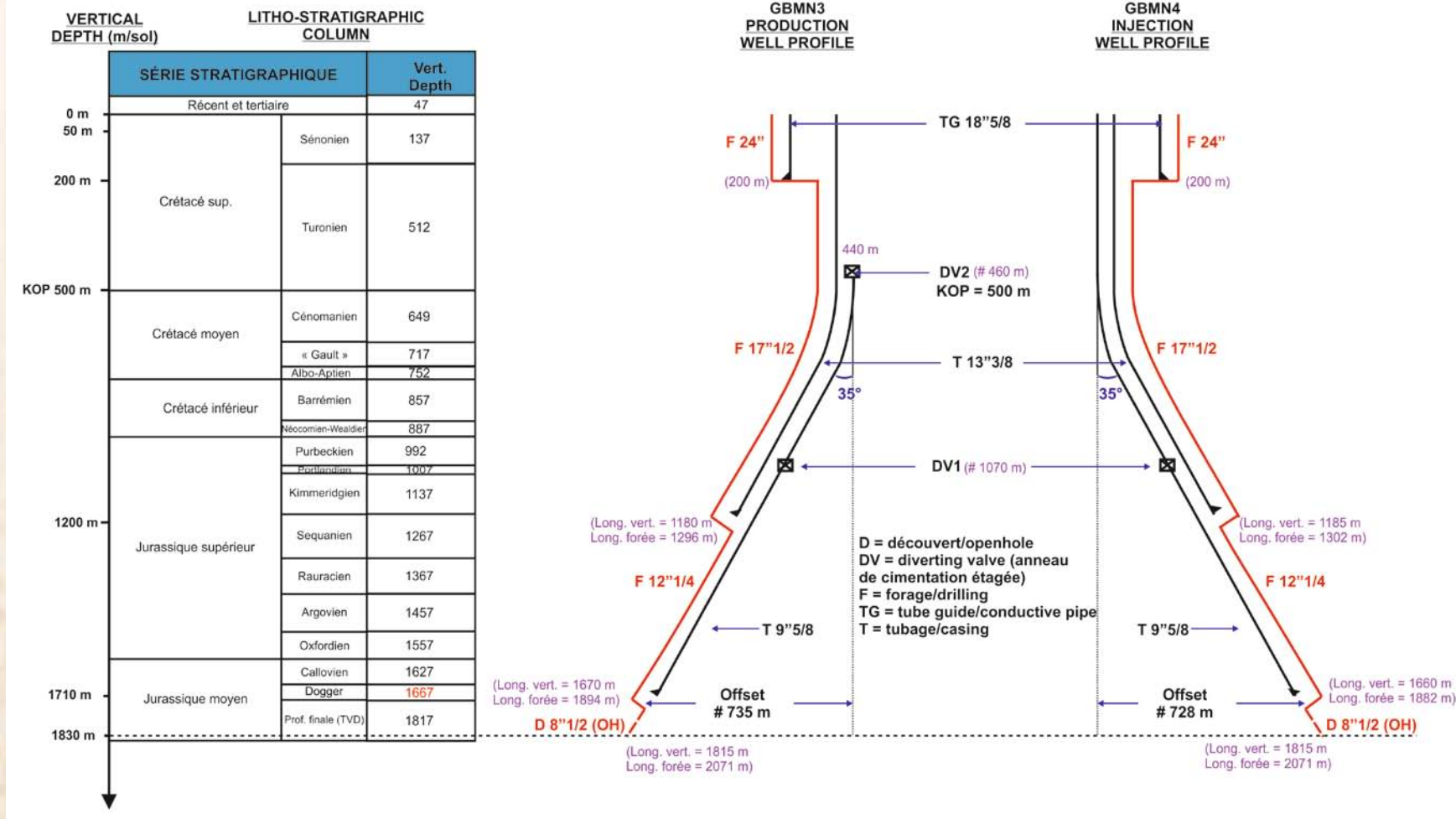
## PARIS BASIN GDH SCHEME





# CASE STUDY

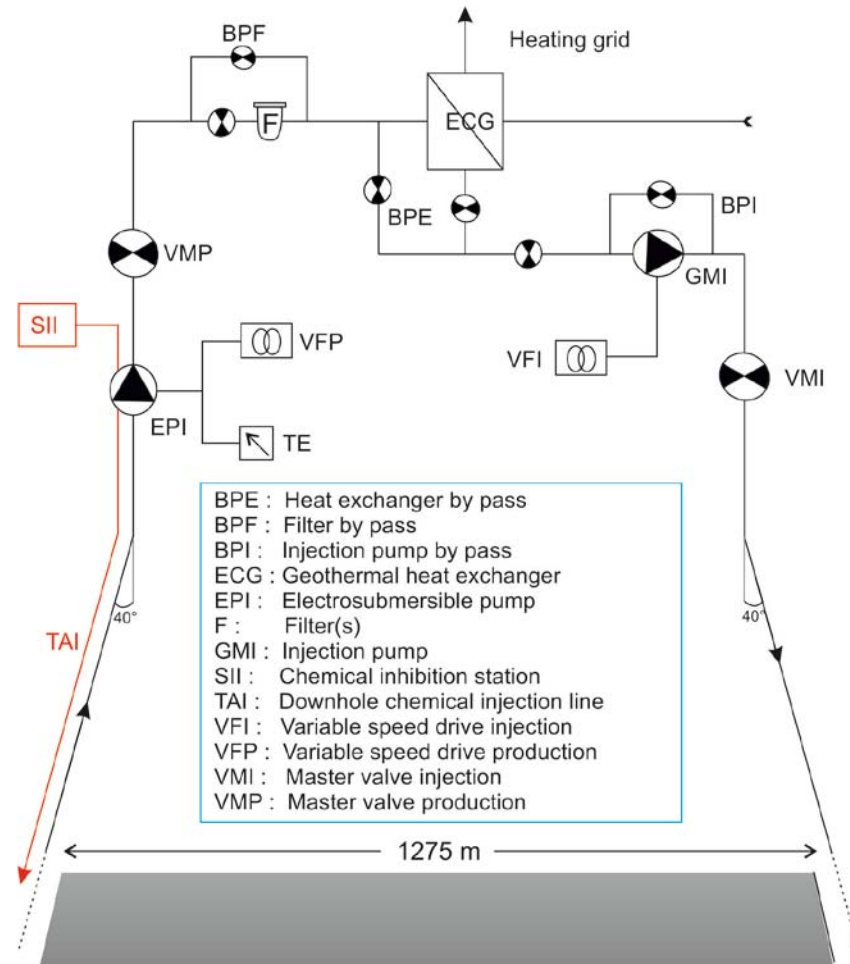
## TYPICAL GDH WELL ARCHITECTURES





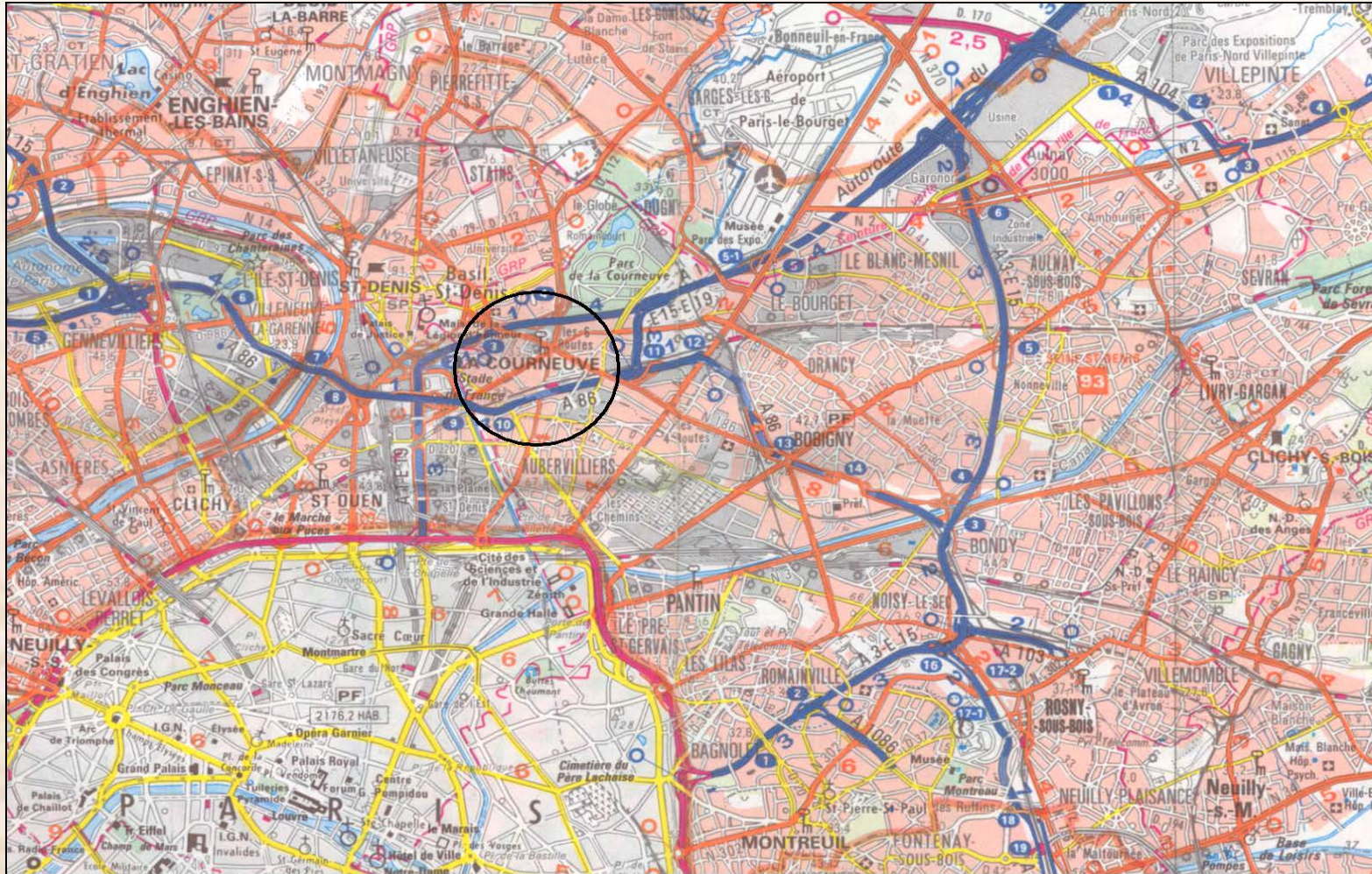
# CASE STUDY

## GEOHERMAL LOOP DESIGN



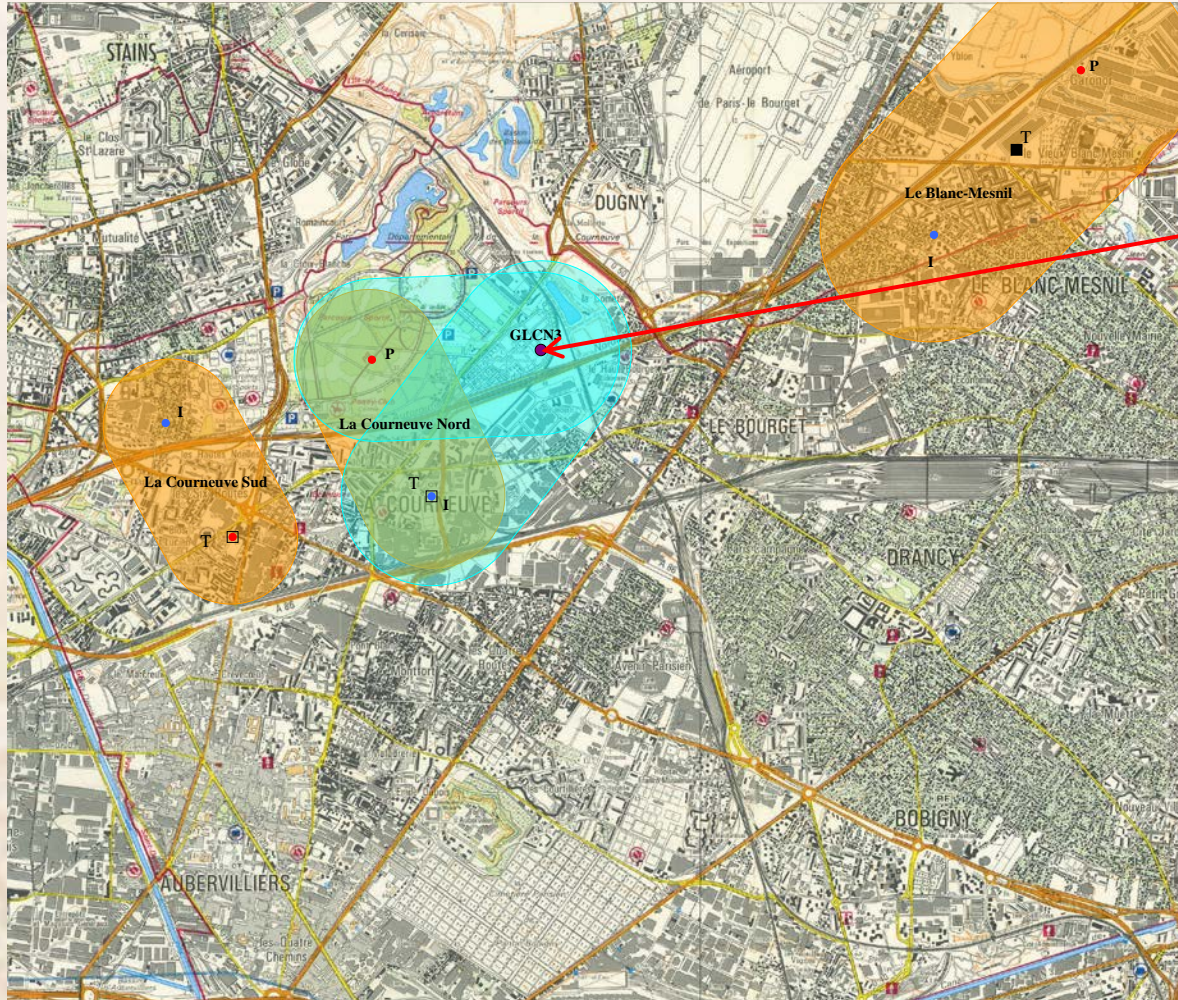


# CASE STUDY GLCN3 WELL LOCATION MAP





# EXPLORATION/EXPLOITATION PERIMETERS OF EXISTING AND FUTURE (TRIplet/DOUBLEt) GDH SYSTEMS



**NEW TRIPLET  
PRODUCTION WELL**

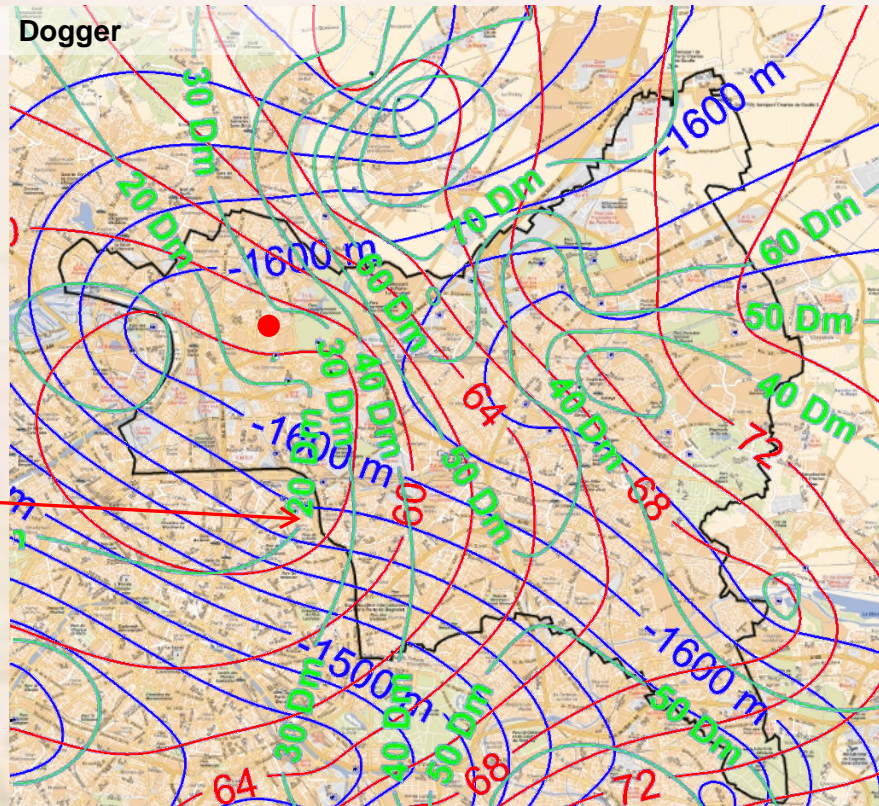


# CASE STUDY GLCN3

## DOGGER RESERVOIR CHARACTERISTICS. PARIS NORTH



GLCN  
3

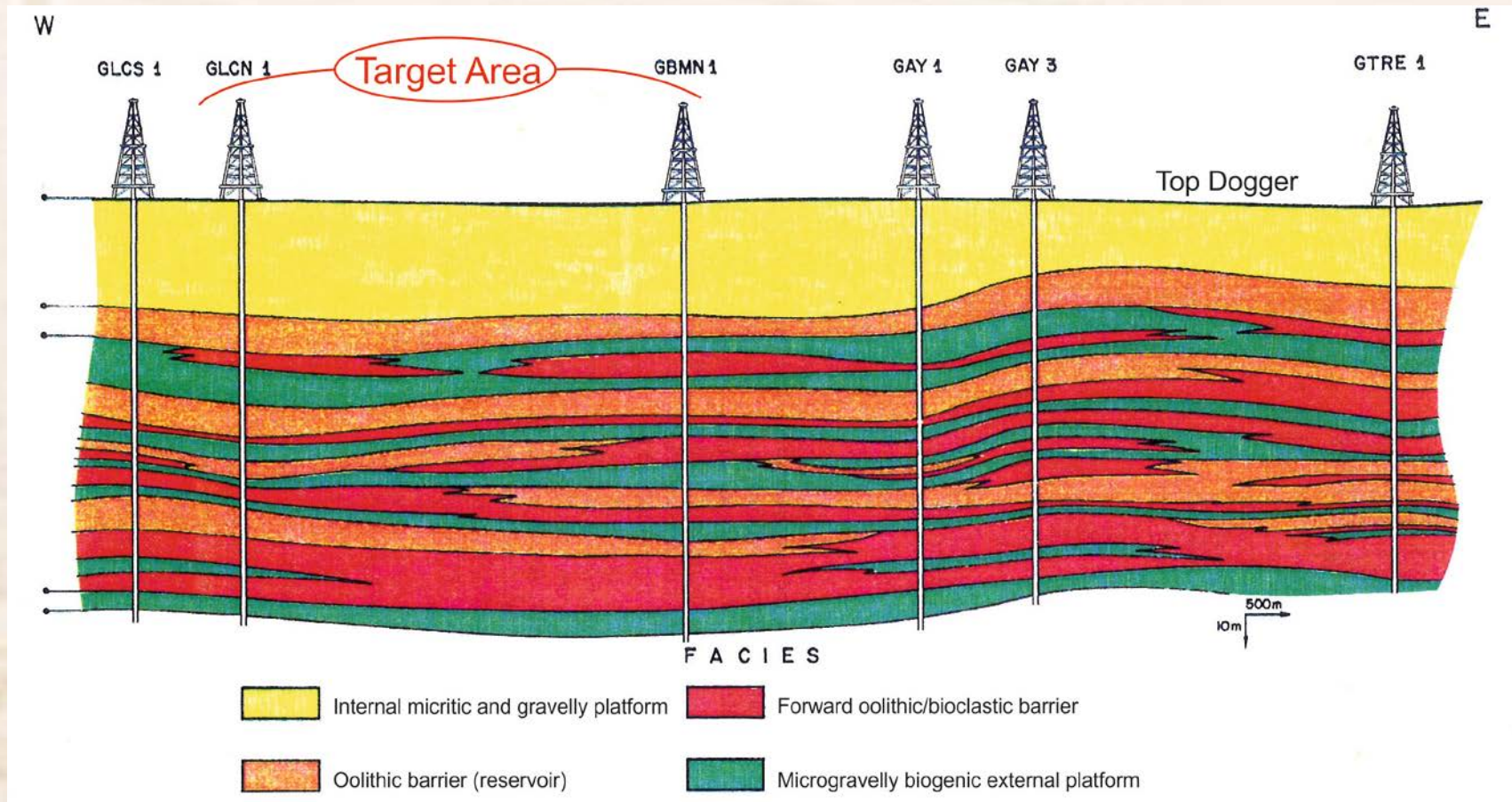




# CASE STUDY GLCN3

## RESERVOIR ASSESSMENT TENTATIVE FACIES CORRELATIONS.

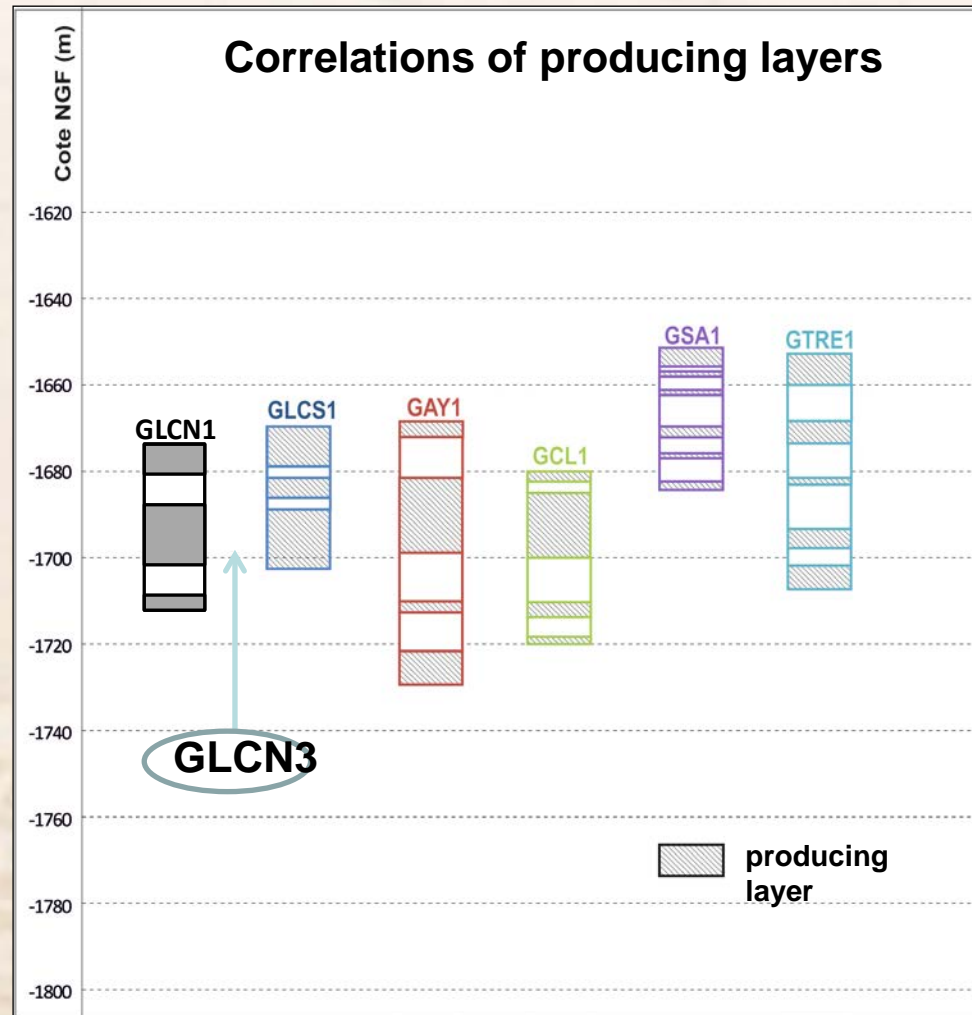
### PARIS NORTH





# CASE STUDY GLCN3

## RESERVOIR ASSESSMENT CORRELATION OF PRODUCING LAYERS

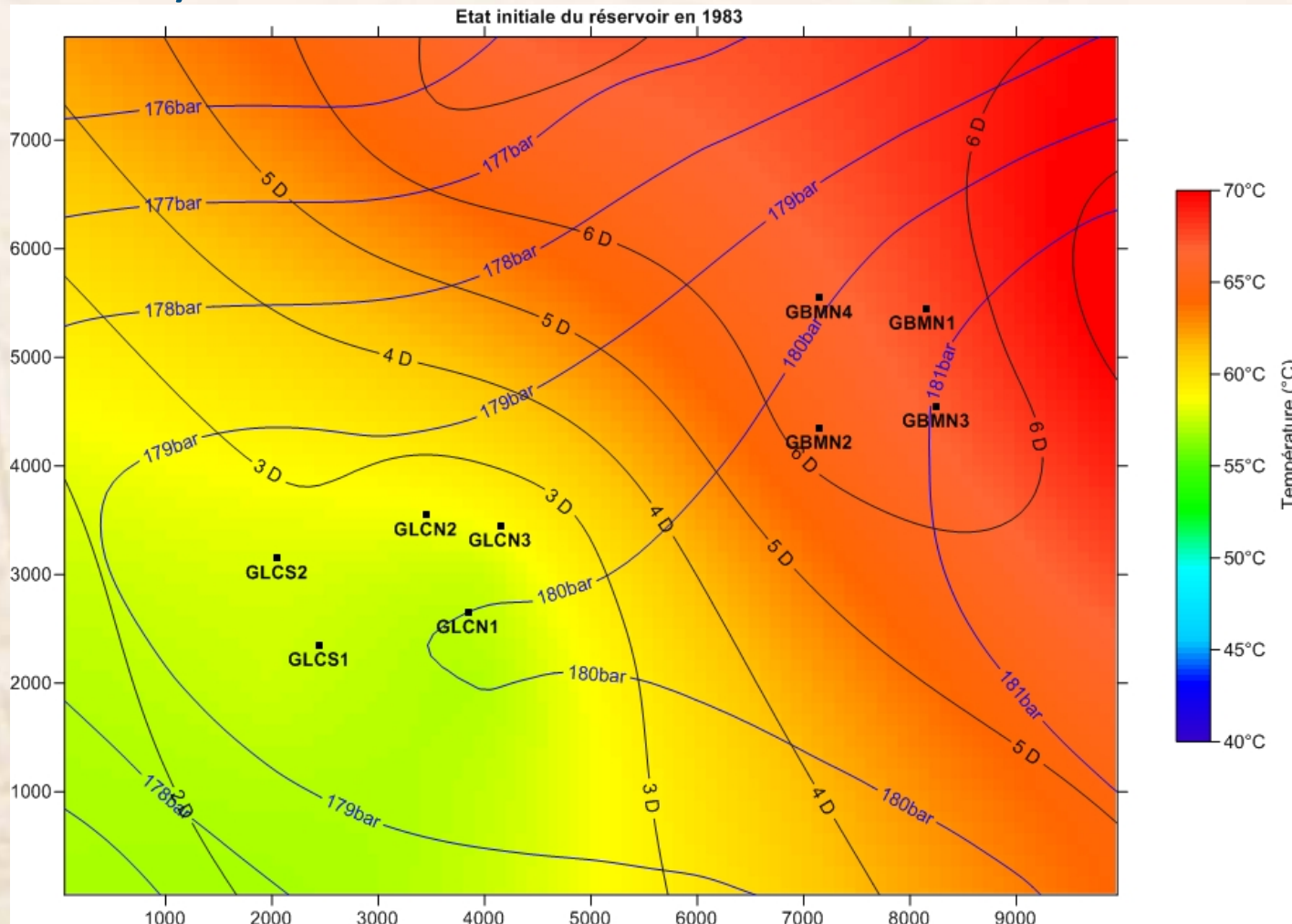




# CASE STUDY GLCN3. RESERVOIR SIMULATION INITIAL PRESSURE, TEMPERATURE & PERMEABILITY STATE



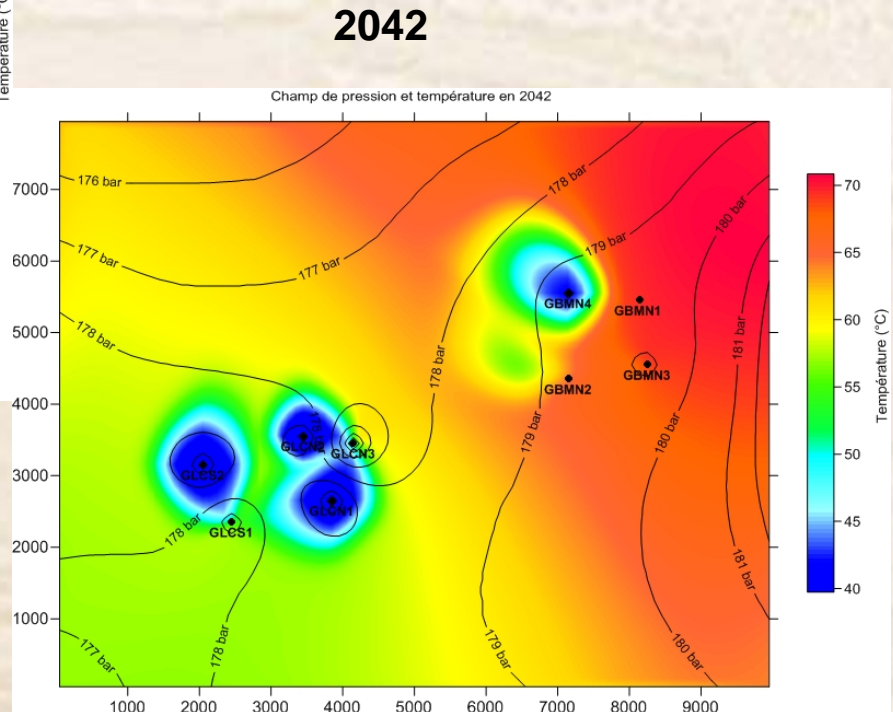
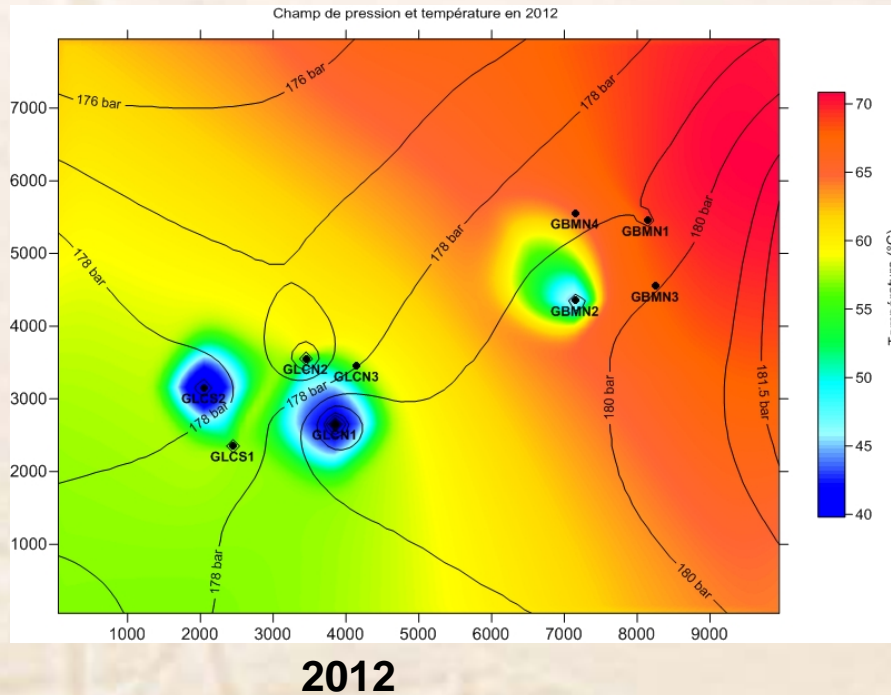
(@ YEAR 1982)





# CASE STUDY GLCN3

## RESERVOIR SIMULATION. BHP & BHT FIELDS (1982-2042)





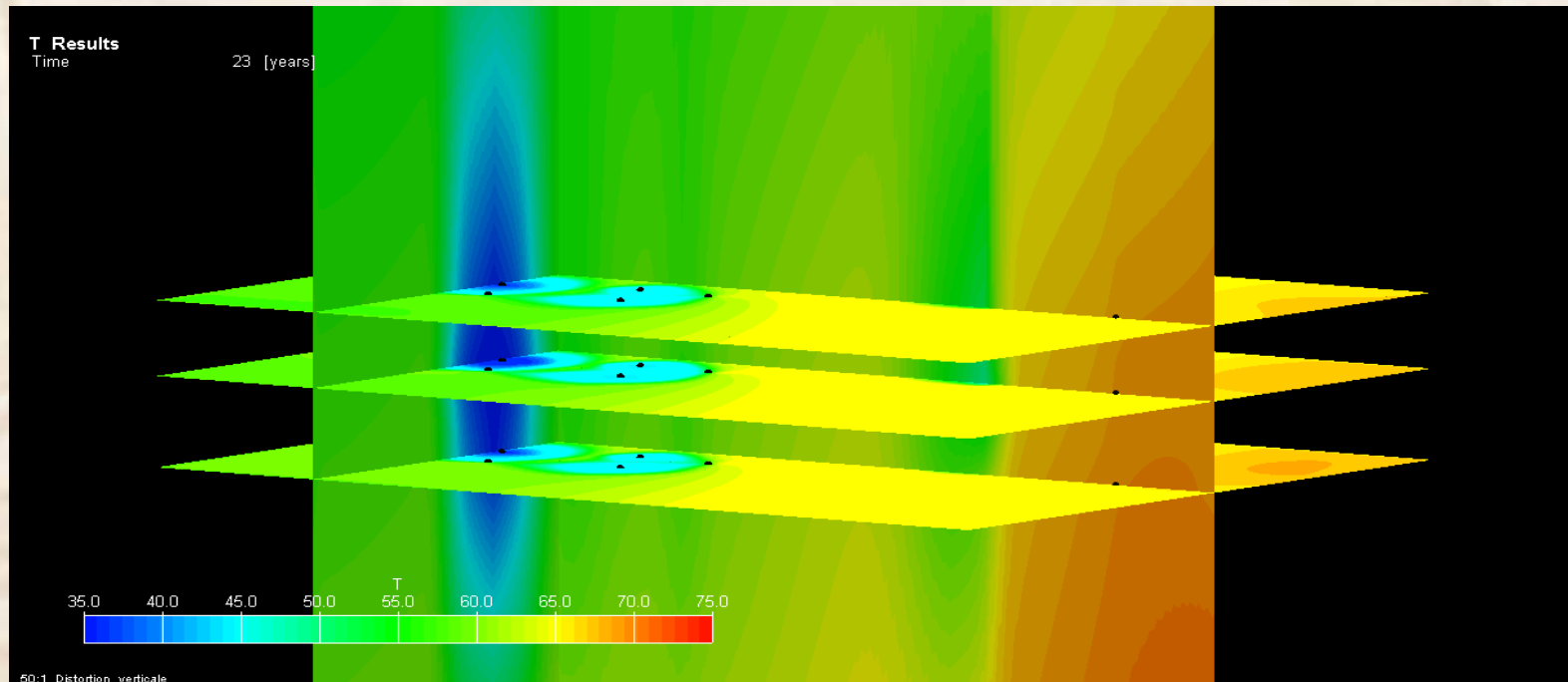
# CASE STUDY

## RESERVOIR SIMULATION



3D display of cooling kinetics (year 2035)  
(280 m<sup>3</sup>/hr)

**Q<sub>nom</sub> = 280 m<sup>3</sup>/h**





# CASE STUDY

## AERIAL VIEW OF GLCN3 DRILL SITE



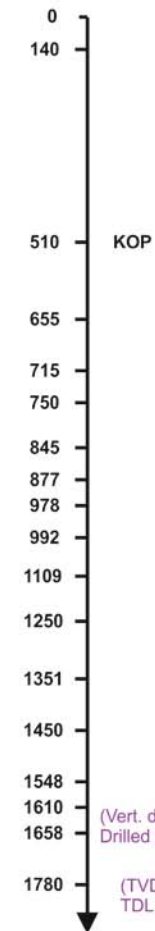


# CASE STUDY

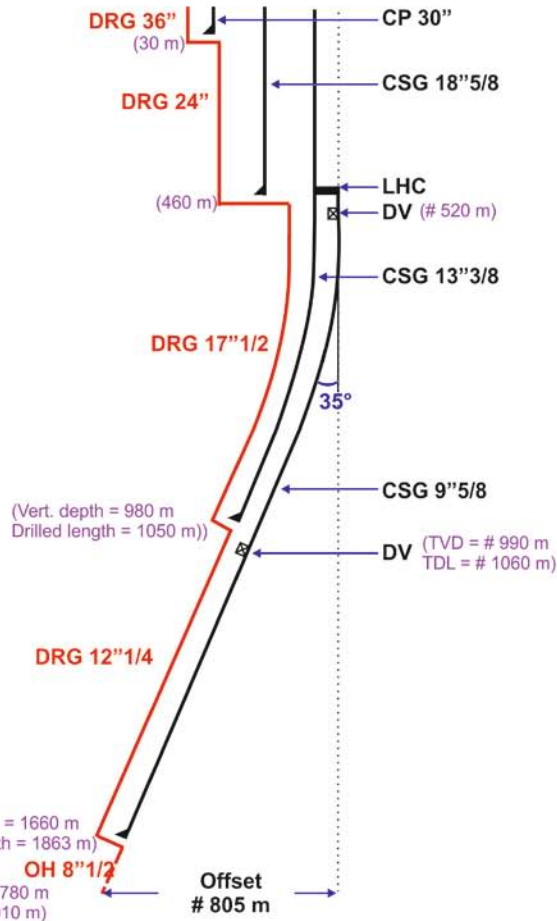
## GLCN3 WELL PROFILE



### VERTICAL DEPTH (m/sol)



### COMPLETION PROFILE WELL ARCHITECTURE



### WIRELINE



OH = openhole  
DV = diverting valve  
DRG = drilling  
CP = conductor pipe  
CSG = casing

BGL: Borehole geometry log  
BHC: Borehole compensated sonic log  
CAL: Caliper log  
CNL: Compensated neutron log  
FMI: Formation micro imager  
GR: Gamma ray  
LDL: Little density log  
CBL-VDL: Cement bond log - Variable density log  
CIC: Casing inspection caliper  
FS: Fluid sampler (bottomhole)  
PLT: Production logging tool  
(temperature, pressure, flowmeter logging)

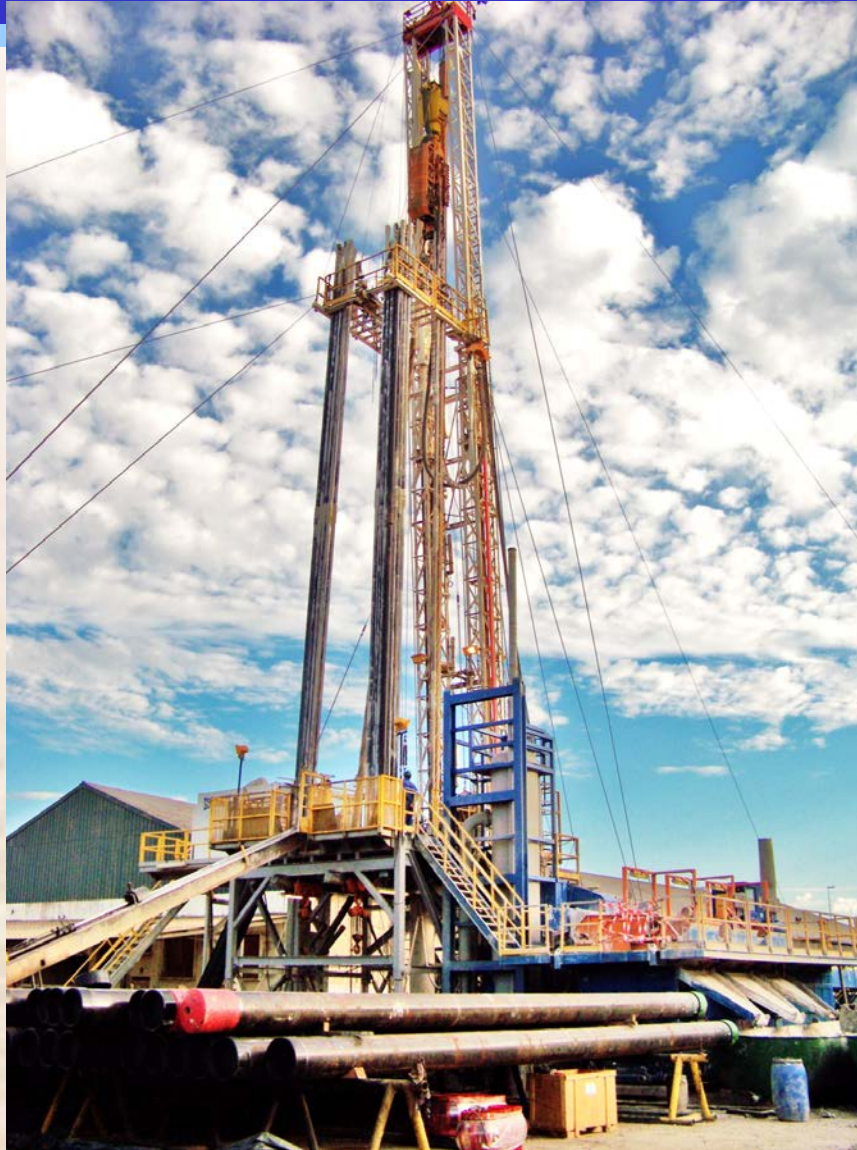
### LITHO-STRATIGRAPHIC SECTION

Stratigraphie		Lithologie des terrains traversés	DOE LCN	CORRELATION GOCAD LCN-LCS-Blanco-Mesnil
3aire	EOCENE	Calcaire, marnes, argiles sableuses.	140	142
CRETACE	SUPERIEUR	SENONIEN		
		Craie blanche à silex.		
	INFERIEUR	TURONIEN		
		Craie gris - blanchâtre +/- compacte		
		CENOMANIEN		
		Calc. glauconneux et marne		
JURASSIQUE	SUPERIEUR	GAULT		
		Argile gris-noir		
		ALBO ARTIEN		
		Sable grossier, jaune-vert, passées d'argiles		
		Argile sableuse		
		NEOCOMIEN		
	MOYEN	PURBECKIEN		
		Calc. oolith.-dolomie		
		PORTLANDIEN		
		Calcaire marneux		
	SUPERIEUR	KIMMERIDGIEN		
		Alternance de marne feuilletée et marne-calcaire		
		SEQUANIEN		
		Calcaire argileux		
		RAURACIEN		
		Calcaire graveleux		
	MOYEN	ARGOVIEN		
		Marnes noires et grises silteuses		
	INFERIEUR	OXFORDIEN		
		Calc. et marnes gréseuse		
		CALLOVIEN		
		Oolith. ferrug. argiles		
		SAVOIEN		
		Alternance de calcaire oolithique, graveleux et micritique		



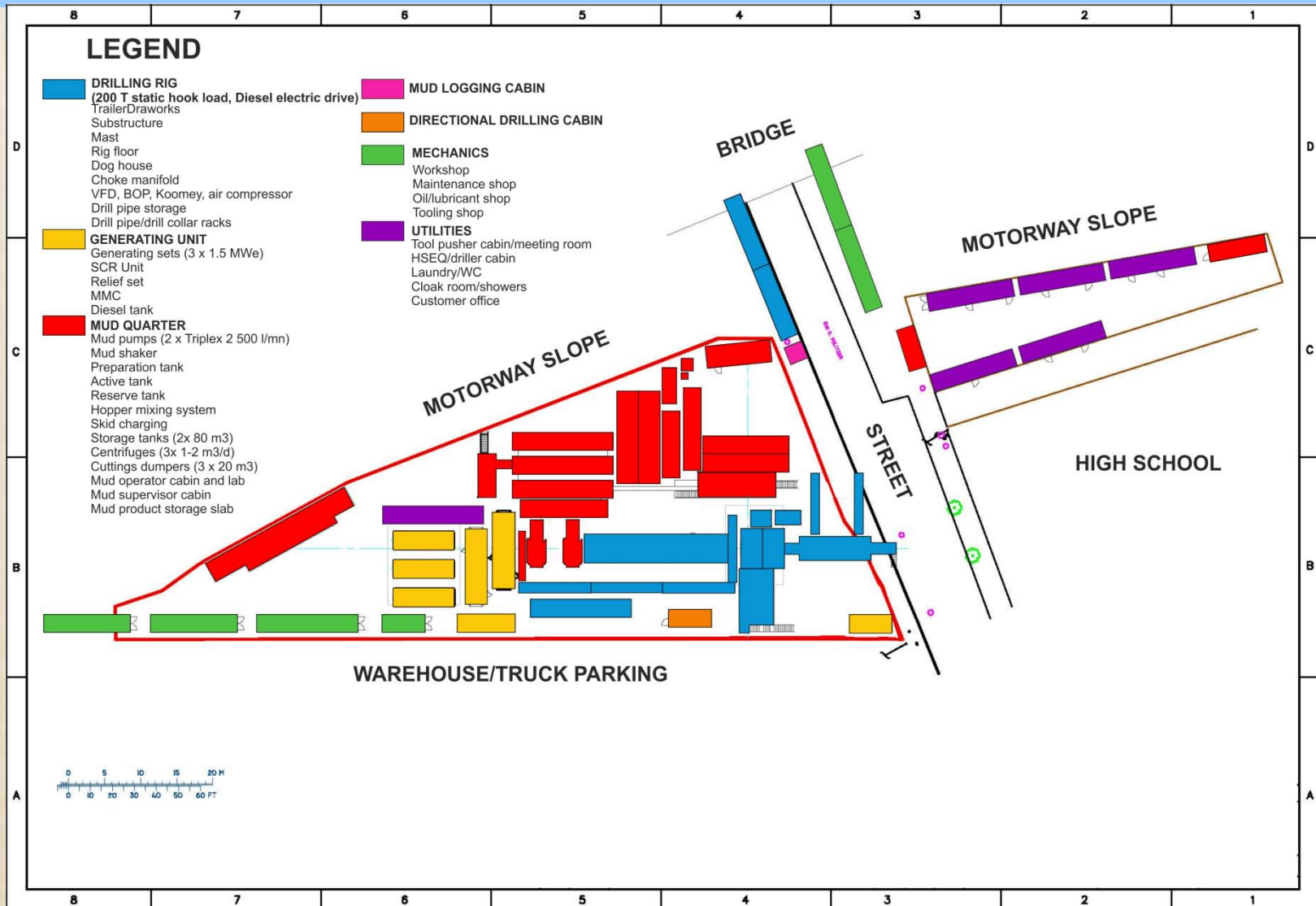
# CASE STUDY

## DRILLING RIG





# CASE STUDY GLCN3 DRILL SITE RIG & EQUIPMENT LAYOUT





# CASE STUDY

## CANDIDATE DRILLING/COMPLETION PROGRAMME



DRILLING PHASES		CASING PHASES						REMARKS
Diameter (")	Drilled interv (mbgl)	Diameter (")	Depths (mbgl) and lengths (m) drilled	Range	Material/grade	Unit weight (lbs/ft)	Thread	
A. STEEL/STEEL COMPLETION								
36	0-30	30	0-30	2	Steel conductor pipe	320.6	ATL	Forewell
24	30-460	18 5/8	0-458	3	K/JSS steel	87.5	BTC	KOP @ 520 mbgl
17 1/2	460-1050	13 3/8	0-1048	3	K/JSS steel	54.5	BTC	Cut@ # 450 mbgl 2 DV@ # 1060 & 520 mbgl
12 1/4	1050-1880	9 5/8	0-1878	3	K/JSS steel	43.5	BTC	
8 1/2	1880-2026	OPENHOLE						
B. COMBINED STEEL CASING/FIBERGLASS LINING COMPLETION								
36	0-30	0-30	30	2	Steel conductor pipe	320.6	ATL	Forewell
24	30-460	0-458	18 5/8	3	K/JSS steel	87.5	BTC	KOP @ 520 mbgl Cut@ # 450 mbgl
17 1/2	460-1880	446-1878	13 3/8	3	K/JSS steel	61	BTC	
12 1/4	1880-2026	0-450	13 3/8	2	Epoxy resin armored fiber glass type E	36.5	API 8 RD	
		450-1878	9 5/8	2		16.9	API 8 RD	
		OPENHOLE						



# CASE STUDY GLCN3

## BIT RECORD GLCN3



Bit type	Bit size	Depth start (mbgl)	Depth end (mbgl)	Total length (m)
Drill bit	24"	36	466	430
Drill bit	17"1/2	471	1058	587
PDC bit	12"1/4	1065	1860	795
Drill bit	8"1/2	1849	1990	141



# CASE STUDY

## DRILLING MUD FORMULAE



DRILLING PHASE [diam.(")/interval (mbgl)]	DENSIT Y Sp. Gr	VM <sup>(1)</sup> s/l	FILTR ATE cc/30 mn	YP <sup>(2)</sup> lbs/100" <sup>2</sup>	GELS Os/10 mn	MUD FORMULAE
<b>A. STEEL/STEEL COMPLETION</b>						
24- 0-460	1.15	60-80		25-30	3/15	BBS <sup>(3)</sup>
17 1/2 460-655 (Chalk)	1.20 <sup>(4)</sup>	60-80 <sup>(4)</sup>		18-22 <sup>(4)</sup>		Fresh water + viscous plugs
655-1050	≤ 1.14	50-55	9-8	18-20	3-15	Cellulosic polymer based mud
12 1/4 655-1880	"	"	"	"	"	"
8 1/2 1880-2026	≤ 1.11	45-50	10-8	10-12	2/12	Brine (10g/l eq.NaCl) biopolymer based mud
<b>B. COMBINED STEEL CASING/FIBERGLASS LINING COMPLETION</b>						
24 0-460	1.15	60-80		25-30	3/15	BBS <sup>(3)</sup>
17 1/2 460-655 (Chalk)	1.00 - 1.20 <sup>(4)</sup>	60-80 <sup>(4)</sup>		18-22 <sup>(4)</sup>		Fresh water + viscous plugs
655-1880	≤ 1.14	50-55	9-8	18-20	3/15	Cellulosic polymer based mud
12 1/4 1880-2026	≤ 1.11	45-50	10-8	10-12	2/12	Brine (10g/l eq.NaCl) biopolymer based mud

<sup>(1)</sup> VM = Marsh viscosity

<sup>(2)</sup> YP = Yield point

<sup>(3)</sup> BBS = Simple bentonitic mud

<sup>(4)</sup> = Viscous plug rhéology



# CASE STUDY CEMENTING



Drilled interval (mbgl)	Diameter (")	Casing diameter (")	Unit volume (l/m)	Total volume (l)	Cement (*) (t)	Water (m³)	
A. STEEL-STEEL COMPLETION							
0	460	24	18 5/8	116.1	53 406,0	45,07	32,15
				108.02 (460-1050 m);			
460	1050	17 1/2	13 3/8	112.76 (0-460 m)	95 605,6	80,69	57,55
				29.1 (1050-1880 m);			
1050	1880	12 1/4	9 5/8	33.70 (520-1050 m)	42 014,0	35,46	25,29
TOTAL				191 025,6	161,22	114,99	
B. STEEL CASING-FIBERGLASS LINING COMPLETION							
0	460	24	18 5/8	116.1	53 406,0	45,07	32,15
460 (*) Class G cement	1880	17 1/2	13 3/8	108.02	153 644	129,68	92,49
TOTAL				207 050,0	174,75	124,64	



# CASE STUDY

## WIRELINE LOGGING PROGRAMME



TOOL(S)	DRILLING PHASE	INTERVAL (mbgl)	CASED PHASE	INTERVAL (mbgl)	REMARK(S)
<b>A. STEEL/STEEL COMPLETION.</b>					
GR/BGL	24	0-460			
GR/BGL	17 1/2	460-1050			o BGL aims at refining cement volume estimates
CBL-VDL/CIC			13 3/8	0-1048	
GR/BGL	12 1/4	1050-1880			o HRT to be performed at the end of pressure build up
CBL-VDL/CIC			9 5/8	450-1878	
GR/LDL/BHC					
CAL/FMI	8 1/2	1880-2020			o Pressure gauge and fluid sampler set 10 m below last casing shoe
FS/PLT/HRT	8 1/2	# 1890			
<b>B. COMBINED STEEL CASING/FIBERGLASS LINING COMPLETION.</b>					
GR/BGL	24	0-460			
GR/BGL	17 1/2	460-1050			o Same as for completion A
CBL-VDL/CIC			13 3/8	0-1880	
GR/LDL/BHC					
CAL/FMI	12 1/4	1880-2020			
FS/PLT/HRT	12 1/4	# 1890			

### Nomenclature:

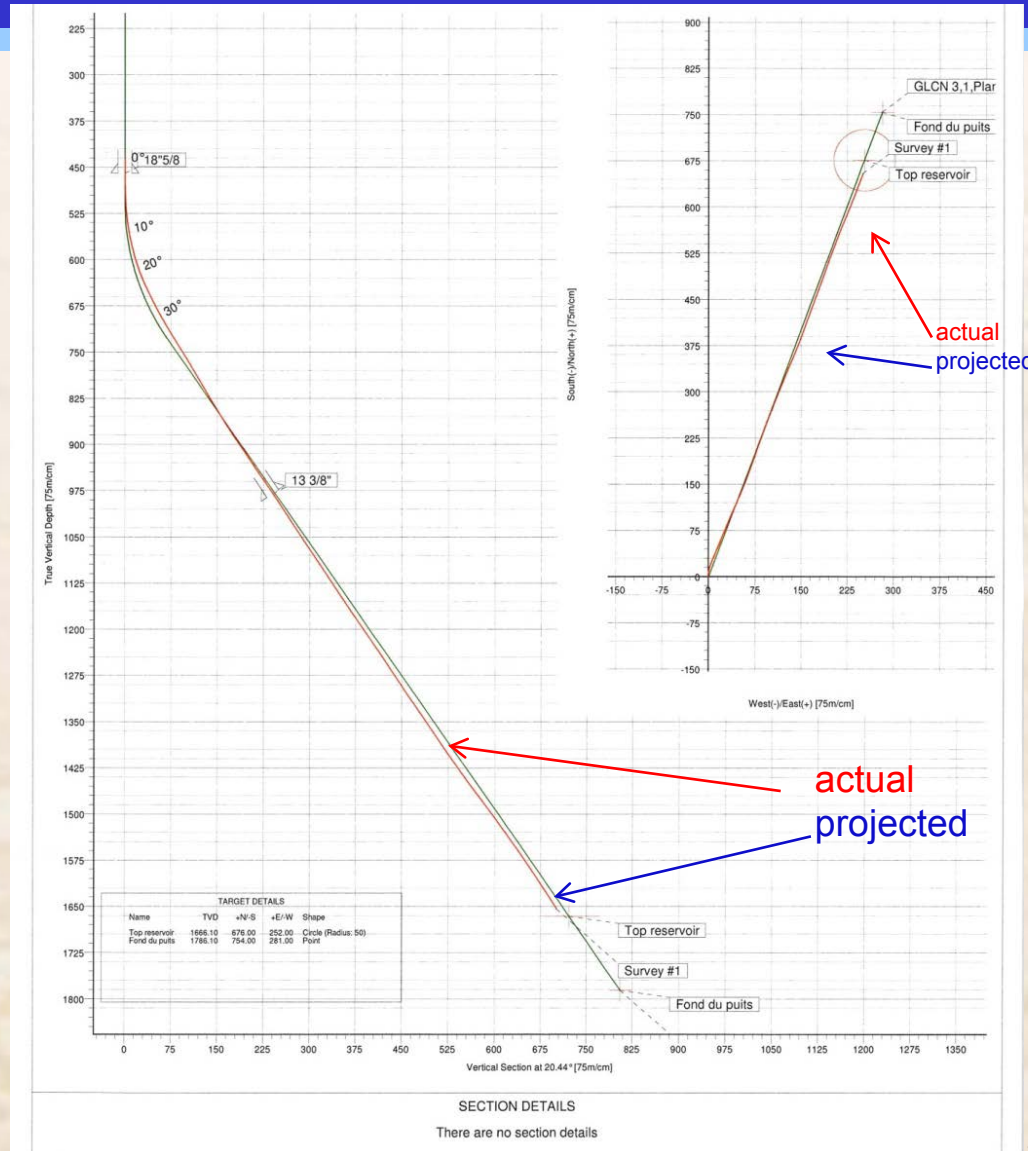
GR = Gamma Ray  
 BGL = Borehole Geometry Log  
 CBL-VDL = Cement Bond Log - Variable Density Log  
 CIC = Casing Inspection Caliper

CAL = Caliper (OH)  
 LDL = Lithodensity Log  
 BH = Borehole Compensated C (Sonic)  
 FMI = Formation Micro Imager

FS = Fluid Sampler  
 = Production Logging Tools  
 PLT (flowmeter, pressure/temperature gauges)  
 HR T = High Resolution Thermometer



# CASE STUDY GLCN3 WELL TRAJECTORIES

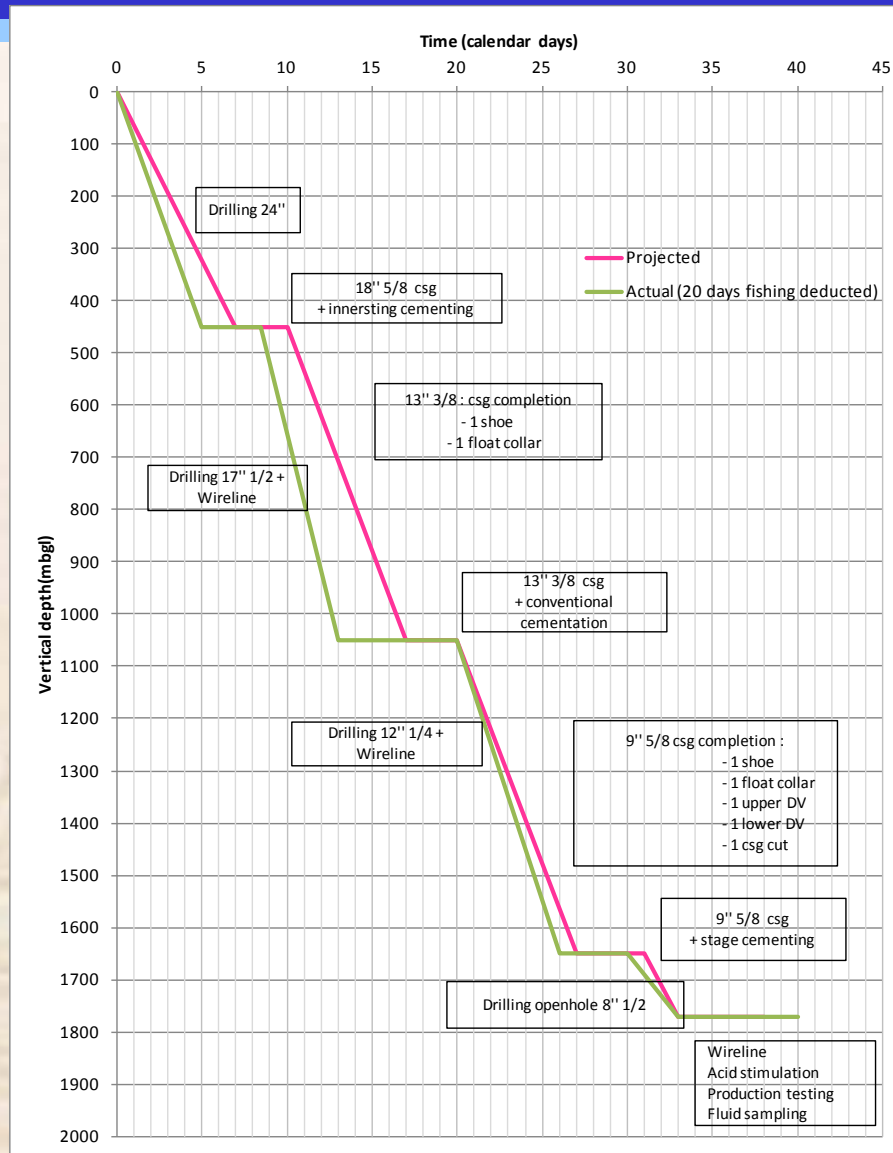


Source : WEATHERFORD



# CASE STUDY

## PROJECTED VS ACTUAL DRILLING TIME CHART





# CASE STUDY GLCN3

## DIRECTIONAL DRILLING BHAs



DIRECTIONAL DRILLING BHAs



Directional drilling  
(drill bit 17"1/2)



Directional drilling  
(PDC bit 12"1/4)

Directional drilling (drill bit 17"1/2)	Directional drilling (PDC bit 12"1/4)
Drill bit 17"1/2	PDC bit 12"1/4
Motor pump	Motor pump
Float sub	MWD tool carrier
Measurement while drilling (MWD) tool carrier	MWD emitting sub
MWD emitting sub	NMDC 9"1/2
Non magnetic drill collars (NMDC) 9"1/2	2 x DC 8 "1/4
2 x Drill collars (DC) 8 "1/4	8 x DC 6"3/4
9 x DC 6"3/4	4 x HWDP 5"
4 x Heavy weight drill pipe (HWDP) 5"	Hydraulic jar
Hydraulic jar	9 x HWDP 5"
9 x HWDP 5"	DP 5"
Drill pipes (DP) 5"	



# CASE STUDY GLCN3

## FISHING BHAs



Imprint 12"



Junk mill 17"1/2



Taper mill 17"1/2

Imprint 12"	Junk mill 17"1/2	Taper mill 17"1/2
Imprint 12"	Junk mill 17"1/2	Taper mill 17"1/2
2 x DC 6"3/4	2 x DC 8 "1/4	1 x DC 8 "1/4
4 x HWDP 5"	9 x DC 6"3/4	Stabilizer
Hydraulic jar	4 x HWDP 5"	1 x DC 8 "1/4
9 x HWDP 5"	Hydraulic jar	2 x DC 6"3/4
DP 5"	9 x HWDP 5"	4 x HWDP 5"
	DP 5"	Hydraulic jar
		9 x HWDP 5"
		DP 5"



Magnet tool 10"



Casing cutter



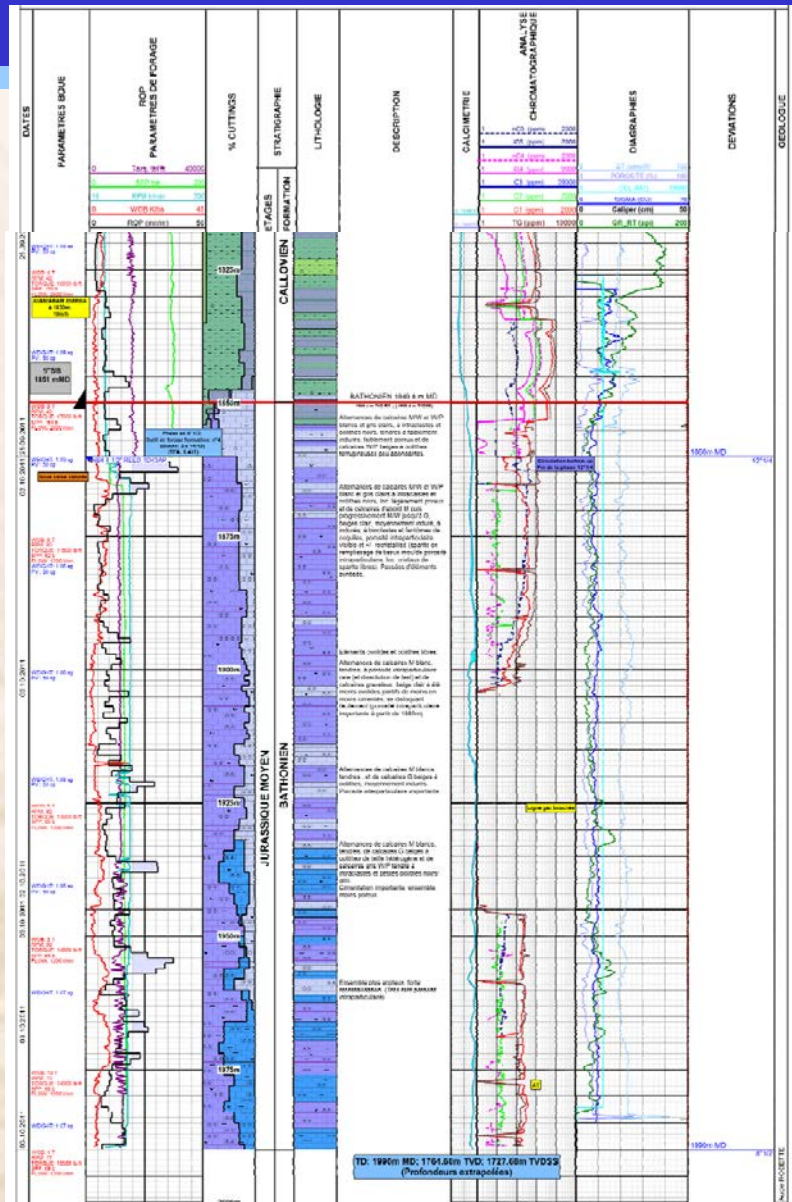
Casing spear

Magnet tool 10"	Casing cutter	Casing spear
Magnet tool 10"	Casing cutter	Casing spear
1 x DC 8 "1/4	4 x HWDP 5"	DP 5"
Stabilizer	Hydraulic jar	
1 x DC 8 "1/4	9 x HWDP 5"	
2 x DC 6"3/4	DP 5"	
4 x HWDP 5"		
Hydraulic jar		
9 x HWDP 5"		
DP 5"		



# CASE STUDY GLCN3

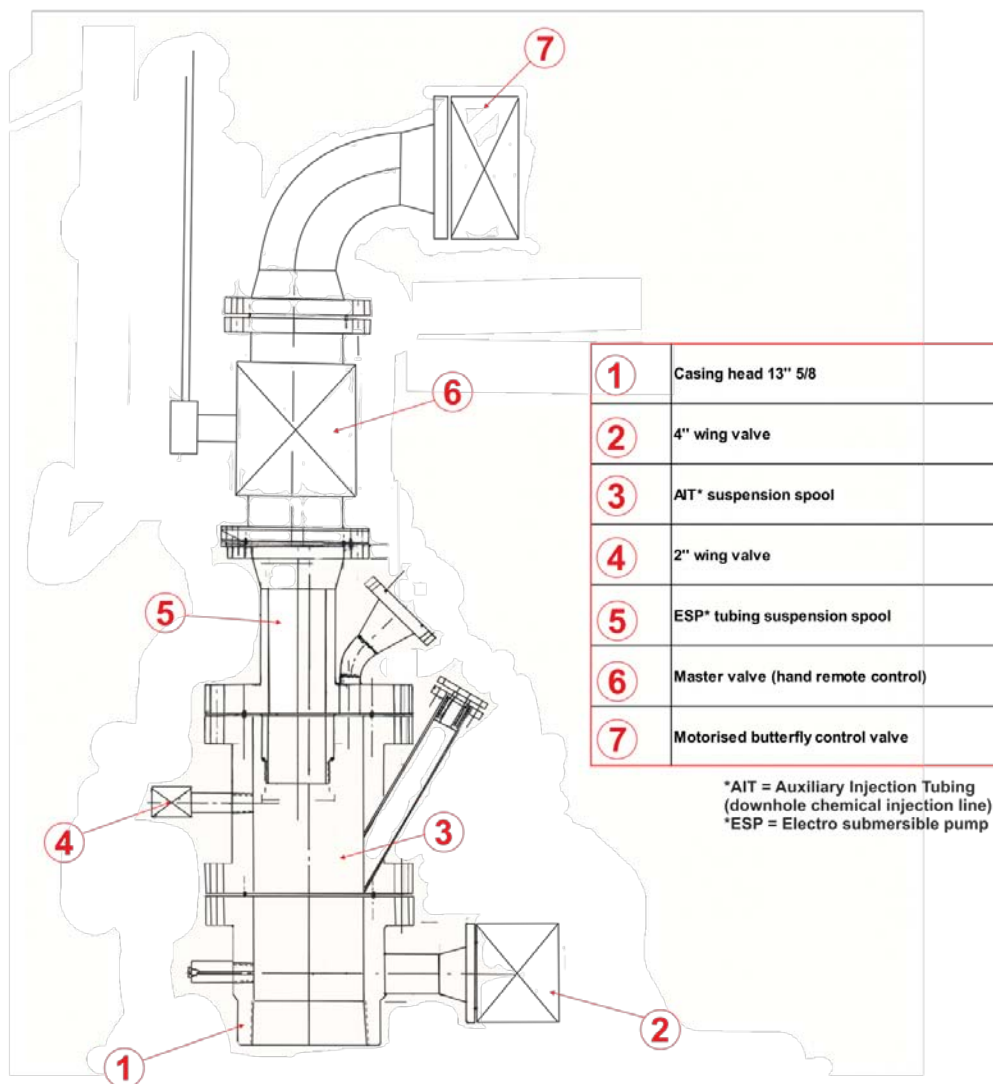
## MUD LOGGING: WELL COMPOSITE LOG OF RESERVOIR SECTION





# CASE STUDY GLCN3

## PRODUCTION WELL HEAD DESIGN





# CASE STUDY

## STIMULATION – PRODUCTION TESTING – FLUID SAMPLING



### (i) Acid stimulation :

- Run drill string to (9"5/8 or 13"3/8) casing shoe,
- Squeeze fresh water to reactivate the well,
- Shut in BOP,
- Pump 20 m<sup>3</sup> of (passivated) HCl 15X,
- Fresh water flush (20 m<sup>3</sup> + dp volume),
- Wait for acid reaction,
- Open BOP,
- Free gas bubble escape,
- Produce well in self-flowing mode via the flow line and waste fluid processing line and measure flowrates, pressure and temperatures at well head;

**(ii) Downhole fluid sampling.** Collect two samples @ 1890 mbgl depth (10 m below last casing shoe);

### (iii) Production testing 1

Run flowmeter/temperature log through drill string to monitor reservoir producing zones, well (self) flowing

- Well shut in,
- POOH flowmeter/temperature tool and run downhole @ 1890 mbgl depth (10 m below last casing shoe) pressure temperature gauge;

### (iv) Production testing 2 (pressure drawdown and buildup cycles)

- Flow the well, measure flowrates, pressures and temperatures at wellhead and record bottomhole pressures and temperatures (duration 8 hrs) (MDH interpretation),
- Shut in well,
- Record (duration 12 hrs) bottomhole pressure buildup (Horner interpretation).



# PARIS BASIN GDH DOUBLET

## TYPICAL COST BREAKDOWN (10<sup>3</sup>€)



Ca 40% of CAPEX

### CAPEX

Mining	min	max
Well drilling/completion	8500	9000
Primary (geothermal) loop	1200	1300
Geothermal heat exchanger	300	400
Total	10000	10700
Surface		
Secondary (grid) loop	600	700
Heat plant	800	900
Grid (piping)	8000	10000
Grid (substations)	2500	3000
Total	11900	14600
<b>GRAND TOTAL</b>	<b>21900</b>	<b>25300</b>

### OPEX

Mining	min	max
P1 Power, chemicals, consummables	200	250
P2 Monitoring, light maintenance	75	90
Heavy duty maintenance, well workover, on duty call	250	300
Miscellaneous	30	50
Total	555	690
Surface		
P1 Power, chemicals	40	50
P2 Heat plant/grid monitoring/maintenance	400	450
P3 Provisions for depreciation	250	350
Miscellaneous	40	60
Total	730	910
<b>GRAND TOTAL</b>	<b>1285</b>	<b>1600</b>

### BREAKEVEN

	WORST CASE	BEST CASE	MEDIUM CASE
CAPEX (10 <sup>3</sup> €)	25000	22000	23000
OPEX (10 <sup>3</sup> €/yr)	1600	1285	1400
SUBSIDY (% CAPEX)	0	35	25
<b>BREAKEVEN (€/MWh<sub>t</sub>)</b>	<b>81</b>	<b>56</b>	<b>64</b>



# OUTLINE



- SCOPE
- INTRODUCTION. GEOTHERMAL VS PETROLEUM
- DEEP WELL DRILLING/COMPLETION FEATURES
  - Rig selection
  - Site preparation. Rig footprint
  - Drilling
  - Bits
  - Drilling fluids
  - Directional drilling
  - Casing/lining
  - Cementing
  - Fishing
  - Waste disposal/processing
- CASE STUDY. PARIS BASIN GDH TRIPLET
- **MEDIUM ENTHALPY CHP EXPLORATION**
  - Deep (4-5 km) exploratory project
  - Slimhole strategy
- UNCONVENTIONAL GEOTHERMAL WELL DESIGNS
  - Dual completion
  - Fiberglass lined anti-corrosion well
  - (sub)Horizontal well concept
- MISCELLANEOUS ISSUES
  - Water injection
  - Mining risk insurance
  - Sustainability
  - Environment
  - Workover
  - Screens
  - Mud solids'control
- DRILLING CONTRACT. RIG MANAGEMENT. WORK SUPERVISION



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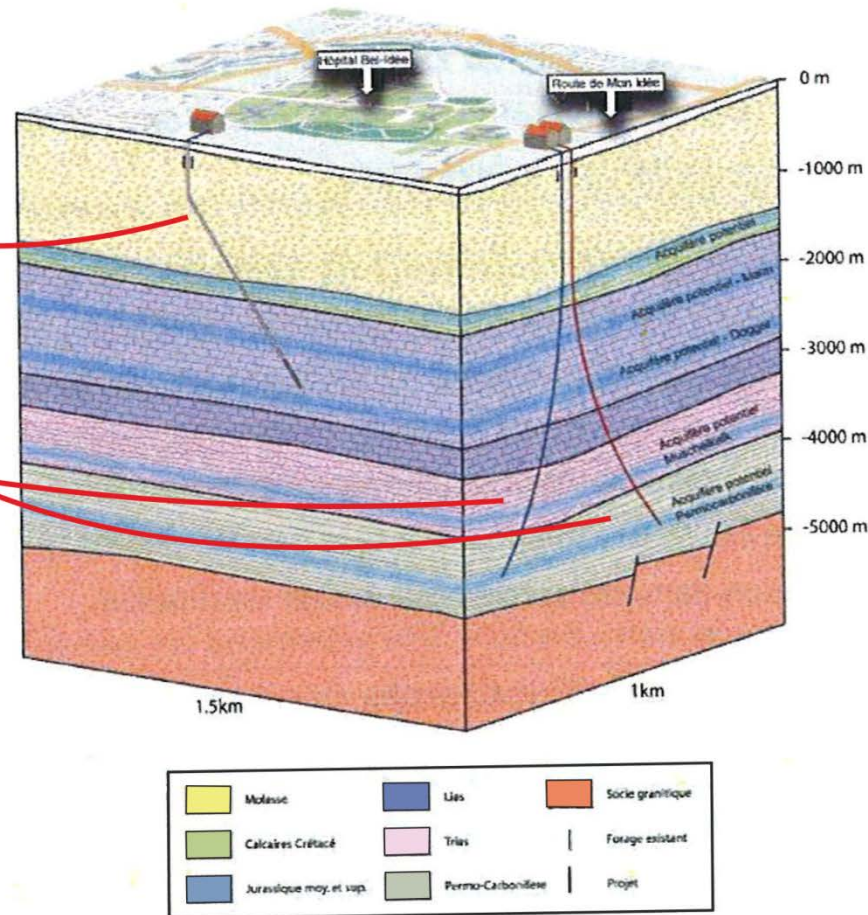
# DEEP DRILLING PROJECT



## Medium enthalpy CHP EXPLO

Existing well

Projected  
(GDH/CHP)  
project



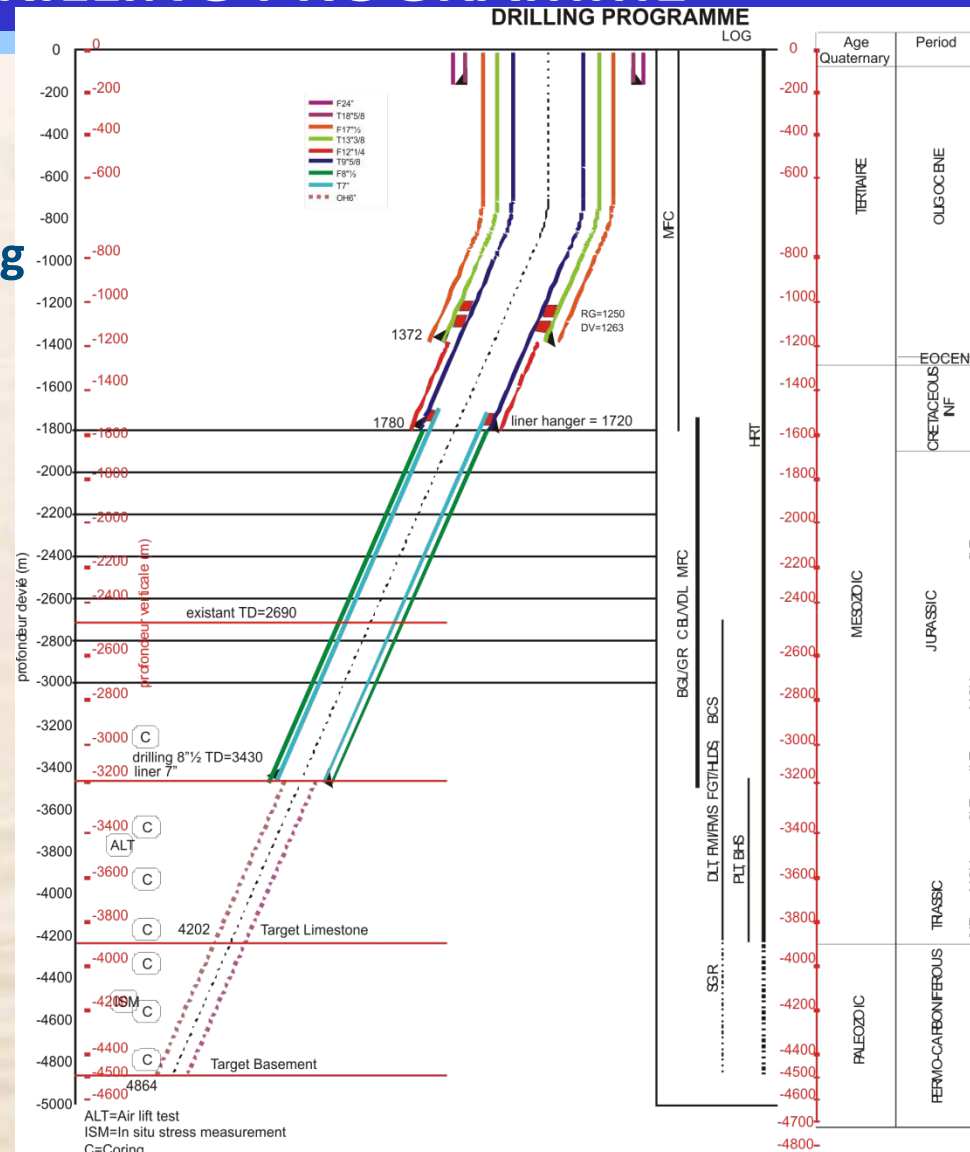
Courtesy : SIG. Geneva.



# DEEP (4-5 km) EXPLORATORY PROJECT DRILLING PROGRAMME



Medium Enthalpy  
(4-5km)  
Deep exploratory drilling





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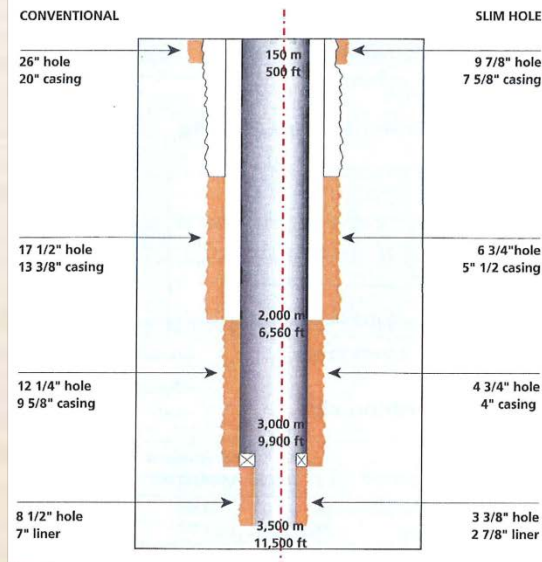
# SLIMHOLE STRATEGY

## Slimhole vs conventional drilling



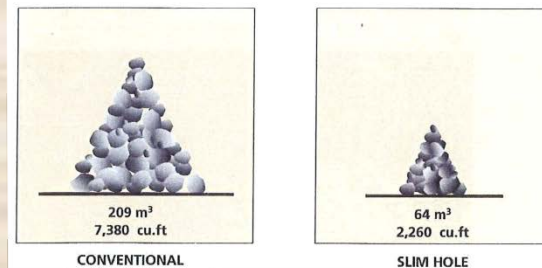
### Technical advantages

Typical 3,500 m (11,500ft) well.  
Slim hole versus conventional.



### Tangible facts:

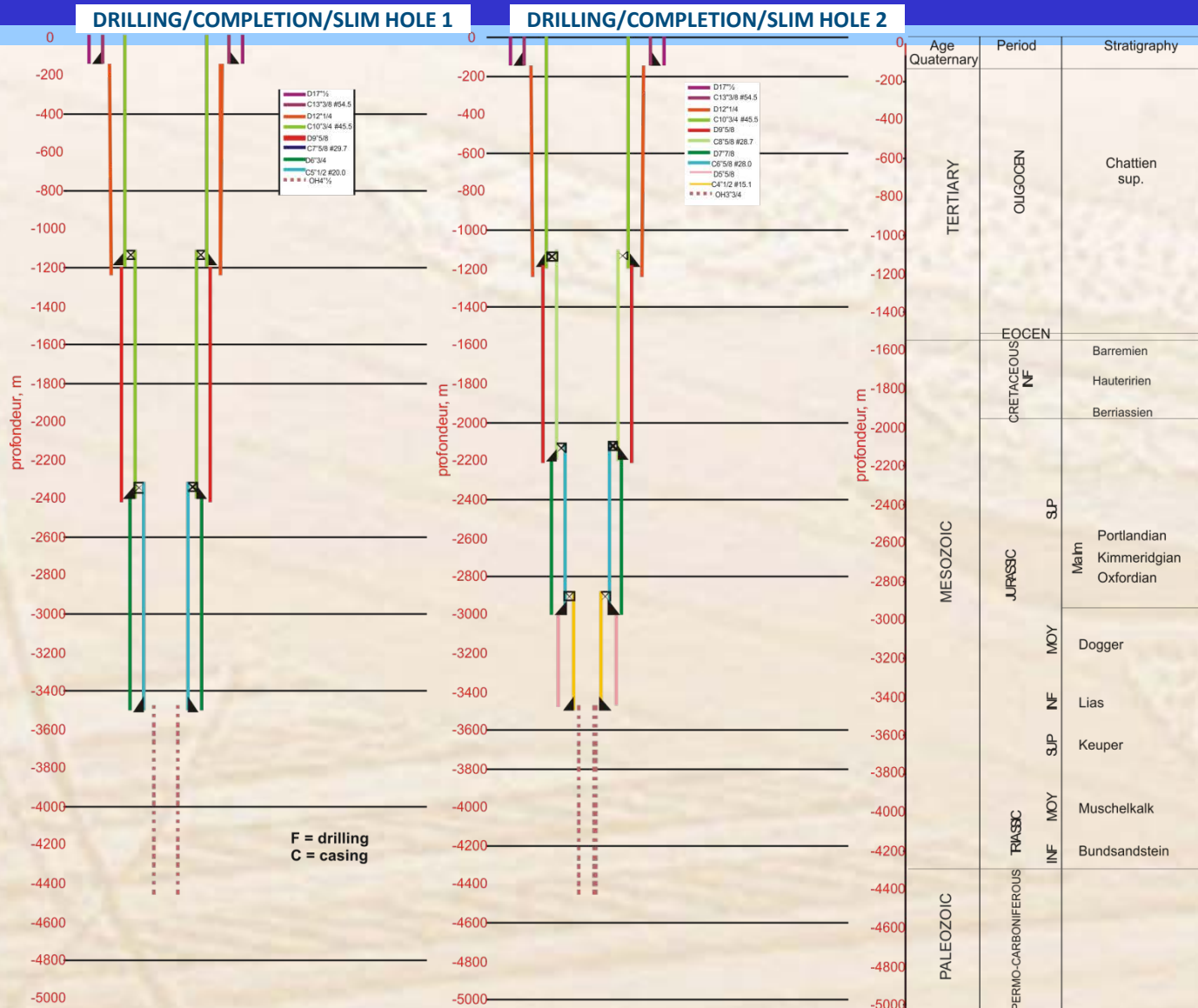
#### 1 - Rocks drilled



SOURCE : FORASOL/FORASLIM



# SLIMHOLE OPTIONS





# SLIMHOLE CONFIGURATION 1



## Casing programme

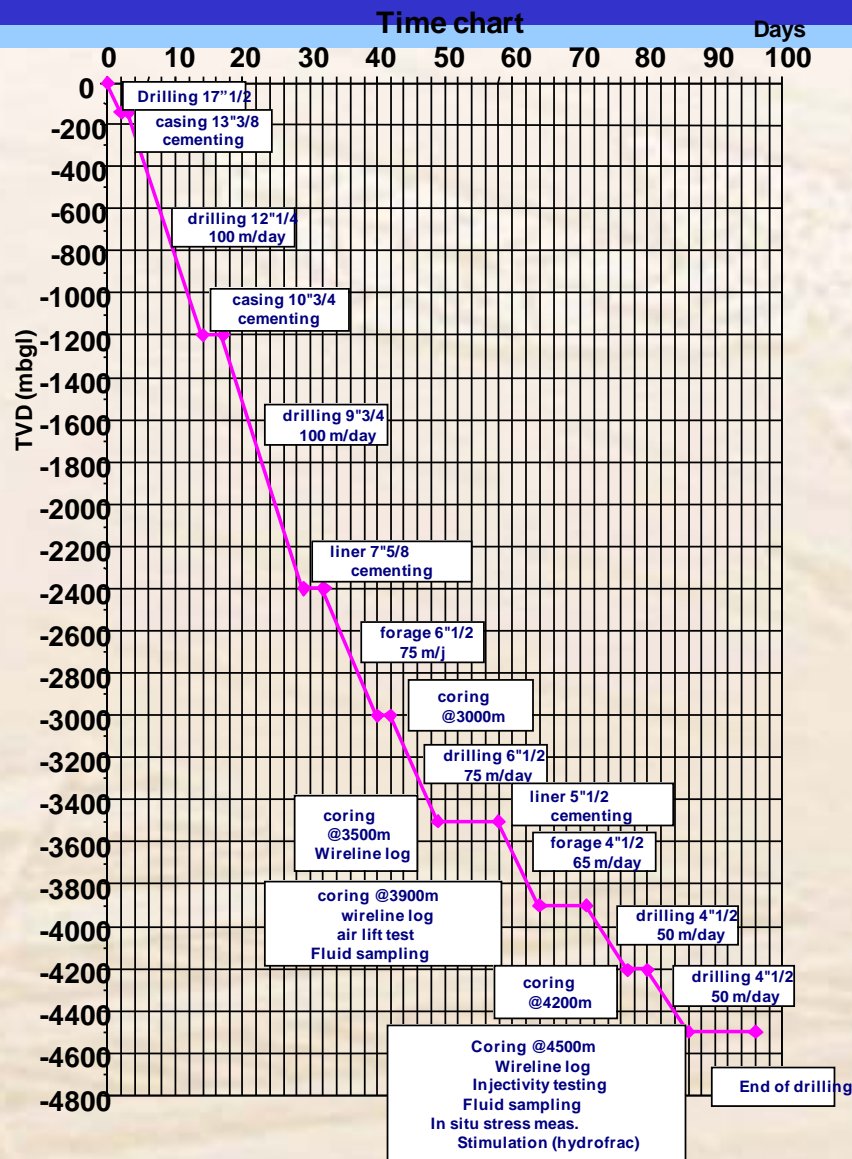
Diameter (OD)"	13 3/8	10 3/4	8 5/8	5 1/2
Interval (mbgl)	0-146	0-1200	1100-2400	2400-3500
Steel grade	K55	K55	K55	K55
Linear weight (lbs/ft)	54.5	45.5	29.7	20
Thread	API	BTC	BTC	BTC
Remark		Float collar @1180 mbgl	Liner hanger (LH) @#2380 mbgl Float valve @#2300 mbgl	Liner hanger (LH) @#2300 mbgl Float valve @#3480 mbgl

## Cementing characteristics

Casing	13 3/8	10 3/4	8 5/8	5 1/2
Interval (mbgl)	0-146	0-1200	1100-2400	2400-3500
Slurry	G, POZZ MIX	G, POZZ MIX	G, POZZ MIX	G, POZZ MIX
Density	1,6-1,65	1,6	1,65	1,6
Volume (m3)	10.4	23.1	25	9.5
Weight (tons)	9.5	21.1	22.8	8.6



# SLIMHOLE CONFIGURATION 1





# SLIMHOLE CONFIGURATION 2



## Casing programme

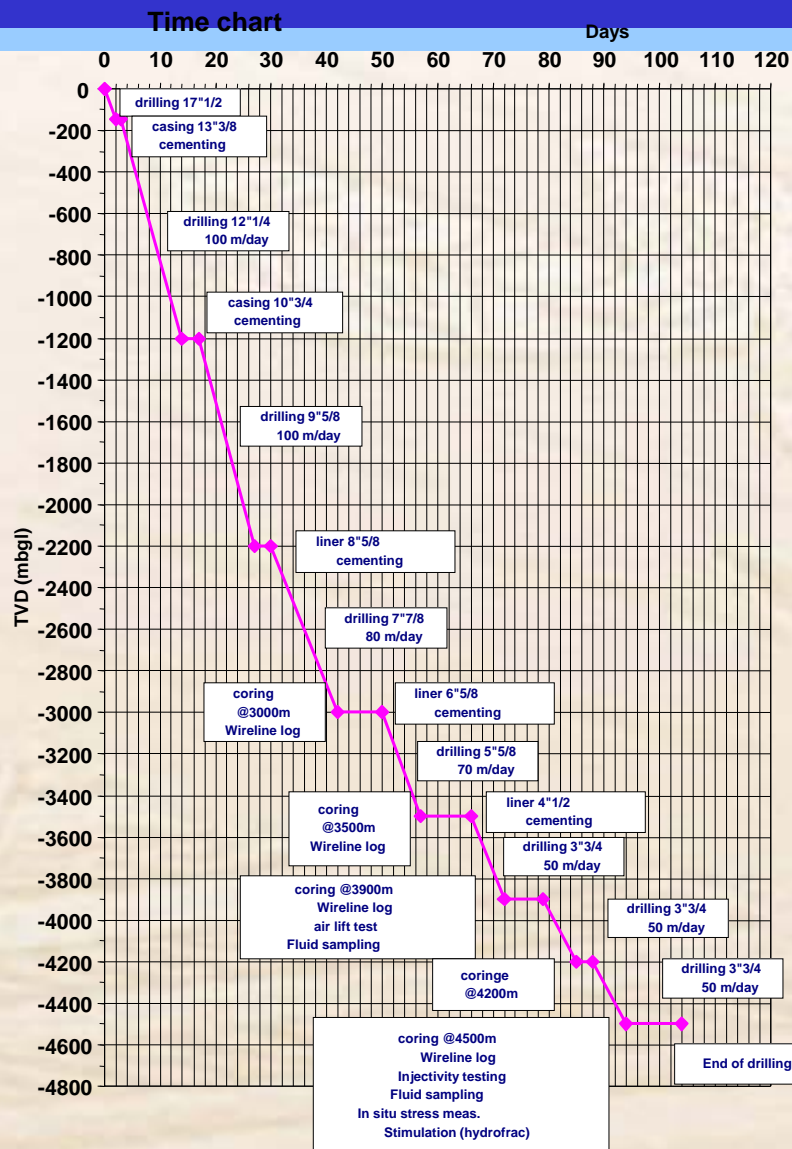
Diameter (OD)"	13 3/8	10 3/4	8 5/8	6 5/8	4"1/2
Interval (mbgl)	0-146	0-1200	1100-2200	2100-3000	3000-3500
Steel grade	K55	K55	K55	K55	K55
Linear weight (lbs/ft)	54.5	45.5	28.7	28	15.10
Thread	API	BTC	BTC	BTC	
Remark		Float collar @1200 mbgl	Liner hanger (LH) @#2400 mbgl Float valve @#2300 mbgl	Liner hanger (LH) @#2100 mbgl Float valve @#3800 mbgl	Liner hanger (LH) @#2100 mbgl Float valve @#3800 mbgl

## Cementing characteristics

Casing	13 3/8	10 3/4	8 5/8	5 1/2
Interval (mbgl)	0-146	0-1200	1100-2400	2400-3500
Slurry	G, POZZ MIX	G, POZZ MIX	G, POZZ MIX	G, POZZ MIX
Density	1,6-1,65	1,6	1,65	1,6
Volume (m3)	10.4	23.1	25	9.5
Weight (tons)	9.5	21.1	22.8	8.6



# SLIMHOLE CONFIGURATION 2





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  - Workover
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  - Mud solids'control
- DRILLING CONTRACT. RIG MANAGEMENT. WORK SUPERVISION





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# DUAL COMPLETIONS

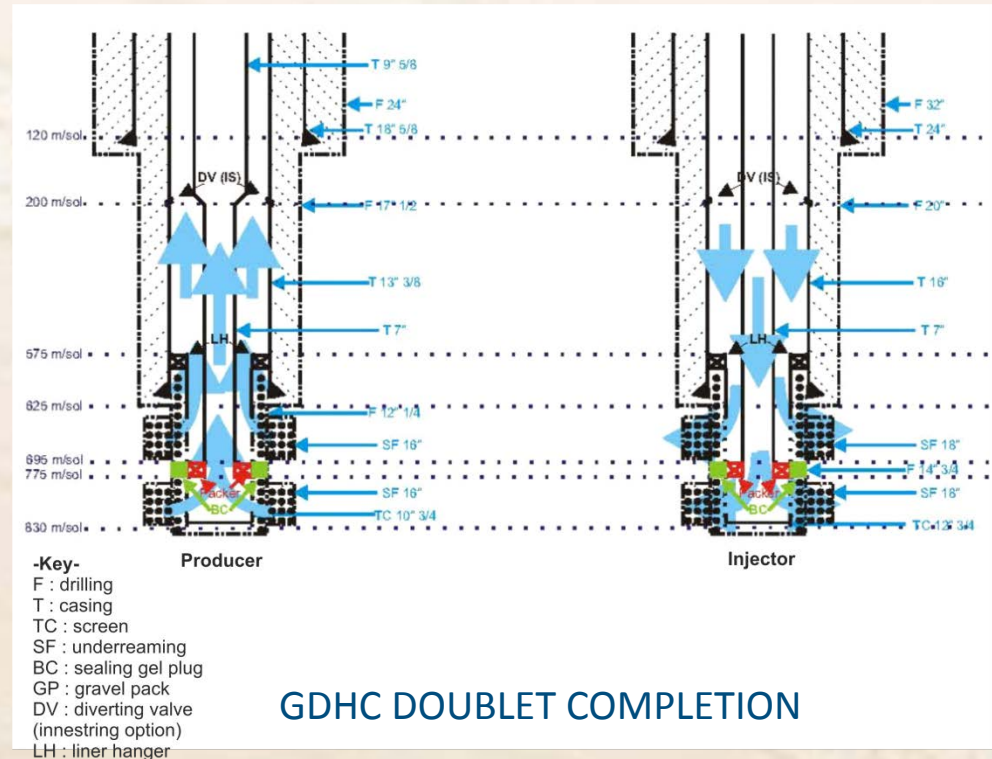
## GEOHERMAL DISTRICT HEATING & COOLING (GDHC)



### Medium depth seated reservoirs

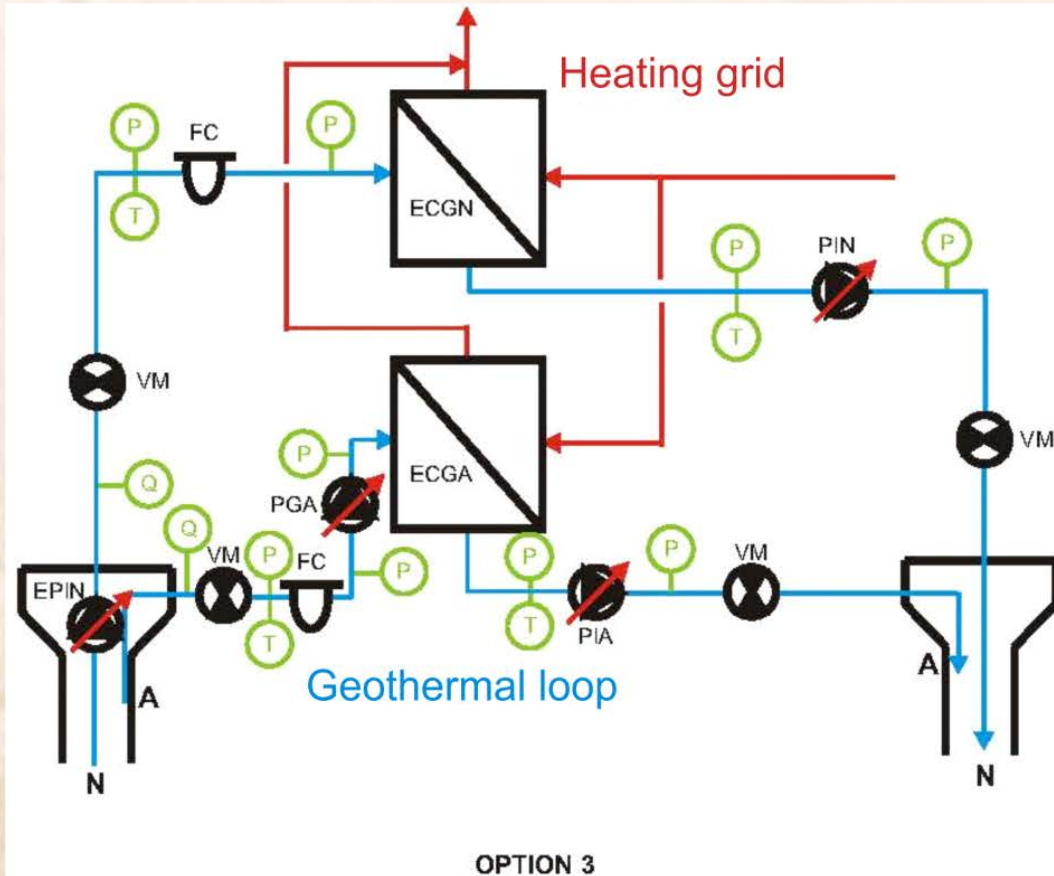
Depth		N°	Thickners (m)	Transmissivity (m <sup>2</sup> /s)
0				
625	Albo-Aptien 1	1	25	$5 \cdot 10^{-3}$
12,5	Aquitard	2	20	$k_v = 15 \text{ mD}$
695	Albo-Aptien 2	1	25	$5 \cdot 10^{-3}$
57,5				
110	Aquitard (Barremien)	3	80	$k_v = 0.1 \text{ mD}$
157,5	Néocomien 1	4	15	$3,5 \cdot 10^{-3}$
775				
175	Aquitard	5	20	$k_v = 5 \text{ mD}$
825	Néocomien 2	4	15	$3,5 \cdot 10^{-3}$
192,5				
200				

### AQUIFER SYSTEM





# DUAL COMPLETIONS GDHC GEOTHERMAL LOOPS



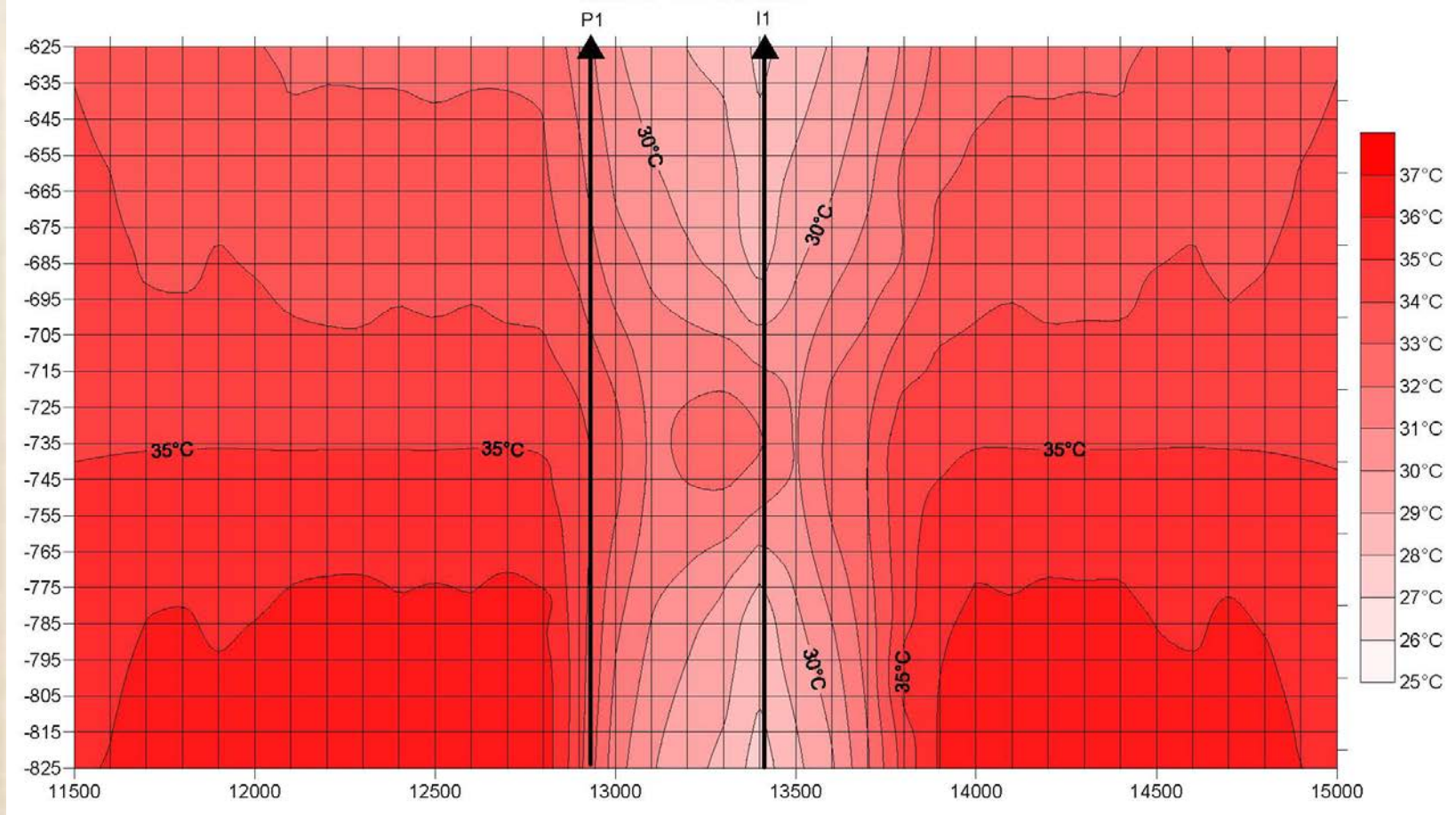
## -Key-

ECGA : geothermal heat exchanger Albian  
 ECGN : geothermal heat exchanger Neocomian  
 EPIA : ESP (Albian)  
 EPIN : ESP (Neocomian)  
 FC : cartridge filter  
 I : injector well  
 PGA : surface boost pump (Albian)  
 PIA : injection pump (Albian)  
 PIN : injection pump (Neocomian)  
 P/Q/T : pressure/flowrate/temperature  
 VM : master valve



# DUAL COMPLETIONS

## MODELLING OF THE GDHC DOUBLET



**VERTICAL TEMPERATURE DISPLAY (YEAR 2030)**



# OUTLINE



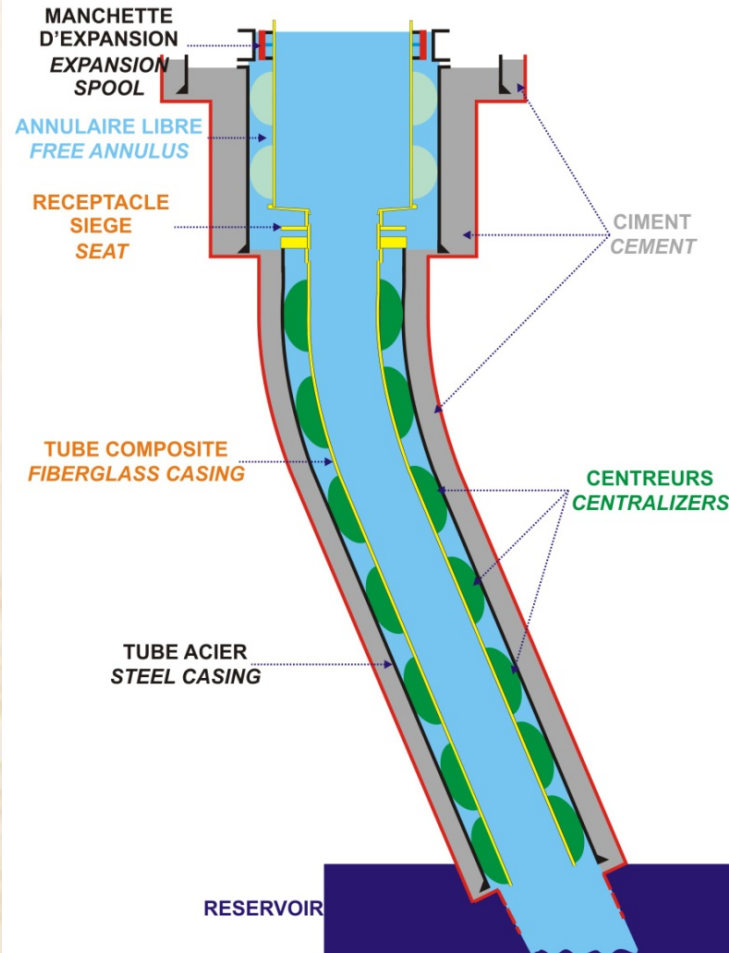
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# ANTI-CORROSION WELL COMPLETION



## PUITS TUBE ACIER/COMPOSITES COMBINED STEEL CASING/FIBER GLASS LINING WELL





# CASING/LINING

## FIBERGLASS CASING/LINER RATINGS (ACT COUPLINGS)



SIZE	Nominal (")	9"5/8 (*)	13"3/8 (**)
TEMPERATURE	Maximum (°C)	93	93
BURST PRESSURE	Rating (bar)	130	140
	STAR Ultimate (bar)	199	182
	Safety margin	1.5	1.3
	Ultimate (ASTM D-1599)	312	280
	Safety margin	2.4	2
TENSILE	Rating (tons)	57	100
	STAR Ultimate (tons)	74	120
	Safety margin	1.3	1.2
COLLAPSE PRESSURE	Rating (tons)	165	140
	STAR Ultimate (ASTM D-2924)	350	280
	Safety margin	2.1	2
NOMINAL DIMENSIONS	ID (mm)	196.6	301.1
	Minimum drift (mm)	192.6	299.3
	OD (mm)	229.9	338.3
	Wall thickness (mm)	16.7	18.6
	Unit mass (daN/m)	24.4	41.8
	Length	9.15 m nominal API range 2, (8.55 to 9.75 m)	
JOINING SYSTEM	Collar OD (mm)	302.26	431.8
	Upset OD (mm)	245.11	355.6
	Thread size (mm)	244.48	339.73
	Thread type	API 8RD	API 8RD
ELASTICITY MODUL	Hoop ( $10^5$ bar)	345	350
	Axial ( $10^5$ bar)	207	210
	Poisson ratio (minimum)	0.25	0.24
PHYSICAL PROPERTIES	Density (kg/m <sup>3</sup> )	196	
	F (W/mK)	0.4	
	Specific heat (Kj/kgK)	1.005	
	Axial expansion (mm/mm/°C)	15.7	
HYDRAULIC PROPERTIES	Rugosity (absolute) (mm)	0.0053	
	Hazen Williams coefficient (C)	150	

(\*) standard

(\*\*) non standard, customised design

Source : STAR FIBERGLASS SYSTEMS



# OUTLINE



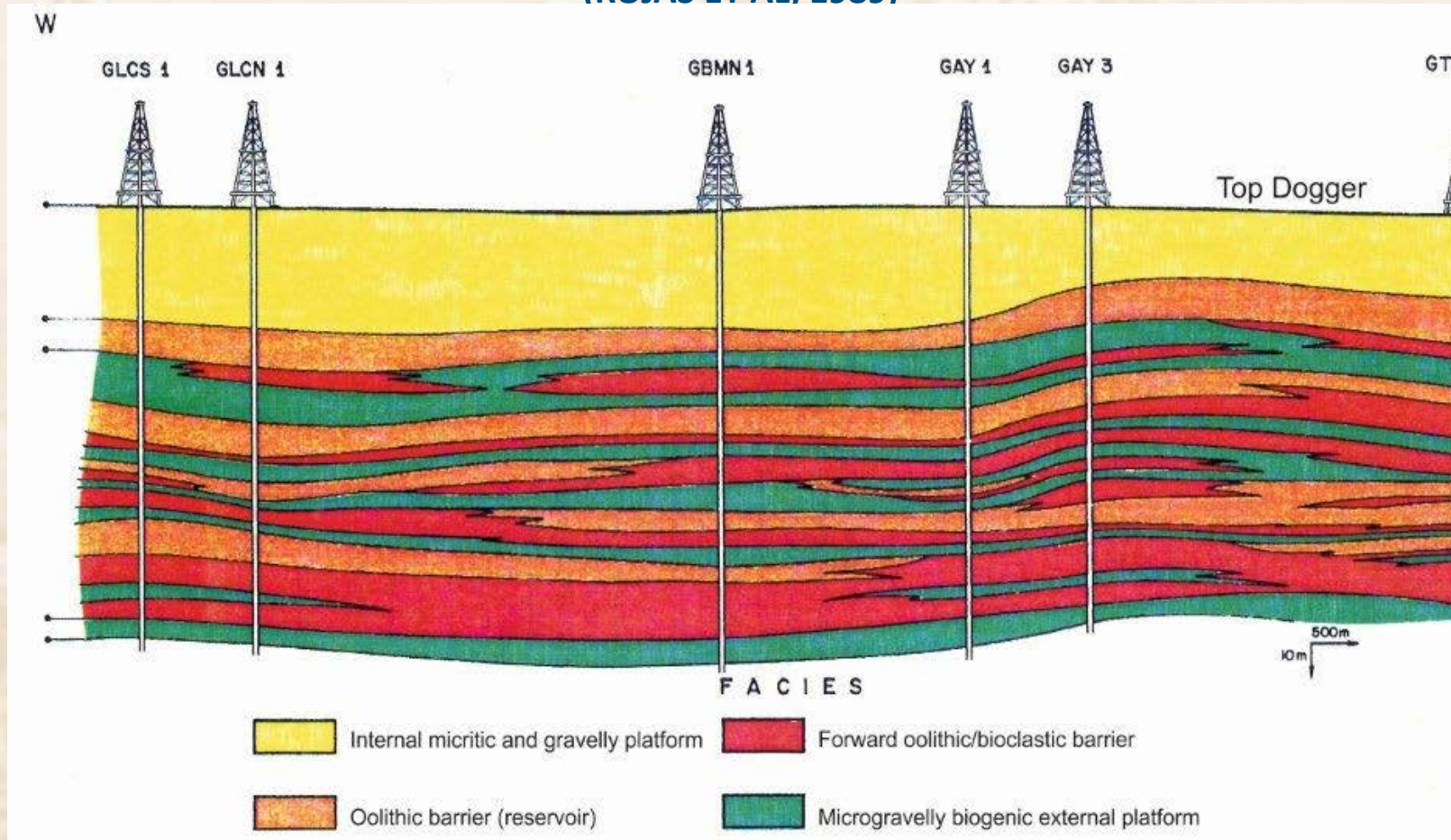
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# (SUB)HORIZONTAL GDH WELL DESIGNS



## MULTILAYERED RESERVOIR STRUCTURE TENTATIVE FACIES CORRELATIONS. NORTHERN AREA (ROJAS ET AL. 1989)

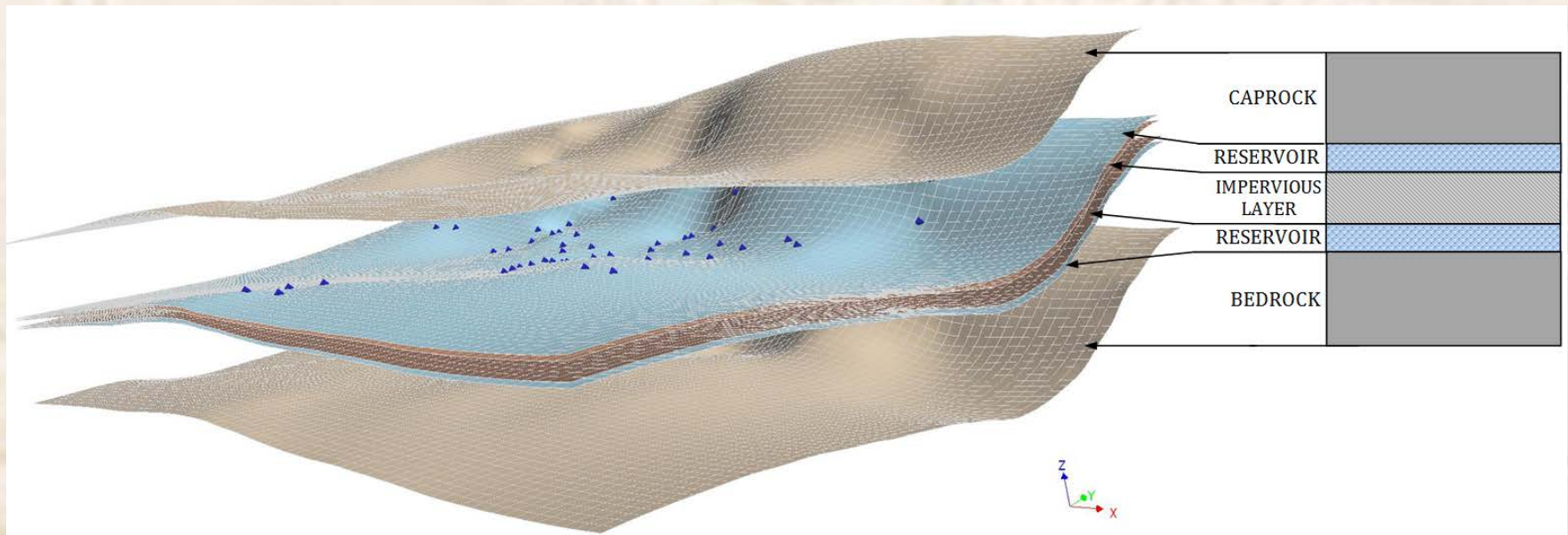




# (SUB)HORIZONTAL GDH WELL DESIGNS



## GOCAD 3D VIEW OF THE SANDWICH HETEROGENEOUS RESERVOIR STRUCTURE

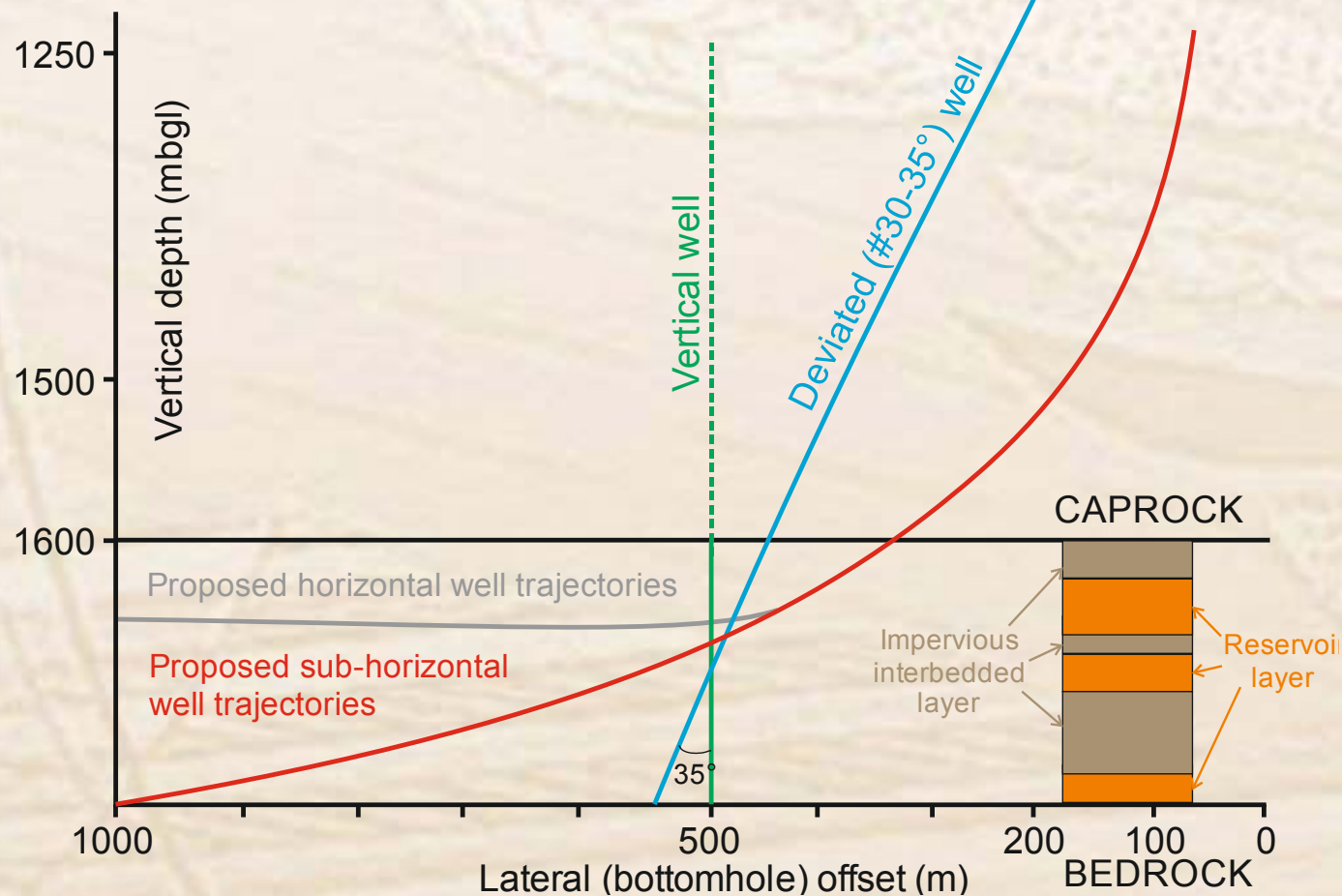




# (SUB)HORIZONTAL WELL DESIGNS



## CANDIDATE WELL TRAJECTORIES MULTILAYERED RESERVOIR CONVENTIONAL (VERTICAL, DEVIATED) AND SUGGESTED [(SUB)HORIZONTAL] WELL TRAJECTORIES

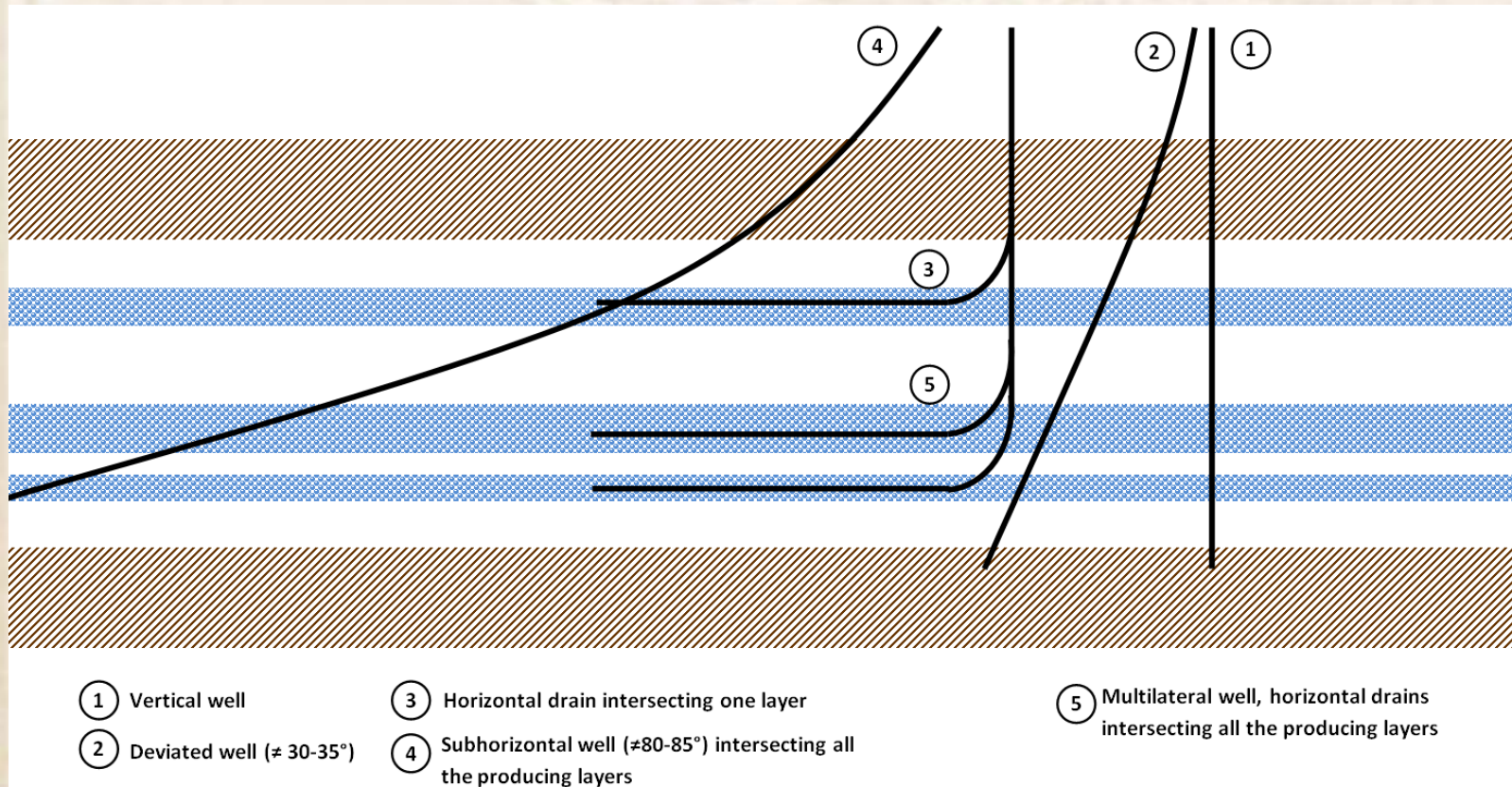




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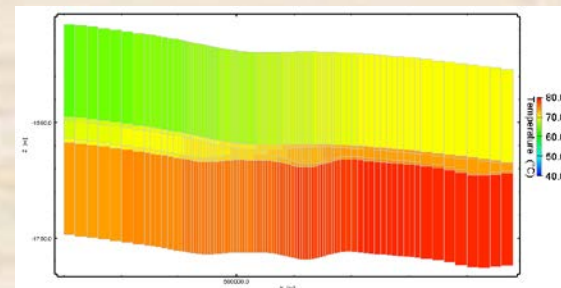
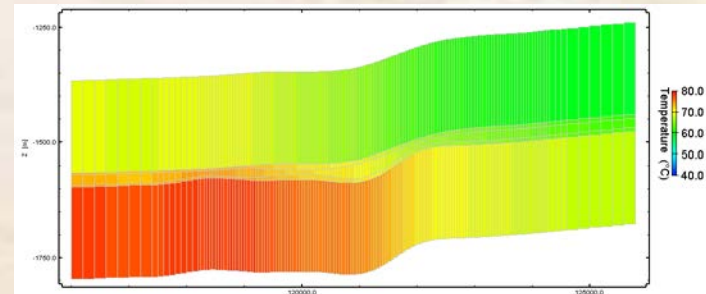
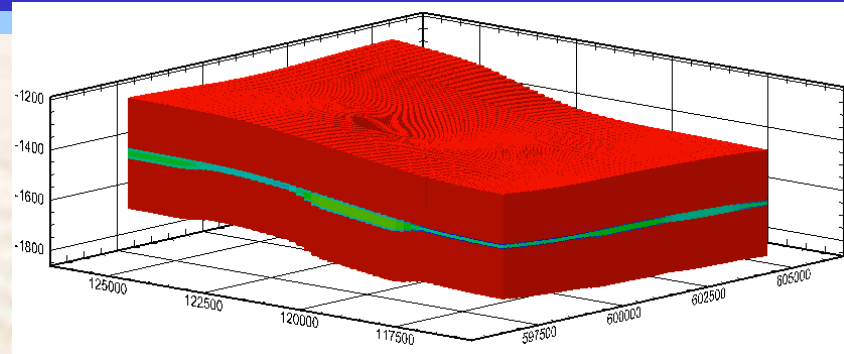
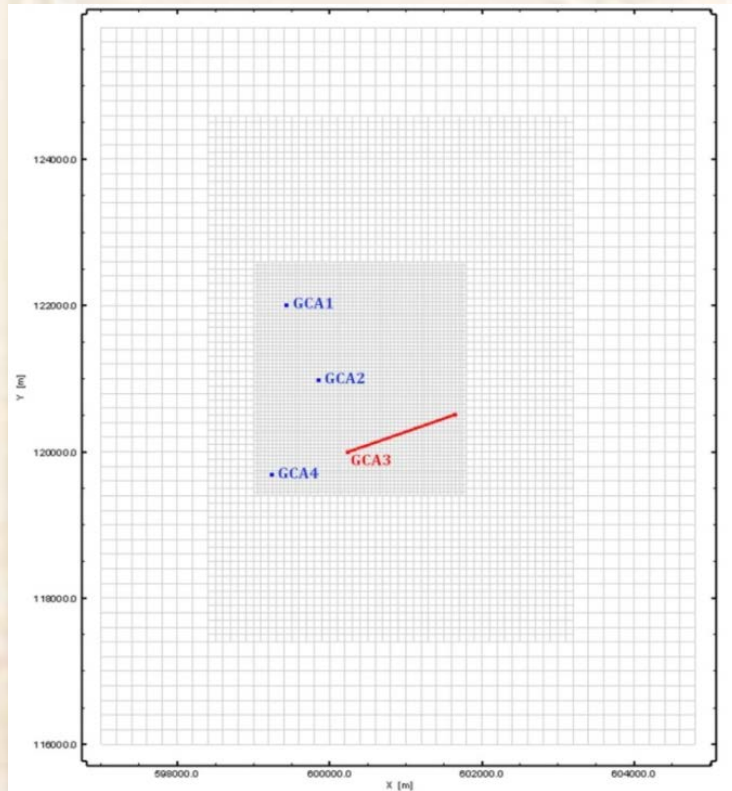




# (SUB)HORIZONTAL WELL MODELLING



## DISCRETISATION GRID



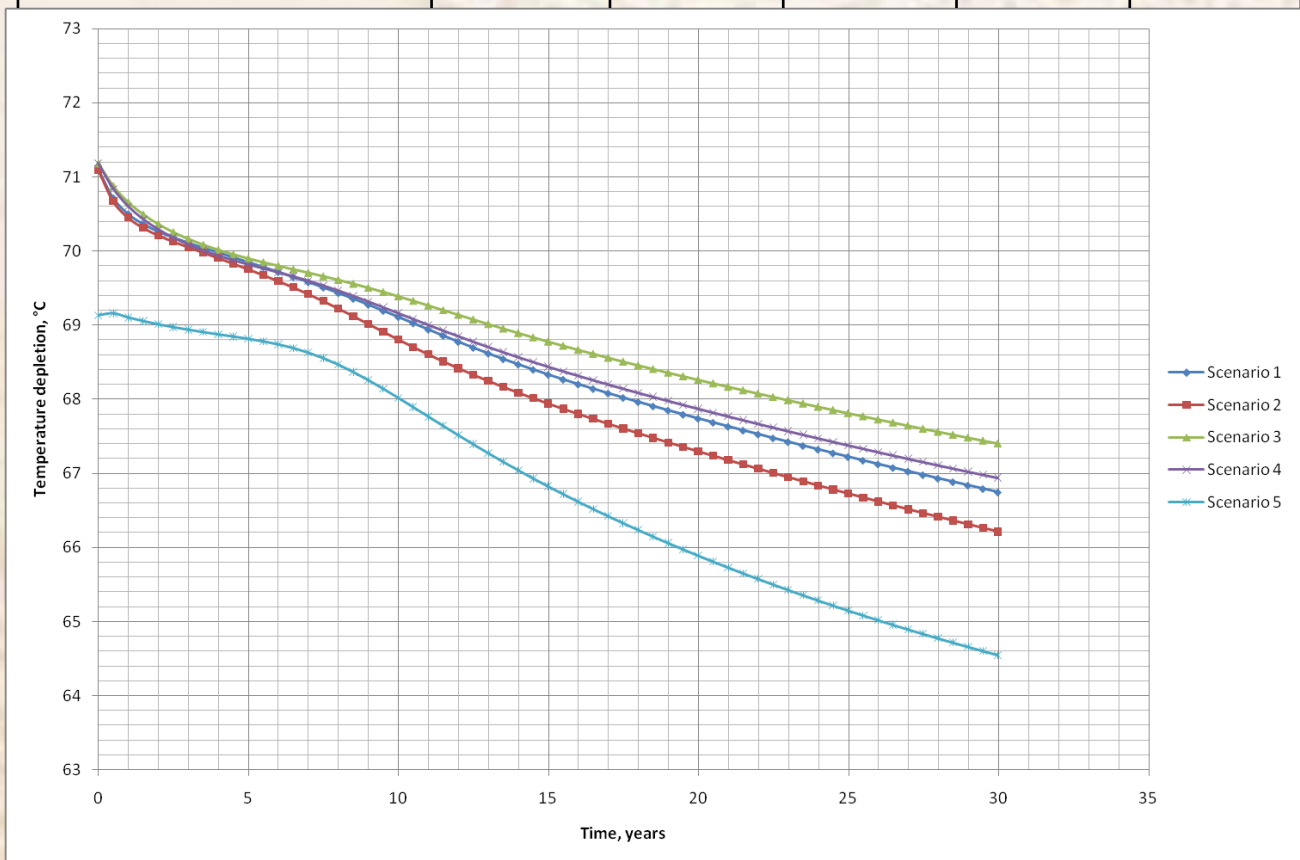


# (SUB)HORIZONTAL WELL MODELLING



## COOLING KINETICS

	Scenario 1	Scenario 2	Scenario 3	Scenario 4	Scenario 5
Well length (meter)	1000	1000	1500	1500	Vertical
Flow rate (m <sup>3</sup> /h)	300	350	300	350	300
Injection temperature (°C)	40	40	40	40	40



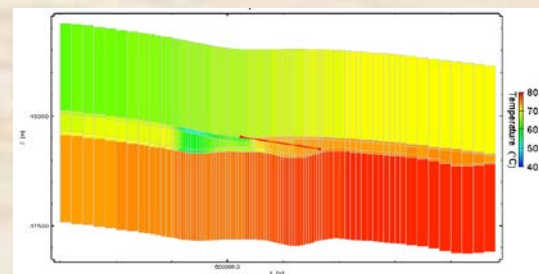
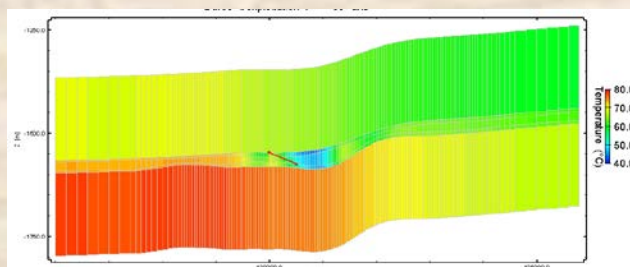
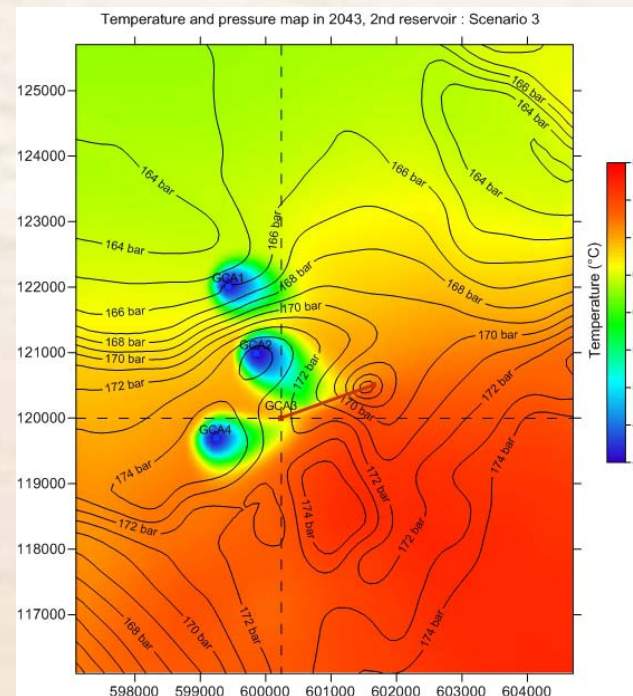
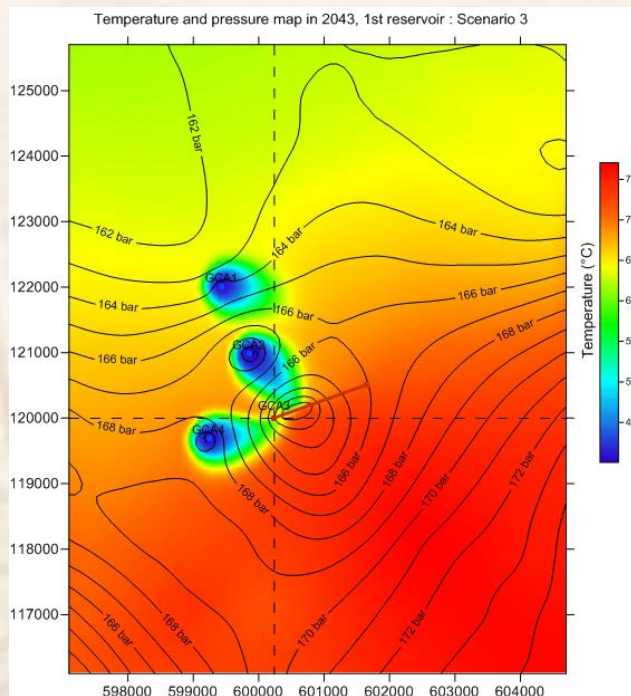


# (SUB)HORIZONTAL WELL MODELLING



## PRESSURE/TEMPERATURE DISPLAYS (YEAR 2043)

### SCENARIO 3







## CONCLUSIONS

(Sub)Horizontal well designs, preferably intersecting the whole pay interbedded sequence, is suggested as a reliable alternative (improved productivities/injectivities and thermal life) to conventional well architectures.



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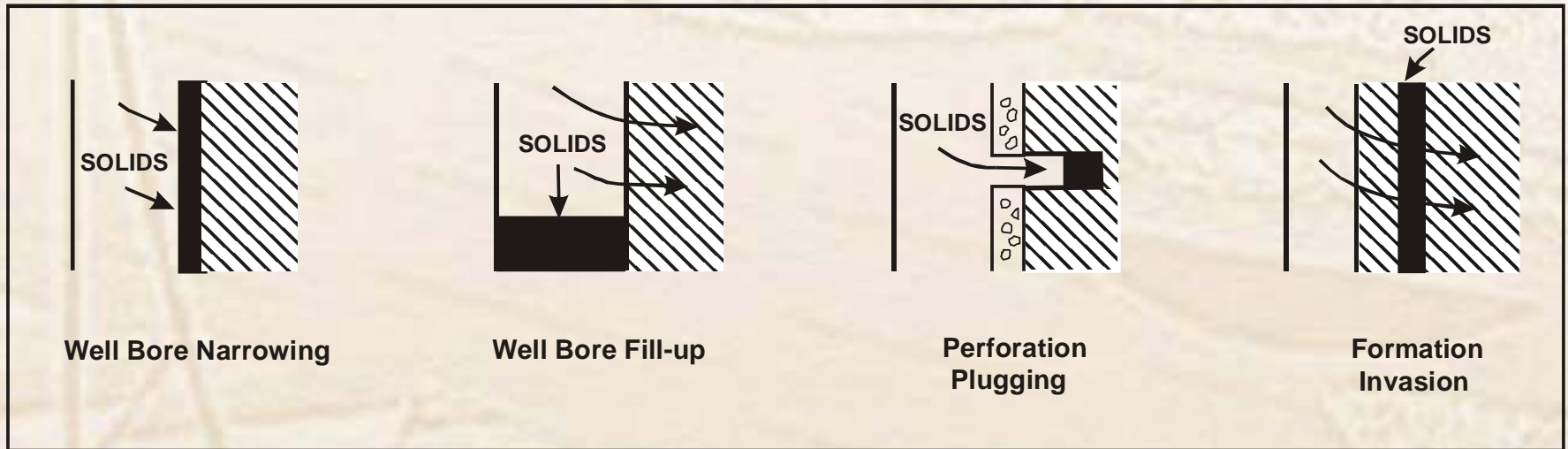
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# WATER INJECTION



## PARTICLE INDUCED DAMAGE MECHANISMS



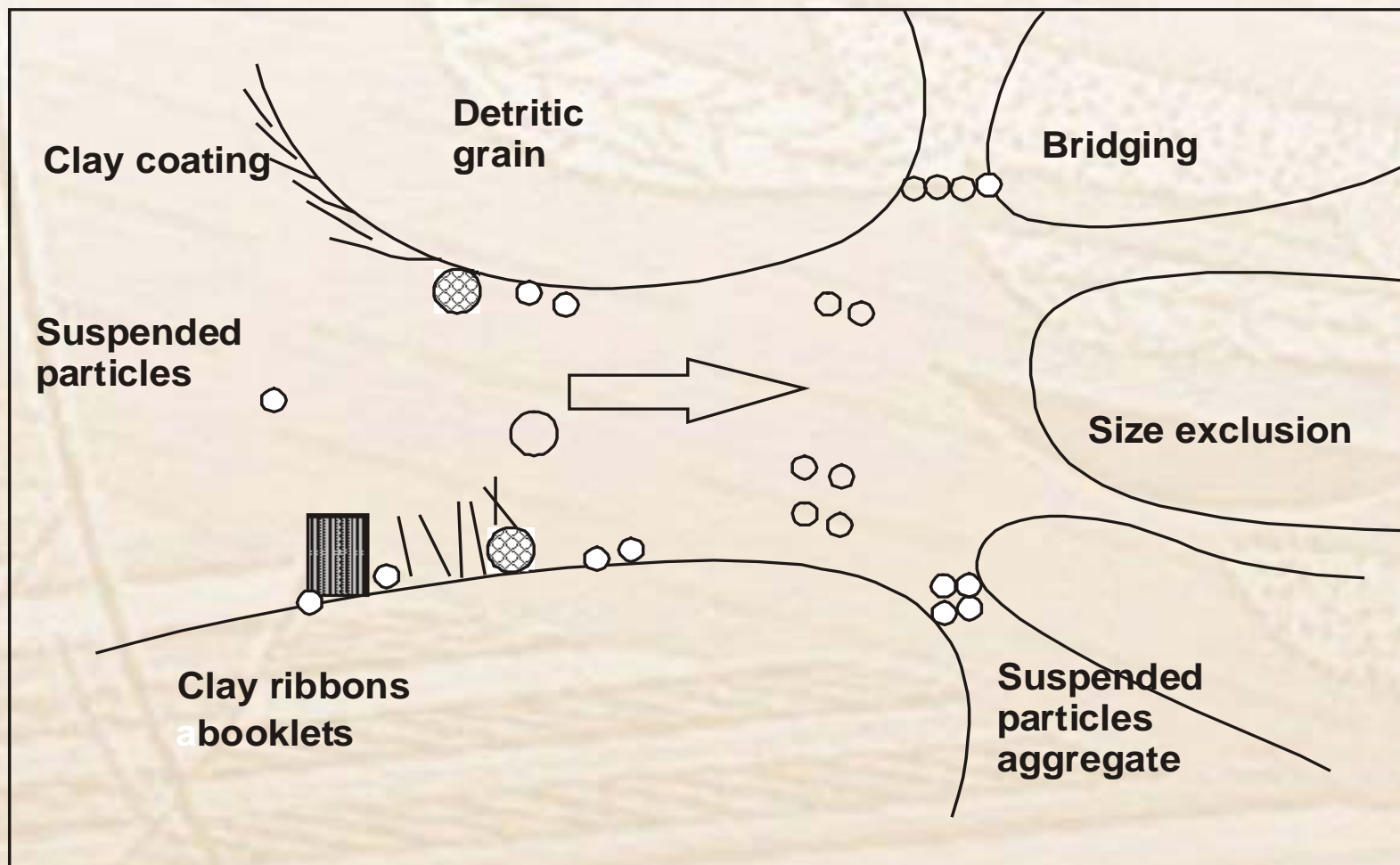
Source : Barkman Davidson  
in Ungemach 2003



# WATER INJECTION



## PARTICLE INDUCED DAMAGE MECHANISMS

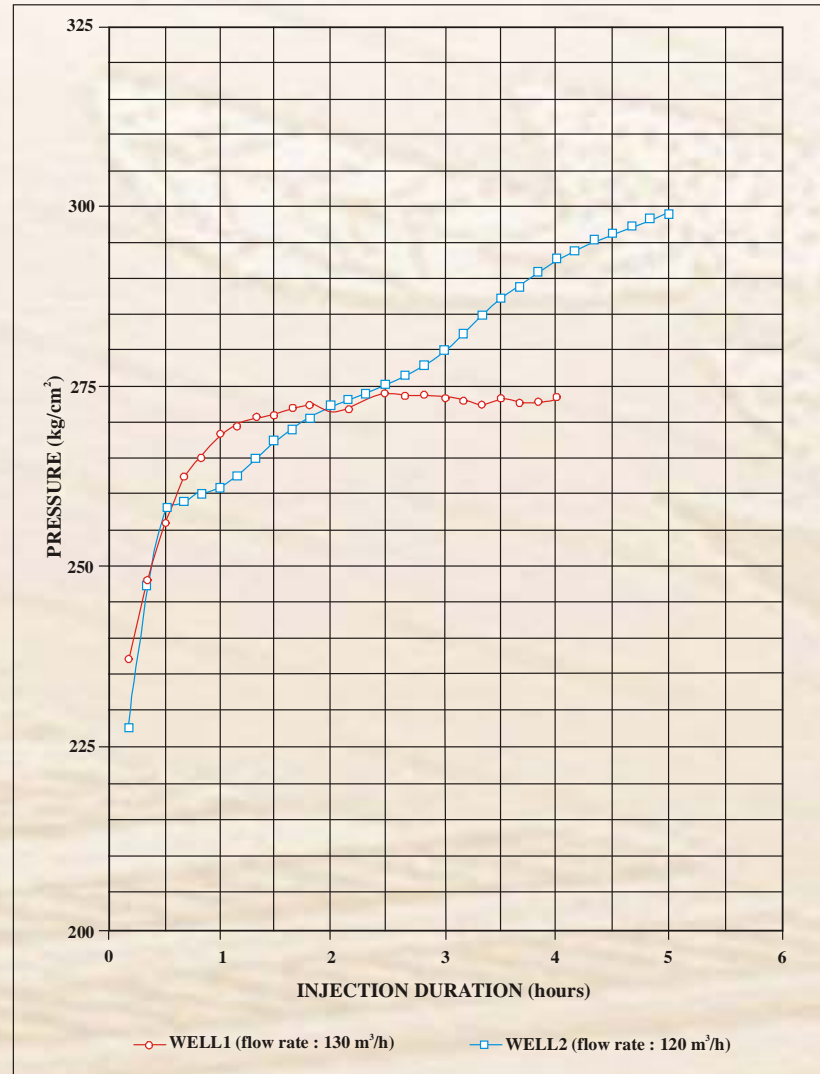




# WATER INJECTION



## PARTICLE INDUCED DAMAGE





# WATER INJECTION IN CLASTIC SEDIMENTS

## WELL COMPLETION REQUIREMENTS

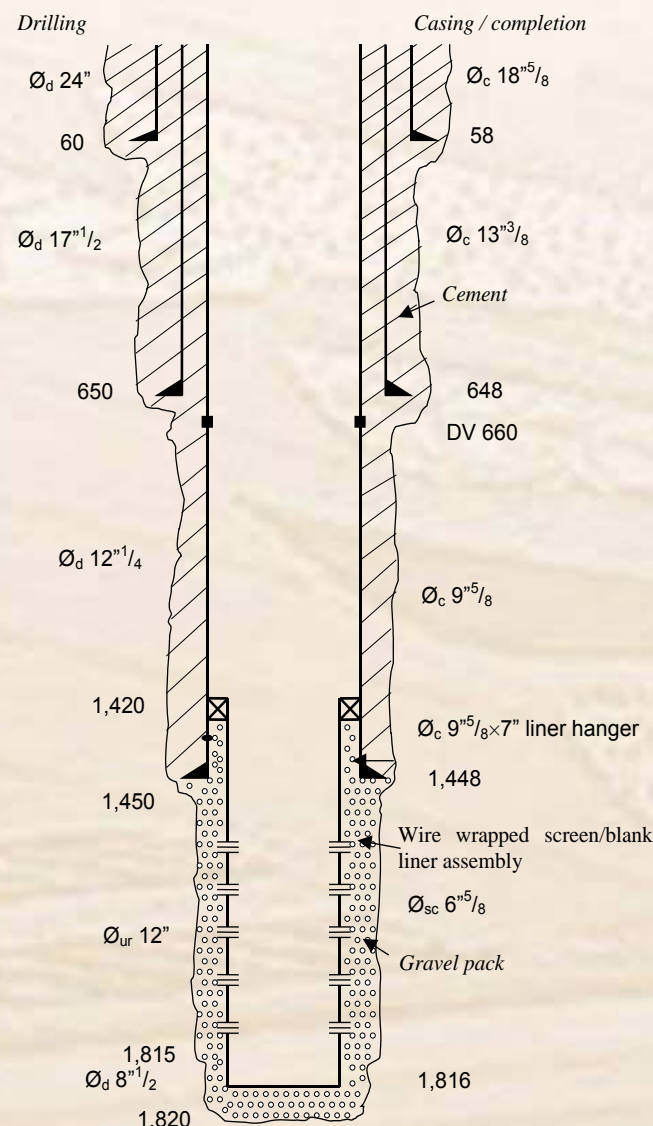
### PROJECTED

### WELL /

### RESERVOIR

### PERFORMANCE

Top reservoir depth .....	1,500 m
Static WHP .....	-5 bars
Total pay .....	400 m
Net pay (h) .....	110 m
Effective porosity ( $\phi_e$ ) .....	0.2
Permeability (k) .....	100 mD
Transmissivity (kh) .....	11,000 mDm
Skin factor (S) .....	-2
Formation temperature .....	90°C
Average injection temperature .....	35°C
Fluid (eq. NaCl) salinity .....	2.5 g/l
Fluid dynamic viscosity (production) ( $\mu_p$ ) .....	0.32 cp
Fluid dynamic viscosity (injection) ( $\mu_i$ ) .....	0.73 cp
Total compressibility factor ( $c_t$ ) .....	$10^{-4}$ bars $^{-1}$
Fluid density ( $\rho_p$ ) at 90°C .....	965.34 kg/m $^3$
Fluid density ( $\rho_i$ ) at 35°C .....	994.06 kg/m $^3$
Target injection rate (Q) .....	150 m $^3$ /hr
WHP (150 m $^3$ /hr, 35°C) .....	20.5 bars
Sandface velocity ( $v_s$ ) .....	0.23 cm/s
Velocity at completion outlet ( $v_c$ ) .....	0.61 cm/s



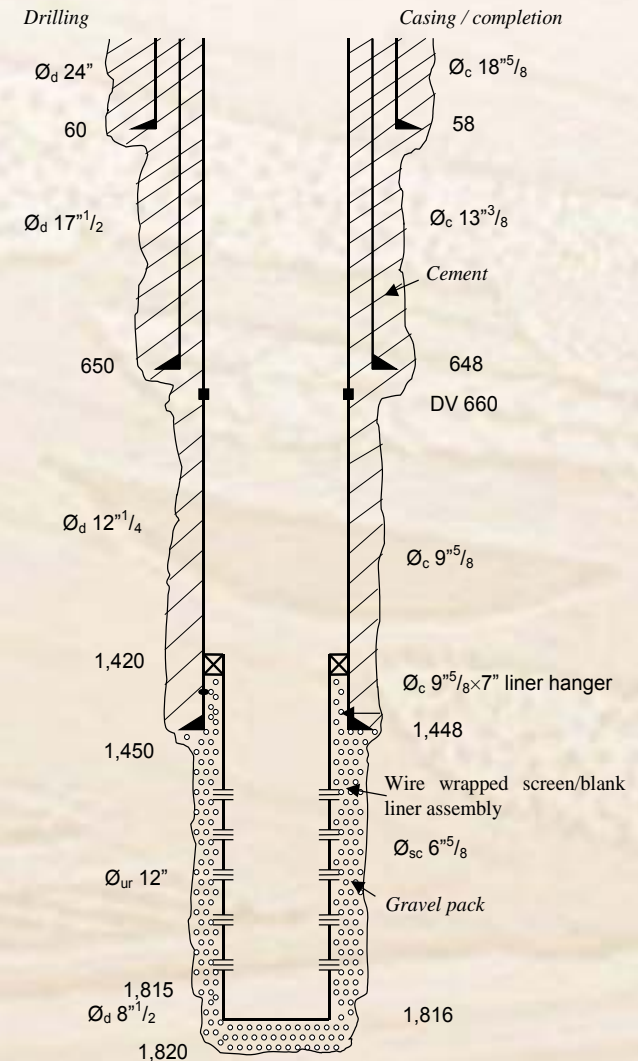


# WATER INJECTION IN CLASTIC SEDIMENTS

## CONCLUSIONS/RECOMMENDATIONS



- **Water injection is merely site specific**
- **Thorough experimental investigations required**
  - petrographic, chemical, turbidity assessments
  - laboratory testing on cores
  - design of brine handling facilities
  - field testing
- **Last but not least sound well completion design**





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# TECHNICAL RISK MATRIX

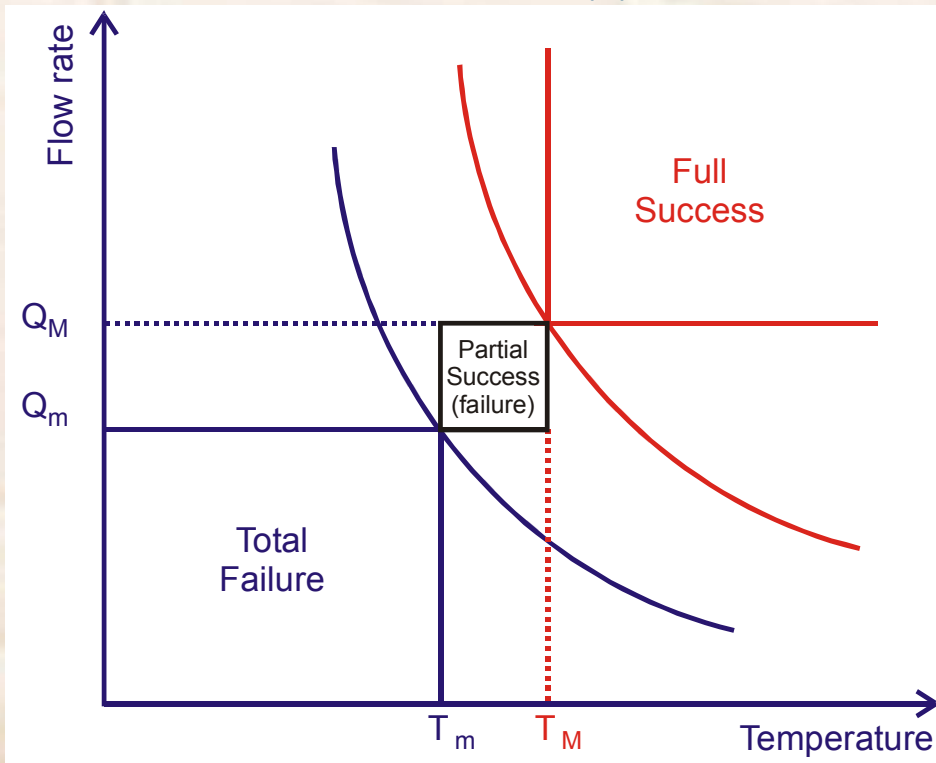
<b>Cause Consequence</b>	<b>Uninsufficient hook load</b>	<b>Inadequate BHAs</b>	<b>Odd cementing</b>	<b>Loose geological control</b>	<b>Odd drilling fluid formulation</b>	<b>Lost BHA, dp</b>
Drilling time	X	X		X	X	X
Dog legs	X	X		X		X
Diameter reduction	X					X
Drilling/completion costs	X		X	X	X	X
Well life			X			
Well loss						X



# MINING RISK INSURANCE



## RISK ASSESSMENT SUCCESS/FAILURE CRITERIA (1)



### Full success:

$$Q(T_{wh} - T_i) = \frac{1}{1.161 \cdot nh \cdot c} \left[ A \cdot INV + OMC + \frac{INV}{n} \right]$$

### Total failure:

$$Q'(T_{wh} - T_i) = \frac{1}{1.161 \cdot nh \cdot c} \left[ A' \cdot INV + OMC + \frac{INV}{n} \right]$$

Where:

$Q, Q'$  = flowrate (yearly average) ( $m^3/h$ )

$T_{wh}$  = production wellhead temperature ( $^{\circ}C$ )

$T_i$  = injection temperature (yearly average) ( $^{\circ}C$ )

$$A = \frac{r(1+r)^n}{(1+r)^n - 1}$$

$$A' = \frac{r'(1+r')^n}{(1+r')^n - 1}$$

$INV$  = capital investment (€)

$OMC$  = operation and maintenance costs (€/yr)

$c$  = heat selling price (€/MWh<sub>t</sub>)

$n$  = project lifetime (years)

$nh$  = number of operating hours per year

$r, r'$  = discount rates

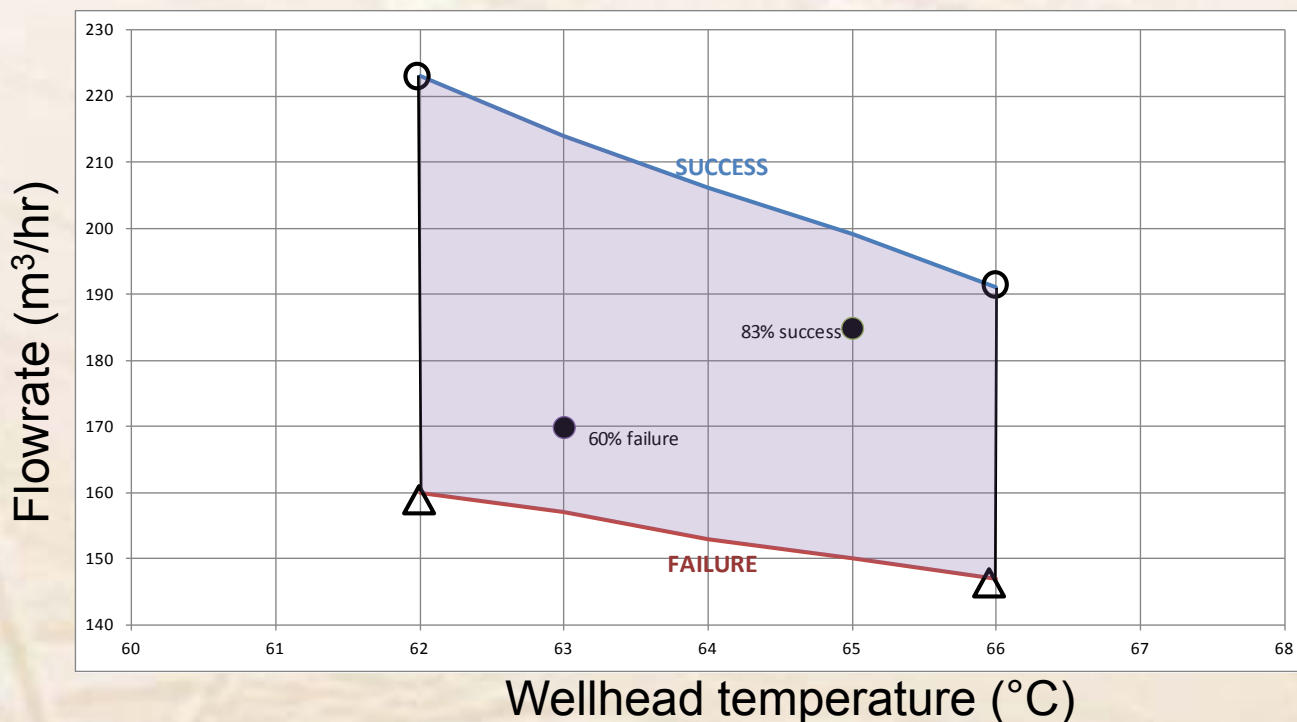
\*  $OMC$  = OPEX

\*  $INV$  = CAPEX



## RISK ASSESSMENT

### SUCCESS/FAILURE CRITERIA (2)



#### Numerical application:

CAPEX =  $12 \cdot 10^6$  €  
 OPEX =  $5 \cdot 10^5$  €  
 n = 20 years  
 nh = 8256 hr/yr  
 r = 5% (total failure)

r = 10% (total success)  
 Full equity (no debt)  
 Subsidies = 0 ; 25% CAPEX  
 c = 35 ; 40 ; 45 €/MWh  
 $T_i$  = 40 ; 45 ; 50 °C



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# SUSTAINABLE GDH RESERVOIR MANAGEMENT



## SUSTAINABILITY

### SUSTAINABLE HEAT EXTRACTION SCENARIOS

Given that GE is renewable and exhaustible

- OBJECTIVE
  - Secure well longevities and reservoir life up to 75/100 years
- PREREQUISITE
  - (Re)Injection of the heat depleted brine into (preferably) the source reservoir
- CONSTRAINTS
  - Project life = 25 years
  - Well life expectation = 20-25 years
  - Target thermal breakthrough = 20 years
- IS THERE A LIFE AFTER ???
  - YES, provided adequate heat mining schemes be designed



# SUSTAINABLE GDH RESERVOIR MANAGEMENT



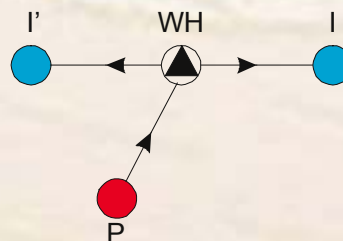
## SUSTAINABILITY MINING SCHEMES

### INITIAL DOUBLET 0-25 yrs



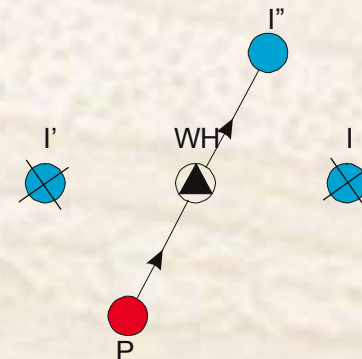
Initial cased wells  
9"5/8 casings

### INTERMEDIATE TRIPLET ARRAY 26-50 yrs

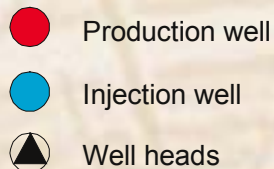


Former doublet wells  
lined (7") as injector wells  
New anti-corrosion production well

### NEW DOUBLET 51-75 yrs



Former injector wells abandoned  
New anti-corrosion injection well



Reservoir impacts

**Sustaining 75 yrs  
System life**



# OUTLINE



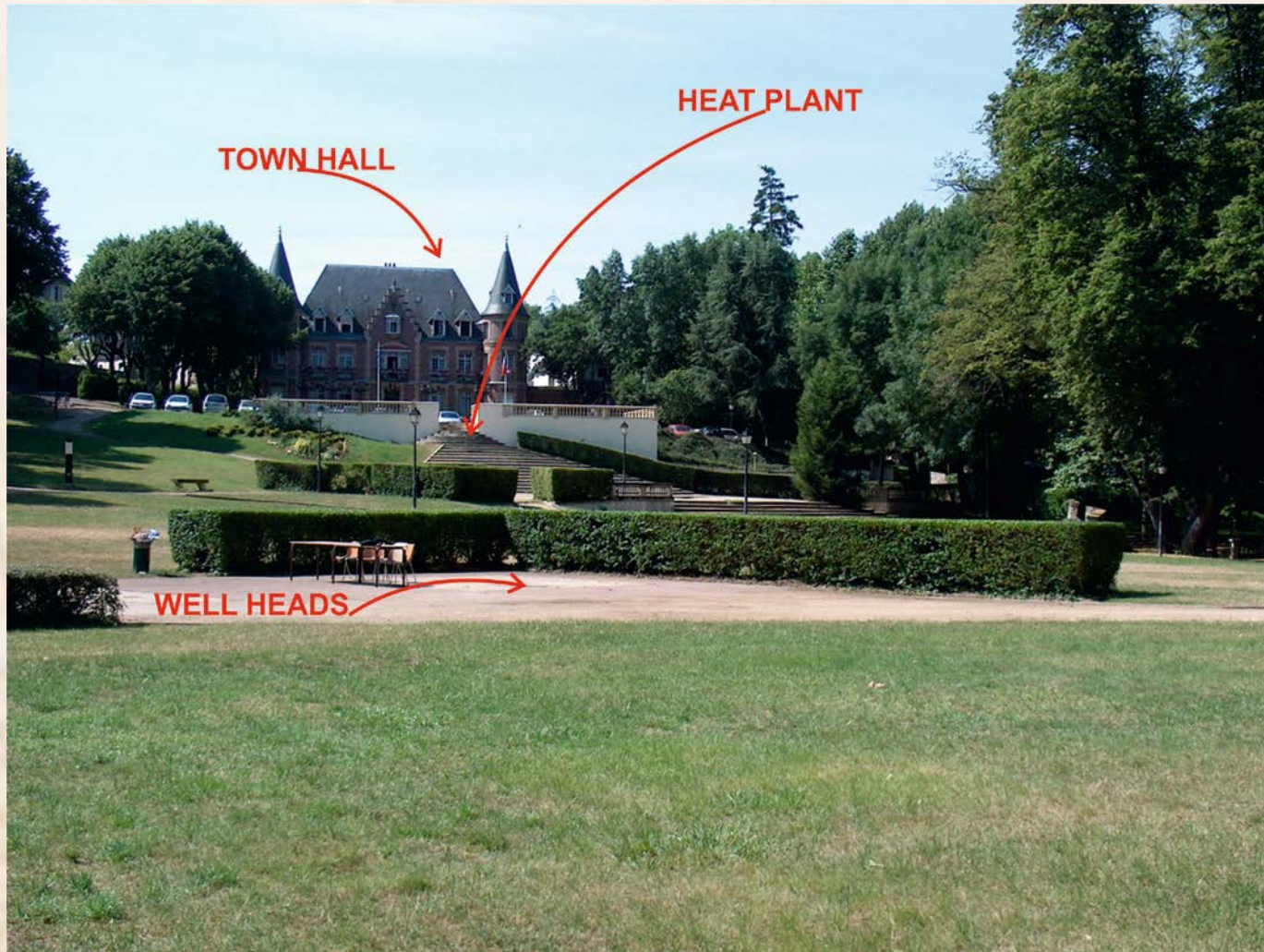
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# A FRIENDLY GDH ENVIRONMENT



## EPINAY-SOUS-SENART AN ENVIRONMENTALLY FRIENDLY SET UP

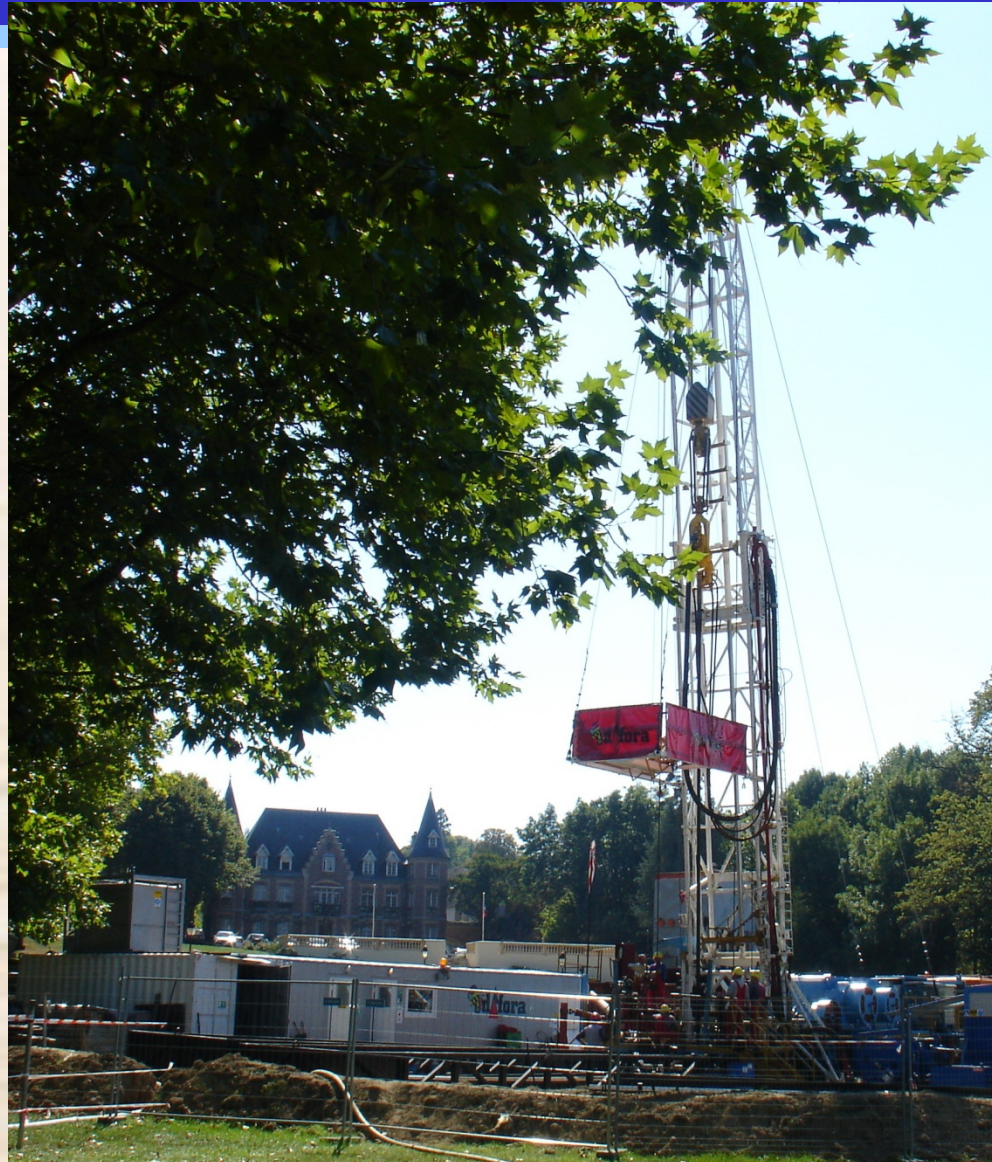




# A FRIENDLY GDH ENVIRONMENT



## WORKOVER SETUP



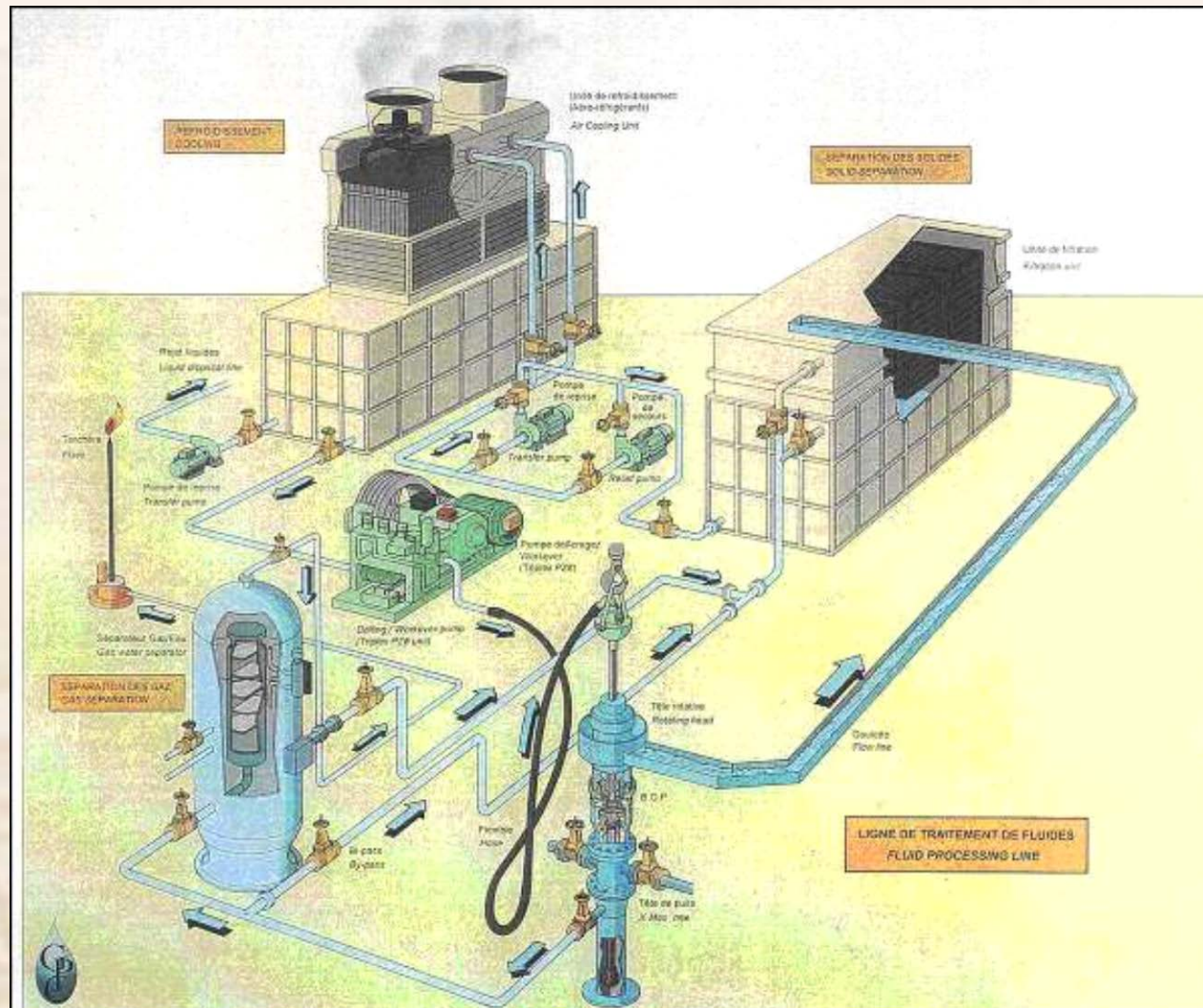


# GAS ABATEMENT LINE





# WORKOVER WASTE PROCESSING LINE





# OUTLINE



- SCOPE
- INTRODUCTION. GEOTHERMAL VS PETROLEUM
- DEEP WELL DRILLING/COMPLETION FEATURES
  - Rig selection
  - Site preparation. Rig footprint
  - Drilling
  - Bits
  - Drilling fluids
  - Directional drilling
  - Casing/lining
  - Cementing
  - Fishing
  - Waste disposal/processing
- CASE STUDY. PARIS BASIN GDH TRIPLET
- MEDIUM ENTHALPY CHP EXPLORATION
  - Deep (4-5 km) exploratory project
  - Slimhole strategy
- UNCONVENTIONAL GEOTHERMAL WELL DESIGNS
  - Dual completion
  - Fiberglass lined anti-corrosion well
  - (sub)Horizontal well concept
- **MISCELLANEOUS ISSUES**
  - Water injection
  - Mining risk insurance
  - Sustainability
  - Environment
  - **Workover**
  - Screens
  - Mud solids'control
- DRILLING CONTRACT. RIG MANAGEMENT. WORK SUPERVISION





# MISCELLANEOUS ISSUES

## TYPICAL GEOTHERMAL WELL WORKOVER PROGRAMME

- 1) Rig mobilisation
- 2) AIT (or equivalent) fishing
- 3) Jetting
- 4) Leak detection logging
  - a. Casing inspection caliper (CIC) (\*)
  - b. Flowmeter / temperature (\*\*)
- 5) Mechanical leak detection
  - Packer leak off tests
- 6) Leak sealing: squeeze cement
- 7) Relining
- 8) Logging:
  - a. CIC
  - b. CBL/VDI(Cement Bond Control)
  - c. ABI (Acoustic Borehole Imager)
- 9) Acid stimulation
- 10) Well test
- 11) Rig de-mobilisation
- 12) Site rehabilitation

(\*) Auxiliary Injection Tubing (Downhole control chemical injection line)

(\*\*) in combination with cold water injection



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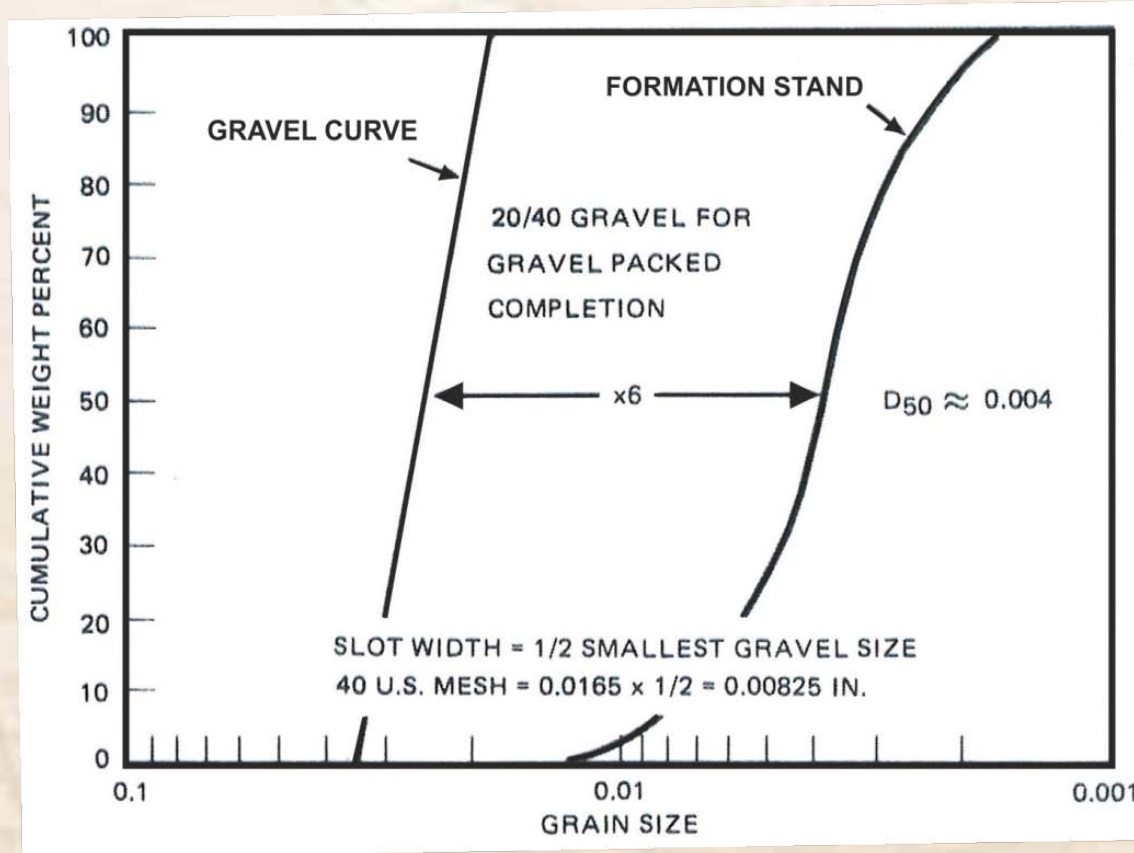


# SCREENS

## GRAVEL PACK DESIGN



### GRAVEL PACK DESIGN



Source : H.P. well screen



# SCREENS

## SCREEN TYPES



### SCREEN TYPES



**WIRE WRAPPED**



**EMBOSSSED RIB**



**SLOTTED LINER**

Source : Johnson screens



# SCREENS

## WIRE WRAPPED SCREENS



### WIRE WRAPPED SCREENS



**STANDARD**



**REINFORCED**



**OIL & GAS  
SUPER REINFORCED**

Source : Johnson screens



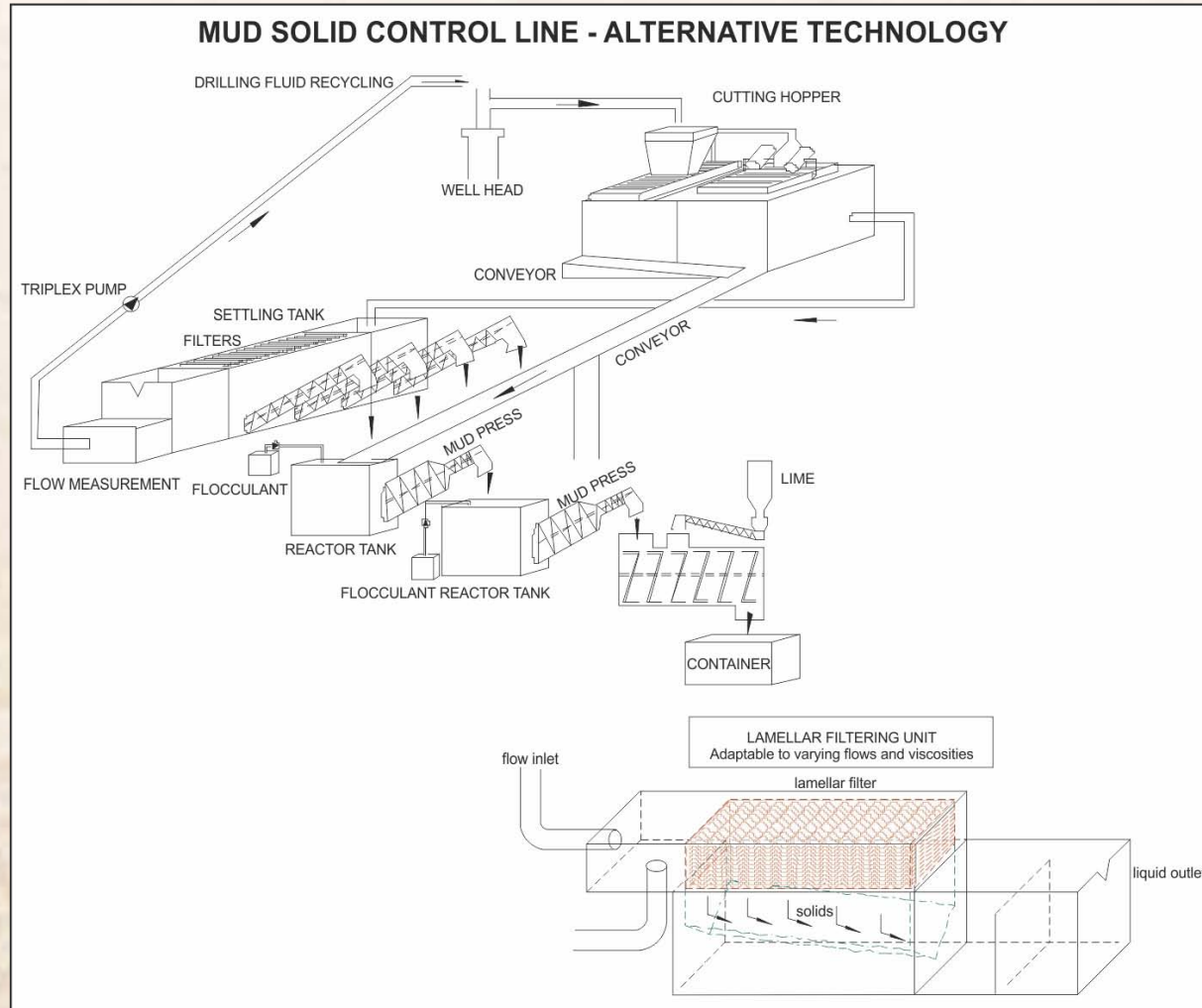
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# MUD SOLIDS CONTROL LINE ALTERNATIVE TECHNOLOGY



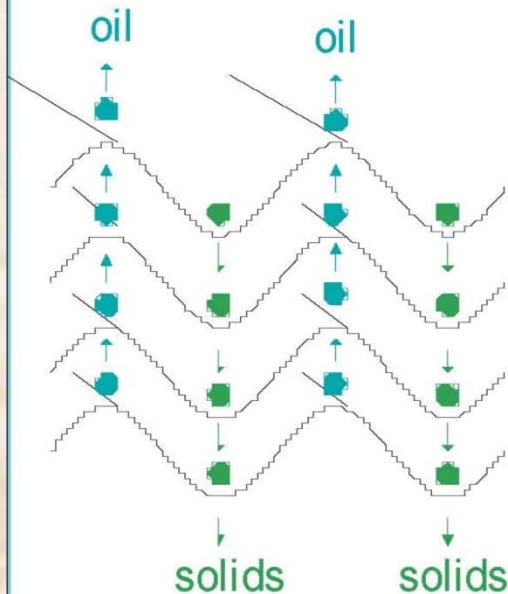


# MUD SOLIDS CONTROL

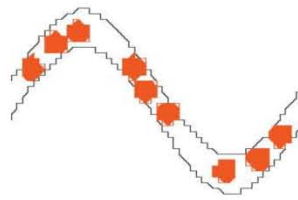
## LAMELLAR FILTERING PRINCIPLE



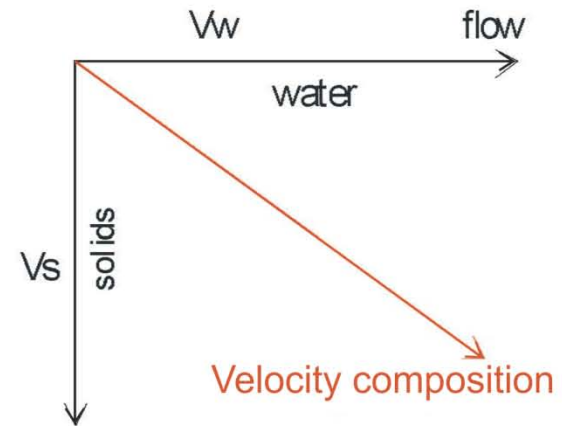
**Wave shaped coalescing plates**



**Particulate aggregation, coalescence**



**Vs calculation**  
 $d < 40 \mu\text{m}$  Stokes Law  
 $d > 40 \mu\text{m}$  Intermediate Law  
 $d > 1000 \mu\text{m}$  Newton Law

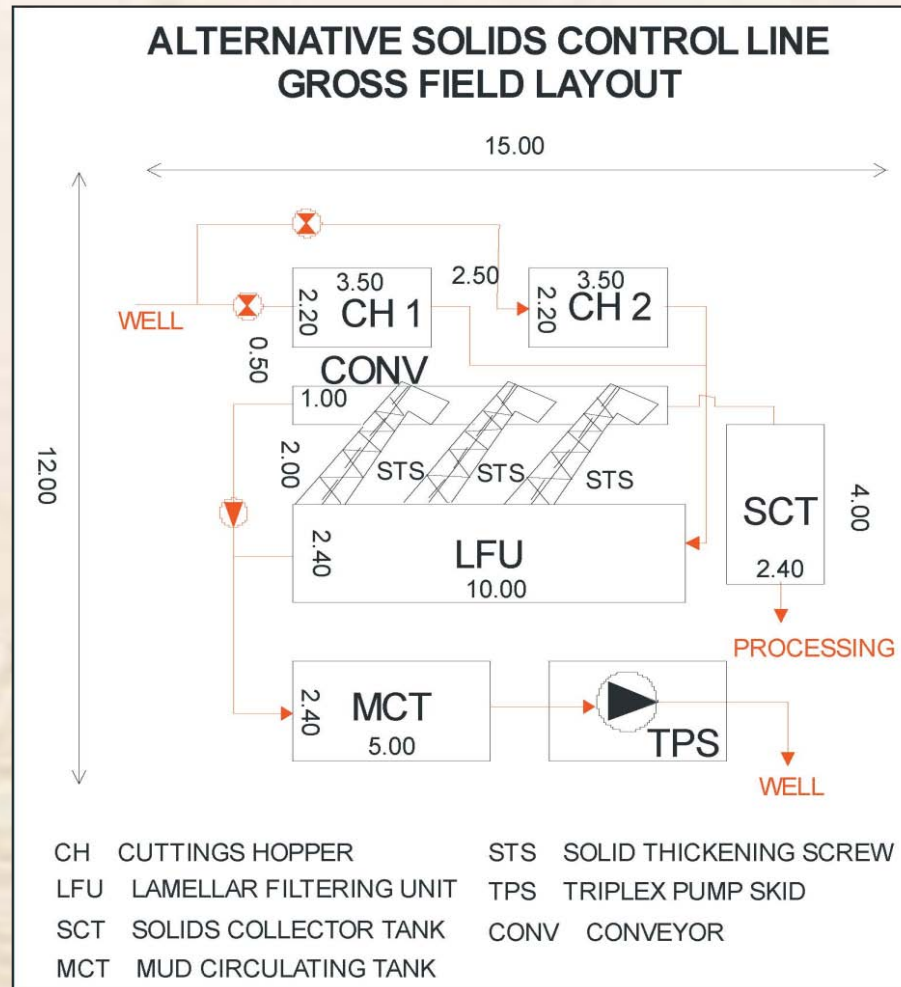


d ( $\mu\text{m}$ )	500	175	125	75	50	20	10
Vs (cm/mn)	550	170	115	65	50	4.4	1.1
tt (mn)	0.2	0.6	0.9	1.5	2.0	20	90
a recycling	85	28	19	11	8.5	0.85	0.2



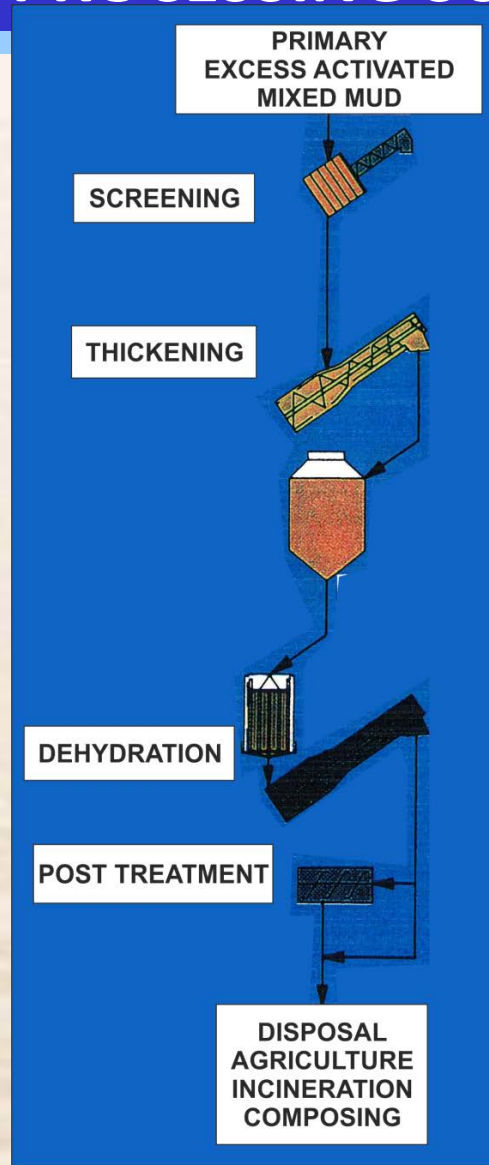
# MUD SOLIDS CONTROL

## ALTERNATIVE SOLIDS CONTROL LINE





# MUD SOLIDS CONTROL MUD PROCESSING SCHEMATICS





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# DRILLING CONTRACTS

Either TURNKEY, METER RATE OR UNIT TIME RATE contracts

TURNKEY	Contractor takes the risk
METER RATE	Both Contractor and Customer share the risk (and costs)
UNIT TIME RATE	Customer takes the risk and costs and responsibility
LOW RISK	Turnkey and meter rate may apply
HIGH RISK	Unit time rate applies

A combination of unit time and meter rate may also be contemplated.



# CONTRACT

## ITEMIZED DRILLING & COMPLETION SEQUENCE

### (Adapted from Hagen Hole)



- Reservoir engineering & Well Targeting (customer)
- Well design and specification (customer)
- Materials specification & procurement (customer)
- Well pad & access road civil design and engineering (customer)
- Water supply design & engineering (customer)
- Civil construction supervision (customer)
- Well drilling engineering and supervision
- Provision of drilling rig and equipment (contractor)
- Provision of drilling personnel (contractor)
- Provision of top drive equipment & personnel (contractor)
- Provision of cementing equipment, personnel & services (contractor)
- Provision of directional drilling equipment & personnel (contractor)
- Provision of mud engineering personnel (contractor)
- Provision of aerated drilling equipment and personnel (optional, contractor)
- Provision of mud logging / geology equipment & personnel (contractor or customer)
- Drilling tool rental or purchase (contractor)
- Drill pipe inspection & hard-banding (customer)
- Provision of well measurements equipment and personnel (customer subcontractor or contractor)



# CONTRACTING

## HYPOTHETICAL EXAMPLE



- An Owner has with its own 'in-house' resources:-
  - Geoscientific and engineering capability  
(or contracts these from Consultants)
  - Reservoir engineering & well targeting
  - Well design, materials specification & procurement
  - Drilling pad & access road design & supervision
  - Drilling engineering & supervision
- Drilling services contract would typically be simple unit time rate contract
  - Owner simply renting equipment & personnel to operate equipment
- - Owner fully responsible to issue all day-to-day instructions for every step of every operation
- Owner carries all the operational responsibility and all operational risk
  - if there are drilling problems - Owner continues to pay day rate.

Source : Hagen Hole



# CONTRACTING ALTERNATIVE MODEL



- Owner may decide that operational responsibility and control is to lie with Contractor  
The extreme of this concept is the 'Pure Turnkey' Contract
- Owners instruction could be – “Drill me a well into this reservoir at this location – come back and tell me when it is completed”
- Owner may have no 'in-house technical capability or necessary managerial resources'
  - Contractor totally responsible, has full control
  - But!!! Carries all of the operational risk

Source : Hagen Hole





# RIG CREW & SUPERVISION STAFF

## RIG CREW

Rig Manager	(1)	Hydraulic electrically powered rigs have been shown to reduce rig crew and mob/demob/rig up/rig down operations
Tool pushers	(2)	
Drillers	(3)	
Assistant driller	(3)	
Derrickman(*)	(3)	
Roughnecks	(6-9)	
Chief mechanics	(2)	
Mechanics	(2-3)	
Chief electrician	(2)	
Electrician	(2-3)	
Rig secretary	(1)	
Safety manager	(1-2)	

## CUSTOMER SUPERVISION STAFF

Drilling/production Engineer	(1)
Drilling supervisor	(1)
Drilling superintendant	(2)
Completion supervisor(**)	(1)
Log Analyst/Testing supervisor	(1)

(\*) if no top drive

(\*\*) optional

Source : ISOR, ICELAND DRILLING



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*The Sun Rises at El Tatio  
But Never Sets on Geothermal Energy*